

# TECHNICAL REFERENCE MANUAL

## Volume 2: Residential Measures

State of Pennsylvania  
Act 129 Energy Efficiency and Conservation Program  
&  
Act 213 Alternative Energy Portfolio Standards

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## TABLE OF CONTENTS

<b>2—RESIDENTIAL MEASURES</b> .....	<b>1</b>
<b>2.1—Lighting</b> .....	<b>1</b>
2.1.1—ENERGY STAR Lighting.....	1
2.1.2—Residential Occupancy Sensors.....	5
2.1.3—LED and Electroluminescent Nightlights.....	7
2.1.4—Holiday Lights.....	9
<b>2.2—HVAC</b> .....	<b>11</b>
2.2.1—High Efficiency Equipment: ASHP, CAC, GSHP, PTAC, PTHP.....	11
2.2.2—High Efficiency Equipment: Ductless Heat Pumps with Midstream Delivery Option.....	16
2.2.3—ECM Circulation Fans.....	24
2.2.4—GSHP Desuperheaters.....	26
2.2.5—Air Conditioner & Heat Pump Maintenance.....	28
2.2.6—Fuel Switching: Electric Heat to Gas/Propane/Oil Heat.....	31
2.2.7—ENERGY STAR Room Air Conditioners.....	34
2.2.8—Room AC (RAC) Retirement.....	37
2.2.9—Duct Sealing & Duct Insulation.....	41
2.2.10—Air Handler Filter Whistles.....	45
2.2.11—ENERGY STAR® Certified Connected Thermostats.....	47
2.2.12—Furnace Maintenance.....	54
<b>2.3—Domestic Hot Water</b> .....	<b>56</b>
2.3.1—Heat Pump Water Heaters.....	56
2.3.2—Solar Water Heaters.....	62
2.3.3—Fuel Switching: Electric Resistance to Fossil Fuel Water Heater.....	65
2.3.4—Water Heater Tank Wrap.....	69
2.3.5—Water Heater Temperature Setback.....	72
2.3.6—Water Heater Pipe Insulation.....	75
2.3.7—Low Flow Faucet Aerators.....	77
2.3.8—Low Flow Showerheads.....	82
2.3.9—Thermostatic Shower Restriction Valves.....	87
2.3.10—Drain Water Heat Recovery Units.....	91
<b>2.4—Appliances</b> .....	<b>95</b>
2.4.1—ENERGY STAR Refrigerators.....	95
2.4.2—ENERGY STAR Freezers.....	103
2.4.3—Refrigerator / Freezer Recycling with and without Replacement.....	107
2.4.4—ENERGY STAR Clothes Washers.....	113
2.4.5—ENERGY STAR Clothes Dryers.....	117
2.4.6—Heat Pump Clothes Dryers.....	120
2.4.7—Fuel Switching: Electric Clothes Dryer to Gas Clothes Dryer.....	123
2.4.8—ENERGY STAR Dishwashers.....	125
2.4.9—ENERGY STAR Dehumidifiers.....	128
2.4.10—Dehumidifier Retirement.....	131
2.4.11—ENERGY STAR Ceiling Fans.....	134

2.4.12	ENERGY STAR Air Purifiers	137
<b>2.5</b>	<b>Consumer Electronics</b>	<b>139</b>
2.5.1	ENERGY STAR Office Equipment	139
2.5.2	Advanced Power Strips	143
<b>2.6</b>	<b>Building Shell</b>	<b>146</b>
2.6.1	Residential Air Sealing	146
2.6.2	Weather Stripping, Caulking, and Outlet Gaskets	151
2.6.3	Ceiling/Attic, Wall, Floor and Rim Joist Insulation	157
2.6.4	Basement or Crawl Space Wall Insulation	162
2.6.5	ENERGY STAR Windows	167
2.6.6	Residential Window Repair	170
<b>2.7</b>	<b>Whole Home</b>	<b>173</b>
2.7.1	Residential New Construction	173
2.7.2	ENERGY STAR Manufactured Homes	181
2.7.3	Home Energy Reports	186
<b>2.8</b>	<b>Miscellaneous</b>	<b>190</b>
2.8.1	Variable Speed Pool Pumps	190
<b>2.9</b>	<b>Demand Response</b>	<b>193</b>
2.9.1	Direct Load Control and Behavior-Based Demand Response Programs	193

**LIST OF FIGURES**

Figure 2-1: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup> ..... 78  
Figure 2-2: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup> ..... 83  
Figure 2-3: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup> ..... 88  
Figure 2-4: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup> ..... 92  
Figure 2-5: Example Regressions for Ductless Mini-splits in Climate Region A ..... 147  
Figure 2-6: Uo Baseline Requirements ..... 183

## LIST OF TABLES

Table 2-1: Terms, Values, and References for ENERGY STAR Lighting.....	2
Table 2-2: Bulb and Fixture Hours of Use and Peak Coincidence Factor Values, by Room.....	3
Table 2-3: Energy and Demand HVAC Interactive Effects by EDC.....	4
Table 2-4: Terms, Values, and References for Residential Occupancy Sensors.....	5
Table 2-5: Terms, Values, and References for LED and Electroluminescent Nightlights.....	7
Table 2-6: Terms, Values, and References for Holiday Lights.....	9
Table 2-7: Terms, Values, and References for High Efficiency Equipment: ASHP, CAC, GSHP, PTAC, PTHP.....	12
Table 2-8: Default Baseline Equipment Efficiency for High Efficiency Equipment.....	14
Table 2-9: Default Oversize Factors for High Efficiency Equipment.....	14
Table 2-10: Terms, Values, and References for High Efficiency Equipment: Ductless Heat Pump.....	18
Table 2-11: Ductless Heat Pump Usage Zones.....	20
Table 2-12: Default Ductless Heat Pump Efficiencies.....	20
Table 2-13: Oversize and Duct Leakage Factors for High Efficiency Equipment.....	20
Table 2-14: Midstream DHP – SEER and EER Baseline Splits.....	20
Table 2-15: Midstream DHP – HSPF Baseline Splits.....	21
Table 2-16: Midstream DHP – $DLF_{cool}$ and $OF_{cool}$ Baseline Splits.....	21
Table 2-17: Midstream DHP – $DLF_{heat}$ and $OF_{heat}$ Baseline Splits.....	21
Table 2-18: Midstream DHP – Composite EFLH Values.....	21
Table 2-19: Terms, Values, and References for ECM Furnace Fan.....	24
Table 2-20: Terms, Values, and References for GSHP Desuperheater.....	26
Table 2-21: Terms, Values, and References for Air Conditioner & Heat Pump Maintenance.....	29
Table 2-22: Terms, Values, and References for Fuel Switching: Electric Heat to Gas Heat.....	32
Table 2-23: Terms, Values, and References for ENERGY STAR Room AC.....	34
Table 2-24: RAC (without reverse cycle) Federal Minimum Efficiency and ENERGY STAR Version 4.1 Standards.....	35
Table 2-25: Casement-Only and Casement-Slider RAC Federal Minimum Efficiency and ENERGY STAR Version 4.1 Standards.....	35
Table 2-26: Reverse Cycle RAC Federal Minimum Efficiency Standards and ENERGY STAR Version 4.1 Standards.....	35
Table 2-27: Deemed EFLH and Default Energy Savings.....	36
Table 2-28: Terms, Values, and References for Room AC Retirement.....	38
Table 2-29: RAC Retirement-Only EFLH and Energy Savings by City.....	39
Table 2-30: Terms, Values, and References for Duct Sealing.....	42
Table 2-31: Distribution Efficiency by Climate Zone; Conditioned Air Type; Duct Location, Leakage & Insulation.....	43
Table 2-32: Distribution Efficiency Adders for Cond. Space (%) by Conditioned Air; Duct Location, Leakage & Insulation.....	44
Table 2-33: Terms, Values, and References for Air Handler Filter Whistle.....	45
Table 2-34: Default Air Handler Filter Whistle Savings.....	46

Table 2-35: Installation Classification ..... 48

Table 2-36: Residential Electric HVAC Calculation Assumptions ..... 49

Table 2-37: Cooling Energy Savings Factors (ESF<sub>cool</sub>) ..... 50

Table 2-38: Heating Energy Savings Factors (ESF<sub>heat</sub>) ..... 51

Table 2-39: Default Statewide Cooling Savings (kWh/yr) ..... 51

Table 2-40: Default Statewide Heating Savings (kWh/yr) ..... 52

Table 2-41: Default Statewide Total Heating and Cooling Savings (kWh/yr) ..... 52

Table 2-42: Terms, Values, and References for Furnace Maintenance ..... 54

Table 2-43: Default Savings per Input kBTU/h for Furnace Maintenance ..... 55

Table 2-44: Terms, Values, and References for Heat Pump Water Heater ..... 57

Table 2-45: Default Cooling and Heating System Efficiencies ..... 58

Table 2-46: Draw Pattern Definitions ..... 58

Table 2-47: Minimum Baseline Uniform Energy Factors Based on Rated Storage Volume and Draw Pattern ..... 58

Table 2-48: UEF De-rating Factor for Various Installation Locations ..... 60

Table 2-49: Terms, Values, and References for Solar Water Heater ..... 63

Table 2-50: Terms, Values, and References for Fuel Switching: Electric Resistance to Fossil Fuel Water Heater ..... 66

Table 2-51: Energy Savings & Demand Reductions for Fuel Switching, Domestic Hot Water Electric to Fossil Fuel ..... 67

Table 2-52: Fuel Consumption for Fuel Switching, Domestic Hot Water Electric to Fossil Fuel .. 67

Table 2-53: Terms, Values, and References for Water Heater Tank Wrap ..... 69

Table 2-54: Deemed savings by water heater capacity ..... 70

Table 2-55: Terms, Values, and References for Water Heater Temperature Setback ..... 73

Table 2-56: Default Energy Savings and Demand Reductions ..... 73

Table 2-57: Terms, Values, and References for Water Heater Pipe Insulation ..... 75

Table 2-58: Low Flow Faucet Aerator Calculation Assumptions ..... 78

Table 2-59: Average Number of Faucets per Home ..... 79

Table 2-60: Default Savings for Low Flow Faucet Aerators ..... 79

Table 2-61: Terms, Values, and References for Low Flow Showerhead ..... 83

Table 2-62: Default Savings for Low Flow Showerheads ..... 84

Table 2-63: Terms, Values, and References for Thermostatic Shower Restriction Valve ..... 88

Table 2-64: Default Savings for Thermostatic Restriction Valve ..... 89

Table 2-65: Terms, Values, and References for Drain Water Heat Recovery Units ..... 92

Table 2-66: Default Savings for Drain Water Heat Recovery Unit ..... 93

Table 2-67: Terms, Values, and References for ENERGY STAR Refrigerators ..... 96

Table 2-68: Federal Standard and ENERGY STAR Refrigerators Maximum Annual Energy Consumption if Configuration and Volume Known ..... 96

Table 2-69: Default Savings Values for ENERGY STAR Refrigerators ..... 98

Table 2-70: ENERGY STAR Most Efficient Annual Energy Usage if Configuration and Volume Known<sup>Source 4</sup> ..... 99

Table 2-71: Default Savings Values for ENERGY STAR Most Efficient Refrigerators<sup>Source 4</sup> ..... 101

Table 2-72: Terms, Values, and References for ENERGY STAR Freezers ..... 103

Table 2-73: Federal Standard and ENERGY STAR Freezers Maximum Annual Energy Consumption if Configuration and Volume Known.....	104
Table 2-74: Default Savings Values for ENERGY STAR Freezers.....	105
Table 2-75: Terms, Values, and References for Refrigerator and Freezer Recycling.....	109
Table 2-76: Terms, Values, and References for ENERGY STAR Clothes Washers.....	114
Table 2-77: Federal Standards and ENERGY STAR Specifications for Clothes Washers <sup>Source 2-8</sup> .....	115
Table 2-78: Default Clothes Washer Savings.....	115
Table 2-79: Terms, Values, and References for ENERGY STAR Clothes Dryers.....	117
Table 2-80: Combined Energy Factor for Federal Minimum Standard and ENERGY STAR Dryers.....	118
Table 2-81: Default Energy Savings and Demand Reductions for ENERGY STAR Clothes Dryers.....	118
Table 2-82: Terms, Values, and References for Heat Pump Clothes Dryers.....	120
Table 2-83: Default Savings for Heat Pump Clothes Dryers.....	121
Table 2-84: Terms, Values, and References for Fuel Switching: Electric Clothes Dryer to Gas Clothes Dryer.....	123
Table 2-85: Terms, Values, and References for ENERGY STAR Dishwashers.....	125
Table 2-86: Federal Standard and ENERGY STAR v 6.0 Residential Dishwasher Standard.....	126
Table 2-87: Default Dishwasher Energy Savings.....	126
Table 2-88: Terms, Values, and References for ENERGY STAR Dehumidifier.....	128
Table 2-89: Dehumidifier Minimum Federal Efficiency Standards.....	129
Table 2-90: Dehumidifier ENERGY STAR Standards.....	129
Table 2-91: Dehumidifier ENERGY STAR Most Efficient Criteria.....	129
Table 2-92: Dehumidifier Default Energy Savings.....	129
Table 2-93: Terms, Values, and References for Dehumidifier Retirement.....	132
Table 2-94: Dehumidifier Retirement Annual Energy Savings (kWh).....	132
Table 2-95: Dehumidifier Retirement Peak Demand Reduction (kW).....	132
Table 2-96: Default Dehumidifier Retirement Annual Energy Savings (kWh).....	133
Table 2-97: Default Dehumidifier Retirement Peak Demand Reduction (kW).....	133
Table 2-98: Terms, Values, and References for ENERGY STAR Ceiling Fans.....	135
Table 2-99: Assumed Wattage of ENERGY STAR Ceiling Fans on High Setting.....	135
Table 2-100: Energy Savings and Demand Reductions for ENERGY STAR Ceiling Fans.....	135
Table 2-101: Terms, Values, and References for ENERGY STAR Air Purifier.....	137
Table 2-102: Energy Savings Calculation Default Values.....	138
Table 2-103: Demand Savings Calculation Default Values.....	138
Table 2-104: Terms, Values, and References for ENERGY STAR Office Equipment.....	140
Table 2-105: ENERGY STAR Office Equipment Energy and Demand Savings Values.....	141
Table 2-106: Terms, Values, and References for Advanced Power Strips.....	144
Table 2-107: Impact Factors for Advanced Power Strip Types.....	145
Table 2-108: Default Savings for Advanced Power Strips.....	145
Table 2-109: Terms, Values, and References for Residential Air Sealing.....	148
Table 2-110: Default Residential Equipment Efficiency.....	149



Table 2-111: Default Unit Energy Savings per Reduced CFM50<sup>2</sup> for Air Sealing..... 149

Table 2-112: Default Unit Energy Savings per Reduced CFM50 for Air Sealing..... 150

Table 2-113: Terms, Values, and References for Weather Stripping ..... 152

Table 2-114: Correlation Factor <sup>Source 2</sup> ..... 153

Table 2-115: Latent Multiplier Values by Climate Reference City..... 153

Table 2-116: Typical Reductions in Leakage <sup>Source</sup> ..... 154

Table 2-117: Default Annual Energy Savings ..... 154

Table 2-118: Default Summer Peak Demand Savings..... 155

Table 2-119: Terms, Values, and References for Basement Wall Insulation ..... 158

Table 2-120: Default Base and Energy Efficient (Insulated) R Values..... 160

Table 2-121: Terms, Values, and References for Basement or Crawl Space Insulation..... 163

Table 2-122: Below-grade R-values ..... 165

Table 2-123: Terms, Values, and References for ENERGY STAR Windows..... 168

Table 2-124: Default UES<sub>region, system</sub>, kWh per Square Foot of Replaced Window ..... 168

Table 2-125: Terms, Values, and References for Residential Window Repair..... 171

Table 2-126: Existing Infiltration Assumptions ..... 172

Table 2-127: Terms, Values, and References for Residential New Construction..... 174

Table 2-128: Baseline Insulation and Fenestration Requirements by Component for Buildings Less Than 4 Stories (Equivalent U-Factors) <sup>Source-10</sup> ..... 175

Table 2-129: Residential New Construction Baseline Building Values for Buildings Less Than 4 Stories..... 175

Table 2-130: Baseline Insulation and Fenestration Requirements by Component for Buildings 4 Stories or Higher (Equivalent U-Factors) <sup>Source-13</sup> ..... 177

Table 2-131: Residential New Construction Baseline Building Values for Buildings 4 Stories or Higher ..... 177

Table 2-132: Minimum Baseline Gas-Fired Uniform Energy Factors Based on Storage Volume and Draw Pattern..... 178

Table 2-133: ENERGY STAR Manufactured Homes – References ..... 182

Table 2-134: ENERGY STAR Manufactured Homes – User Defined Reference Home ..... 183

Table 2-135: Home Energy Report Persistence Example ..... 186

Table 2-136: Calculation of Avoided Decay and Incremental Annual Compliance Savings ..... 187

Table 2-137: Terms, Values, and References for HER Persistence Protocol ..... 189

Table 2-138: Terms, Values, and References for Variable Speed Pool Pumps ..... 190

Table 2-139: Single Speed Pool Pump Specification ..... 191

Table 2-140: Definition of Terms for Estimating DLC and Behavior-based Load Impacts..... 195

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## 2 RESIDENTIAL MEASURES

The following section of the TRM contains savings protocols for residential measures.

### 2.1 LIGHTING

## 2 ENERGY STAR RESIDENTIAL MEASURES

### 2.1 LIGHTING

#### 2.1.1 RESIDENTIAL LED LIGHTING

Target Sector	Residential Establishments
Measure Unit	Light Bulb or Fixture
Measure Life	LED Replace on Burnout: 15 years <sup>Source 1</sup> Early Replacement: 2 years <sup>Source 2</sup>
Vintage	Replace on Burnout (Upstream, Kit) Early Replacement (Direct Install)

Savings for residential energy efficient LED lighting products are based on a straightforward algorithm that calculates the difference between baseline and new wattage and the average daily hours of usage for the lighting unit being replaced. As of the writing of this TRM, federal standards for 2024 are uncertain. Baseline values in this measure represent the known EISA 2020 “backstop” provisions. An “in-service” rate is used to reflect the fact that not all lighting products purchased are actually installed. The algorithms include default values for estimating savings from sales to non-residential customers. Screw-based general service LED lamps are limited to direct install programs due to the US Department of Energy’s codification of the 45 lumen per watt “backstop” requirement for general service lamps (GSLs). Linear LED fixtures are eligible measures while LED fixtures that effectively replace GSLs, such as downlighting, are not eligible.

#### ELIGIBILITY

##### Definition of Efficient Equipment

Table 2.1 provides a summary of the eligibility for residential LED lighting measures and program delivery channels.

Table 2. In order for this measure protocol to apply, the high-efficiency equipment must be a screw-in ENERGY STAR LED bulb (general service or specialty bulb) or LED fixture.<sup>2</sup>

##### 1: Eligibility for Residential LED Lighting

Efficient LED Lighting Product	Lumen Range	Program Delivery	Eligibility
GSL bulb type, below 310 lumens	Less than 310	All	Yes
GSL	310 to 3,300	Retail / upstream	No
		Kit	No

<sup>1</sup> Act 129 Legislation caps measure life at 15 years. Assuming 3 hours of use a day, 15 years equals 16,425 hours. As of December 2018, average rated life hours for ENERGY STAR qualified LEDs was >22,000 hours. See <https://www.energystar.gov/products/lighting-fans>.

<sup>2</sup> The protocol also applies to products that are pending ENERGY STAR qualification.

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<u>Efficient LED Lighting Product</u>	<u>Lumen Range</u>	<u>Program Delivery</u>	<u>Eligibility</u>
		<u>Direct Install</u>	<u>Yes</u>
<u>GSL bulb type, above 3,300 lumens</u>	<u>Greater than 3,300</u>	<u>All</u>	<u>Yes</u>
<u>GSL, exempt bulb type / category</u>	<u>NA</u>	<u>All</u>	<u>Yes</u>
<u>Linear LED fixture</u>	<u>NA</u>	<u>All</u>	<u>Yes</u>
<u>All other fixtures</u>	<u>NA</u>	<u>All</u>	<u>No</u>

### Definition of Baseline Equipment

The baseline equipment is assumed to be a bulb or fixture with an efficacy equal to 45 lumens per watt. For upstream buy-down, retail (time of sale), or efficiency kit programs, baseline wattages can be determined using the methods described below. For varies by lighting product and delivery channel. GSLs<sup>Source 3</sup> are only eligible for direct install programs where the wattage of the existing bulb is known, and the existing bulb was in working condition; the baseline wattage is the wattage of the existing lamp removed by the program may be used as. For LED lamps outside the GSL lumen range (below 310 lumens or above 3,300 lumens) and/or exempt bulb type/categories, the baseline wattage is the manufacturer rated comparable wattage. Baseline wattages for linear LED fixtures are defined in Table 2-3. GSLs are defined in accordance with the US DOE's updated definition of GSLs effective July 8, 2022, which expanded GSLs to include previously exempt bulb types such as, but not limited to, reflector lamps, rough service lamps, shatter-resistant lamps, 3-way lamps, candelabra lamps, and vibration service lamps. <sup>Source 4</sup>

### ALGORITHMS

The general form of the equation for the ENERGY STAR or other high-efficiency residential LED lighting energy savings algorithm is:

$$\text{Total Savings} = \text{Number of Units} \times \text{Savings per Unit}$$

Energy and demand savings algorithms include a term to account for cross-sector sales (i.e., lamps that end up in non-residential use). Default values for non-residential terms are based on values in Vol. 3, Sec. 3.1.7 Lighting Improvements for Midstream ([http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/technical\\_reference\\_manual.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/technical_reference_manual.aspx)). For direct install programs or other programs where it is known that all lamps will be in residential end uses, there are no non-residential energy or demand savings.

$$\Delta kWh_{res} = \frac{Watts_{base} - Watts_{EE}}{1000 \frac{W}{kW}} \times (1 + IE_{kWh,res}) \times ISR_{res} \times HOU_{res} \times 365 \frac{days}{yr} \times (1 - CSS)$$

$$\Delta kWh_{non-res} = \frac{Watts_{base} - Watts_{EE}}{1000 \frac{W}{kW}} \times (1 + IE_{kWh,non-res}) \times ISR_{non-res} \times HOU_{non-res} \times 365 \frac{days}{yr} \times CSS$$

$$\Delta kW_{peak,res} = \frac{Watts_{base} - Watts_{EE}}{1000 \frac{W}{kW}} \times (1 + IE_{kW,res}) \times ISR_{res} \times CF_{res} \times (1 - CSS)$$

$$\Delta kW_{peak,non-res} = \frac{Watts_{base} - Watts_{EE}}{1000 \frac{W}{kW}} \times (1 + IE_{kW,non-res}) \times ISR_{non-res} \times CF_{non-res} \times CSS$$

**DEFINITION OF TERMS**

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$$\Delta kWh = \frac{Watts_{base} - Watts_{EE}}{1,000} \times (1 + L \times IE_{kWh}) \times ISR \times HOU \times 365$$

$$\Delta kW_{summer\ peak} = \frac{Watts_{base} - Watts_{EE}}{1,000} \times (1 + L \times IE_{kW,s}) \times ISR \times CF_s$$

$$\Delta kW_{winter\ peak} = \frac{Watts_{base} - Watts_{EE}}{1,000} \times (1 + L \times IE_{kW,w}) \times ISR \times CF_w$$

For linear LED fixtures, the following algorithm is used to calculate Watts<sub>base</sub> for use in the above formulas:

$$Watts_{base} = \frac{Lumens_{ge}}{Efficacy_{base}}$$

**DEFINITION OF TERMS**

Table 2-2: Terms, Values, and References for ENERGY STAR Residential LED Lighting

Term	Unit	Value	Sources
Watts <sub>base</sub> , Wattage of baseline case lamp/fixture	Watts	Direct install: EDC Data Gathering <sup>3</sup> GSLs outside of EISA lumen range or see Baseline Wattage Values below exempt bulb type: Manufacturer rated comparable wattage Linear LED fixture: EDC Data Gathering (Lumens <sub>ge</sub> ) and Table 2-3 (Efficacy <sub>base</sub> )	EDC data gathering, 3 and 4
Watts <sub>EE</sub> , Wattage of efficient case lamp/fixture	Watts	EDC Data Gathering	EDC Data Gathering
HOU <sub>res</sub> , Average hours of use per day per unit installed for residential use	hours/day	Table 2-4	27
HOU <sub>non-res</sub> , Average hours of use per day per unit installed for non-residential use. Factor to adjust interactive effect factors to account for proportion of LEDs installed in interior locations	hours/day %	EDC Data Gathering Default = 6.85 Interior: 100% Exterior: 0% Unknown: 90.3%	510

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<sup>3</sup> EDCs may use the wattage of the replaced bulb for directly installed program bulbs

Term	Unit	Value	Sources
<del><math>IE_{kW,res}</math>, HVAC Interactive Effect for LED energy for residential use</del>	<del>None</del>	<del>EDC Data Gathering Default = Table 2-5 Exterior Fixtures: 0%</del>	<del>36</del>
<del><math>IE_{kW,res,s}</math>, HVAC Summer Interactive Effect for LED demand for residential use lighting in conditioned residential spaces.</del>	<del>None</del>	<del>EDC Data Gathering Default = Table 2-3 Table 2-5 Exterior Fixtures: 0%</del>	<del>36</del>
<del><math>IE_{kW,non-res}</math>, HVAC Interactive Effect for LED energy for non-residential use</del>	<del>None</del>	<del>EDC Data Gathering Default = 0%</del>	<del>5</del>
<del><math>IE_{kW,non-res,w}</math>, HVAC Winter Interactive Effect for LED demand for non-Residential use lighting in conditioned residential spaces.</del>	<del>None</del>	<del>EDC Data Gathering Default = 19.2% Default = Table 2-5</del>	<del>56</del>
<del><math>ISR_{res}</math>, In-service rate per incented product for residential use</del>	<del>%</del>	<del>Direct Install: 100% All other program delivery: EDC Data Gathering<sup>4</sup> Default = 92%<sup>5</sup></del>	<del>EDC Data Gathering<sup>4</sup></del>
<del><math>ISR_{non-res}</math>, In-service rate per incented product for non-residential use</del>	<del>%</del>	<del>EDC Data Gathering, Default = 98%</del>	<del>5</del>
<del><math>CF_{res}</math>, Demand Coincidence Factor for residential use</del>	<del>None Proportion</del>	<del>Table 2-20.101</del>	<del>25</del>
<del><math>CF_{non-res}</math>, Demand Coincidence Factor for non-residential use <math>CF_w</math>, Winter coincidence factor</del>	<del>None Proportion</del>	<del>EDC Data Gathering, Default = 0.60121</del>	<del>5</del>
<del>GSS, Cross-sector sales. Share Lumen rating of the incentivized lamps that go to non-residential uses lighting product</del>	<del>% Lumens</del>	<del>EDC Data Gathering, Default = 7.4%</del>	<del>EDC Data Gathering<sup>6</sup></del>
<del><math>Efficacy_{base}</math>, Efficacy of the baseline fixture type for linear fluorescents</del>	<del>Lumens/watt</del>	<del>Table 2-3</del>	<del>8, 9</del>

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**VARIABLE INPUT VALUES**

**Baseline Wattage Values, Linear LEDs**

For delivery methods where the install location is unknown, such as upstream programs linear LEDs, baseline wattage is dependent on lumen output. To determine the  $Watts_{base}$  use the following formula:

$$Watts_{base} = Lumen\ Output \div 45 \frac{lumens}{watt}$$

where *Lumen Output* is the rated light output of the the least-efficient bulb, commercially-available, commonly-installed technology available in lumens.

<sup>4</sup> For EDC Data Gathering, EDCs must use the method established in the DOE Uniform Methods Project, October 2017. (<https://www.nrel.gov/docs/fy17osti/68562.pdf>)

<sup>5</sup> For direct install, giveaway, and energy kit program bulbs, EDCs have the option to use an evaluated ISR when verified through PA program primary research.

For direct installation programs where the removed bulb is known, and the bulb is in working condition, EDCs may use the market Linear LED baseline wattage of the replaced bulb in lieu of the formula.<sup>6</sup> ( $Watts_{base}$ ) is calculated by dividing Lumens<sub>ee</sub> by Efficacy<sub>base</sub> (Table 2-3).

#### Hours of Use and Peak Coincidence Factor Values

In the absence of more current EDC data gathering and analysis, the default values for daily hours of use ( $HOU_{res}$ ) and coincidence factors ( $CF_{res}$ ) are below in Table 2-2. The “all bulbs”  $HOU_{res}$  should be used for programs where it is known that the majority (> 90% or entirety) of the home’s sockets are retrofitted with efficient lighting (e.g., a direct installation program that replaces most of the bulbs in a home). All other programs, including upstream programs, should default to the efficient  $HOU_{res}$  and  $CF_{res}$ . Specific room-based  $HOU_{res}$  and  $CF_{res}$  may be used for programs where the room type of installation is known and recorded, otherwise the whole house or unknown room value should serve as the estimate.

<sup>6</sup> Bulbs that are not installed during the home visit do not qualify for this exemption. This includes bulbs that are left for homeowners to install. In these instances, baseline wattages should be calculated using the provided formula.

**Table 2-3: ~~Bulb and Fixture Hours of Use and Peak Coincidence Factor Values, by Room: Baseline Wattage, Linear Lamps & Fixtures~~**





Room	Efficient HOU <sub>res</sub> Lamp or Fixture	Efficient HOU <sub>res</sub> CFLs	Efficient HOU <sub>res</sub> CFLs	Efficient HOU <sub>res</sub> CFLs
Dining Room	3.2	0.4 48	2.7	0 4 0 8
Exterior Linear Lamps, Fixtures, and Retrofit Kits, 5 ft		4 8 0 7 4	0 2 9 4	0 2 6 5
Hallway	2.4	0.0 85	1.9	0 7 7 6

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Room	Efficient HOU <sub>res</sub> Lamp or Fixture	Efficient CFLs	All Bulbs HOU <sub>res</sub>	All bulbs CFLs
Kitchen Linear Lamps, Fixtures, and Retrofit Kits, 8 ft	4.4	0.3450	0.142	0.142
Living Room	4.1	0.106	3.7	0.998
Other	2.1	0.070	1.7	0.640
Overall Household or unknown room	3.0	0.106	2.5	0.404

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**Interactive Effects Values**

In the absence of EDC data gathering and analysis, the default values for Energy and Demand HVAC Interactive Effects are below. Exterior Fixtures should apply a 0% IE value.

**Hours of Use**

Daily hours of use (HOU) are provided in Table 2-4. Specific room-based HOU may be used for programs where the room-type of installation is known and recorded; otherwise, the overall household or unknown room value should serve as the estimate.

**Table 2-4: EnergyBulb and Demand HVAC Interactive Effects Fixture Hours of Use by EDC<sup>7</sup>Room**

EDCRoom	IE <sub>res</sub> <sup>kWh</sup> <sub>HOU</sub>	IE <sub>res</sub> <sup>kW</sup>
DuquesneBasement	8%1.7	13%
FE (Met-Ed)Bathroom	-8%2.3	13%
BedroomFE (Penelec)	1%0.8	10%
FE (Penn Power)Closet	0%0.6	20%
FE (WPP)Dining Room	-2%0.7	30%
ExteriorPPL	-6%3.9	12%
PECOHallway	1%0.9	23%
Kitchen		3.9
Living Room		3.7
Other		1.7
Overall Household or Unknown Room		2.5

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**Interactive Effects Values**

Default Energy and Demand HVAC Interactive Effects are provided in Table 2-5.

**Table 2-5: Energy and Demand HVAC Interactive Effects by EDC**

EDC	IE <sup>kWh</sup>	IE <sub>s</sub> <sup>kW</sup>	IE <sub>w</sub> <sup>kW</sup>
PECO	-0.0007	0.1193	-0.0581
PPL	-0.0681	0.1046	-0.1480
Duquesne Light	0.0005	0.0957	-0.0291
FE (Met-Ed)	-0.0448	0.1193	-0.1242
FE (Penelec)	-0.0442	0.0736	-0.0872
FE (Penn Power)	-0.0102	0.1311	-0.0555
FE (WPP)	-0.0537	0.1001	-0.1163

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with

<sup>7</sup>HVAC Interactive Effects modeled through REM/Rate models, using EDC specific inputs. Values were weighted to the saturation of HVAC equipment and housing types present in each EDC service territory as reported in the Pennsylvania Statewide Residential End Use and Saturation Study, 2012. PECO values are based on an analysis of PY4 as performed by Navigant.

verification of open variables. The Pennsylvania Evaluation Framework<sup>8</sup> provides specific guidelines and requirements for evaluation procedures.

#### SOURCES

- ~~1) EISA standards require efficacy of 45 lumens/watt.  
[https://www.energy.gov/sites/prod/files/2017/01/f34/gsl-irl-finalrule\\_2016-12-29\\_0.pdf](https://www.energy.gov/sites/prod/files/2017/01/f34/gsl-irl-finalrule_2016-12-29_0.pdf)~~
- 1) [Act 129 Legislation caps measure life at 15 years. Assuming 3 hours of use a day, 15 years equals 16,425 hours. As of January 2024, average rated life hours for ENERGY STAR-qualified LEDs was >21,800 hours. Accessed January 2024. Weblink](#)
- 2) [Early replacement measure life calculated by multiplying one-half \(the assumed proportion of remaining life\) times the product of \(1\) the distribution of incandescent, halogen, and CFL bulbs from the 2023 PA residential baseline study and \(2\) the service lifetimes for incandescent, halogen, and CFL bulbs assumed in DOE Impact Statement for US Department of Energy Appliance and Equipment Standards Rulemakings and Notices. July 25, 2022. Weblink](#)
- 3) [US Department of Energy Appliance and Equipment Standards Rulemakings and Notices. July 25, 2022. Weblink](#)
- 4) [US Department of Energy Appliance and Equipment Standards Rulemakings and Notices. July 8, 2022. Weblink](#)
- 5) [Average "all bulb" probably of operation during PJM summer and winter peak periods calculated using load shapes from Statewide Evaluation Team for Pennsylvania Public Utilities Commission. \(2014, January\). Pennsylvania Statewide Act 129 2014 Commercial & Residential Light Metering Study. Appendix A Residential Load Shapes. Weblink](#)
- 6) [SWE Interactive Effect Calculator.](#)
- 2)7) [Statewide Evaluation Team \(GDS Associates, Inc, Nexant, Research into Action, Apex Analytics LLC, " \) for Pennsylvania Public Utilities Commission. \(2014, January\). 2014 Commercial & Residential Light Metering Study", January 13, 2014. Based on data derived from Tables 1-2 & Pg 4, table 1-3 but exclusive of inefficient bulbs1. Weblink](#)
- ~~3) GDS Simulation Modeling, September-November 2013. PECO values are based on an analysis of PY4 as performed by Navigant.~~
- 8) [The ISR is based on an installation rate "trajectory" and includes savings for all program bulbs that are believed to be installed within three years of purchase as established in the DOE Uniform Methods Project \(UMP\), Chapter 6: Residential Lighting Evaluation Protocol. October 2017. This protocol estimates the three-year ISR based on a researched first year ISR. For the purposes of this TRM, a 79% first-year ISR was used based on intercept surveys conducted in the PECO service territory \(Grainger Lighting Product Web Pages: Weblink1, Weblink2](#)
- 9) [PA 2026 TRM Appendix C. Weblink](#)
- 10) [9.7% of LEDs observed for 2023 Pennsylvania Statewide Act 129 Residential Baseline study were exterior.](#)

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<sup>8</sup> [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/act\\_129\\_statewide\\_evaluator\\_swe.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/act_129_statewide_evaluator_swe.aspx)

- 4) ~~Navigant Consulting, Inc. "Final Annual Report to the Pennsylvania Public Utility Commission. Prepared for PECO. Program Year 5". November, 2014.)~~
- 5) ~~See Pennsylvania TRM Vol. 3, Sec. 3.1.7 Lighting Improvements for Midstream. [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/technical\\_reference\\_manual.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/technical_reference_manual.aspx)~~
- 6) ~~Based on a savings-weighted average of EDC-reported cross-sector sales values for PY6-PY9. [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/electric\\_distribution\\_company\\_act\\_129\\_reporting\\_requirements.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/electric_distribution_company_act_129_reporting_requirements.aspx)~~

### 2.1.2 RESIDENTIAL OCCUPANCY SENSORS

Target Sector	Residential <del>Establishments</del>
Measure Unit	Occupancy Sensor
Measure Life	108 years <sup>Source 3</sup>
Vintage	Retrofit

Savings for residential occupancy sensors inside residential homes ~~or common areas~~ are based on a straightforward algorithm that calculates savings based on the wattage of the bulb(s) or fixture(s) being controlled by the occupancy sensor, the daily run hours before installation, and the daily run hours after installation. This protocol provides a deemed savings value for occupancy sensors sold through an upstream buy-down or retail (time of sale) program (and therefore the controlled wattage is unknown).

#### ELIGIBILITY

#### ELIGIBILITY

This protocol is for the installation of ~~occupancy sensors and/or hard-wired or plug-in occupancy sensors in single-family homes or inside multifamily units. It can also be used to estimate savings from connected (aka “smart”) lighting inside residential homes. Occupancy sensors installed outdoors or in multifamily common areas are not eligible under this protocol.~~

#### ALGORITHMS

#### ALGORITHMS

$$\Delta kWh = \frac{Watts_{controlled}}{1000 \frac{W}{kW}} \times (RH_{old} - RH_{new}) \times \frac{Watts_{controlled}}{1,000} \times (1 + IE_{kWh}) \times (RH_{old} - RH_{new}) \times 365 \frac{days}{yr} \times ISR$$

~~$\Delta kW_{peak} = 0$~~

#### DEFINITION OF TERMS

$$\Delta kW_{summer\ peak} = \frac{Watts_{controlled}}{1,000} \times (1 + IE_{kW,s}) \times \left( \frac{RH_{old} - RH_{new}}{RH_{old}} \right) \times ISR \times CF_s$$

$$\Delta kW_{winter\ peak} = \frac{Watts_{controlled}}{1,000} \times (1 + IE_{kW,w}) \times \left( \frac{RH_{old} - RH_{new}}{RH_{old}} \right) \times ISR \times CF_w$$

#### DEFINITION OF TERMS

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**Table 2-6: Terms, Values, and References for Residential Occupancy Sensors**

Term	Unit	Value	Source
<b>Residential Occupancy Sensors</b>			
<u>Watts<sub>controlled</sub></u> - Wattage of the fixture(s) being controlled by the occupancy sensor	<u>W</u>	EDC Data Gathering Default = 105.5 W	EDC Data Gathering
<u>Watts<sub>controlled</sub></u> , Wattage of the bulb(s) or fixture(s) being controlled by the occupancy sensor	<u>W</u>	EDC Data Gathering, Hard-wired Default: 108W Plug-in Default: 9W	EDC Data Gathering, 7, 8
<u>IE<sub>kWh</sub></u> - HVAC Interactive Effect for lighting energy	<u>None</u>	Table 2-5	9
<u>IE<sub>KW_s</sub></u> - Summer Interactive Demand Factor – applies to residential lighting in conditioned residential spaces.	<u>None</u>	Table 2-5	9
<u>IE<sub>KW_w</sub></u> - Winter Interactive Demand Factor – applies to residential lighting in conditioned residential spaces.	<u>None</u>	Table 2-5	9
<u>RH<sub>old</sub></u> , Daily run hours before installation	<u>Hours</u>	2.5	1
<u>RH<sub>new</sub></u> - Daily run hours after installation	<u>Hours</u>	1.75 (70% of RH <sub>old</sub> )	2

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**DEEMED SAVINGS**

For occupancy sensors for which the controlled wattage is unknown, the deemed savings are 28.9 kWh/year per occupancy sensor. This value is based on the Phase III Market Potential Study for Pennsylvania.<sup>Source 4</sup>

<u>RH<sub>new</sub></u> , Daily run hours after installation	<u>Hours</u>	1.5 (60% of RH <sub>old</sub> )	2
<u>ISR</u> , In-service rate	<u>%</u>	EDC Data Gathering, Upstream Default: 95% Kit Hard-wired Default: 16% Kit Plug-in: EDC Data Gathering Direct Install Default: 100%	5, 6, 7
<u>CF<sub>s</sub></u> , Summer coincidence factor	<u>None</u>	0.101	4
<u>CF<sub>w</sub></u> , Winter coincidence factor	<u>None</u>	0.121	4



## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

- 1) [Statewide Evaluation Team \(GDS Associates, Inc, Nexant, Research into Action, Apex Analytics LLC\),<sup>4\)</sup> for Pennsylvania Public Utilities Commission. \(2014, January\). 2014 Commercial & Residential Light Metering Study<sup>2\)</sup>, January 13, 2014-. Weblink](#)
- 2) [Lighting control savings fractions consistent with current programs offered by National Grid, Northeast Utilities, Long Island Power Authority, NYSEERDA, and Energy Efficient Vermont](#)
- 3) [GDS Associates, Inc. \(2007\). Measure Life Report: Residential and Commercial/Industrial Lighting and HVAC Measures. Prepared for The New England State Program Working Group.](#)
- 4) [Statewide Evaluation Team \(GDS Associates, Inc, Nexant, Research into Action, Apex Analytics LLC\), “2015 Energy Efficiency Potential Study for Pennsylvania”, February 27, 2015. <http://www.puc.pa.gov/pcdocs/1345079.pdf>](#)
- 2) [Weighted average of percentage reduction by hours of use per room \(excluding exterior and other\). Navigant for Consortium for Energy Efficiency. \(2014, January\). Residential Lighting Controls Market Characterization. Pg 19, table 7. Weblink.](#)
- 3) [California Public Utilities Commission Database for Energy Efficient Resources \(DEER\) EUL Support Table for 2020.](#)
- 4) [Average “all bulb” probably of operation during PJM summer and winter peak periods calculated using load shapes from Statewide Evaluation Team for Pennsylvania Public Utilities Commission. \(2014, January\). Pennsylvania Statewide Act 129 2014 Commercial & Residential Light Metering Study. Appendix A Residential Load Shapes. Weblink](#)
- 5) [Maryland EmPOWER Technical Reference Manual Volume 2 – Residential Measures. \(2023, version 11.0\). “Occupancy Sensor – Wall-Mounted”.](#)
- 6) [Weighted average of evaluated PY13 and PY14 outlet gasket ISRs from FirstEnergy kits.](#)
- 7) [Calculated as average number of bulbs controlled times average bulb wattage. Average bulbs controlled is assumed to be the average bulbs per room found in the 2023 PA residential baseline study. Average bulb wattage is calculated by multiplying the distribution of bulb technologies \(LED, CFL, linear fluorescent, incandescent, and halogen\) found in the 2023 PA residential baseline study by the average wattage per technology reported in Buccitelli, N., Elliott, C., Schober, S., and Yamada, M. \(2017, November\). “2015 U.S. Lighting Market Characterization”. Pg 54, table 4.5. Navigant Consulting. Weblink](#)
- 8) [Mean, median, and mode wattage of ENERGY STAR-certified 60w equivalent LEDs. Accessed August 2023. Weblink](#)
- 9) [SWE Interactive Effect Calculator.](#)

### **2.1.3 LED AND ELECTROLUMINESCENT NIGHTLIGHTS**

<b>Target Sector</b>	<b>Residential</b>
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### 2.1.32.1.1 LED AND ELECTROLUMINESCENT NIGHTLIGHTS

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Nightlight
<b>Measure Life</b>	8 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout

Savings from installation of plug-in LED and electroluminescent nightlights are based on a straightforward algorithm that calculates the difference between existing and new wattage and the average daily hours of usage for the lighting unit being replaced. ~~An in-service rate is used to modify the savings based upon the outcome of participant surveys, which will inform the calculation. Demand savings is assumed to be zero.~~ Zero demand savings are assumed for this measure.

#### ELIGIBILITY

This measure documents the energy savings resulting from the installation of an LED or electroluminescent nightlight instead of a standard nightlight. ~~The target sector is primarily residential.~~

#### ALGORITHMS

The general form of the equation for the nightlight energy savings algorithm is:

$$\Delta kWh = \frac{(W_{base} \times HOU_{base} - W_{ee} \times HOU_{ee})}{1000 \frac{W}{kWh}} \times \frac{(W_{base} \times HOU_{base} - W_{ee} \times HOU_{ee})}{1,000}$$

$$\times ISR_{NL} \times 365 \frac{days}{yr}$$

~~$\Delta kW_{peak} = 0$  (assumed)~~

$\Delta kW_{summer\ peak} = 0$

$\Delta kW_{winter\ peak} = 0$

#### DEFINITION OF TERMS

Table 2-7: Terms, Values, and References for LED and Electroluminescent Nightlights

Term	Unit	Value	Sources
$W_{base}$ , Watts per baseline nightlight	Watts	EDC Data Gathering Default = 7	1
$W_{ee}$ , Watts per efficient nightlight	Watts	EDC Data Gathering Default values: LED = 1 Electroluminescent = 0.03	2
$HOU_{base}$ , Daily hours of use for baseline nightlight	$\frac{hours}{day}$	12	1
$HOU_{ee}$ , Daily hours of use for efficient nightlight	$\frac{hours}{day}$	LED = 12 Electroluminescent = 24	3
$ISR_{NL}$ , In-Service Rate per efficient nightlight	None	EDC Data Gathering Default = 0.2014	4

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### DEEMED DEFAULT ENERGY SAVINGS

$$LED \Delta kWh = \frac{(7 \times 12 - 1 \times 12)}{1,000 \frac{W}{kW}} \times \frac{(7 \times 12 - 1 \times 12)}{1,000} \times 0.214 \times 365 \frac{days}{yr} = 5.3.7 kWh$$

$$Electroluminescent \Delta kWh = \frac{(7 \times 12 - 0.03 \times 24)}{1,000 \frac{W}{kW}} \times \frac{(7 \times 12 - 0.03 \times 24)}{1,000} \times 0.214 \times 365 \frac{days}{yr} = 6.14.3 kWh$$

### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

- 1) Southern California Edison Company, (2009, February). "LED, Electroluminescent & Fluorescent Night Lights", Work Paper WPSCRELG0029 Rev. 1, February 2009, pppg. 2–3.
- 2) Limelite Equipment Specification. Personal Communication, Ralph Ruffin, EL Products, 512-357-2776/-ralph@limelite.com.
- 3) Electroluminescent nightlights are assumed to operate continuously.
- 4) Based on ISR rates reported by FirstEnergy for nightlights in kits for PY9. See [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/electric\\_distribution\\_company\\_act\\_129\\_reporting\\_requirements.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/electric_distribution_company_act_129_reporting_requirements.aspx)
- 4) Weighted average of ISRs from surveys of FirstEnergy customers that received nightlights in kits in PY13 and PY14.

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## 2.1.4 HOLIDAY LIGHTS

Target Sector	Residential <del>Applications</del>
Measure Unit	One <del>50-bulb</del> Strand of Holiday lights
Measure Life	10 <del>years</del> <sup>Source 1</sup> <del>years</del> <sup>Source 2</sup>
Vintage	Replace on Burnout

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LED holiday lights reduce light strand energy consumption by up to 90%. Up to 25 strands can be connected end-to-end in terms of residential grade lights. Commercial grade lights require different power adapters and as a result, more strands can be connected end-to-end. There are no demand savings as holiday lights are assumed to operate only at night during the holiday season.

### ELIGIBILITY

#### ELIGIBILITY

This protocol documents the energy savings attributed to the installation of LED holiday lights indoors and outdoors. ~~LED lights must replace traditional~~ instead of incandescent holiday lights.

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### ALGORITHMS

Algorithms yield kWh savings results per package (kWh/yr per package of LED holiday lights).

$$\Delta kWh_{C9} = \frac{[(INC_{C9} - LED_{C9}) \times \#Bulbs \times \#Strands \times HOU]}{1000 \frac{W}{kW}} \frac{[(INC_{C9} - LED_{C9}) \times \#Bulbs \times \#Strands \times HOU]}{1,000}$$

$$\Delta kWh_{C7} = \frac{[(INC_{C7} - LED_{C7}) \times \#Bulbs \times \#Strands \times HOU]}{1000 \frac{W}{kW}} \frac{[(INC_{C7} - LED_{C7}) \times \#Bulbs \times \#Strands \times HOU]}{1,000}$$

$$\Delta kWh_{mini} = \frac{[(INC_{mini} - LED_{mini}) \times \#Bulbs \times \#Strands \times HOU]}{1000 \frac{W}{kW}} \frac{[(INC_{mini} - LED_{mini}) \times \#Bulbs \times \#Strands \times HOU]}{1,000}$$

$$\Delta kW_{summer\ peak} = 0$$

$$\Delta kW_{winter\ peak} = 0$$

### Key assumptions

- 1) All estimated values reflect the use of residential ~~(50ct. per strand)~~ LED bulb holiday lighting.
- 2) Secondary impacts for heating and cooling were not evaluated.
- 3) It is assumed that 50% of rebated lamps are of the "mini" variety, 25% are of the C7 variety, and 25% are of the C9 variety. If the lamp type is known or fixed by program design, then the savings can be calculated as described by the algorithms above. Otherwise, the savings for the mini, C7, and C9 varieties should be weighted by 0.5, 0.25 and 0.25, respectively, as in the algorithm below.

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$$\Delta kWh_{Default} = [\%_{C9} \times \Delta kWh/yr_{C9}] + [\%_{C7} \times \Delta kWh/yr_{C7}] + [\%_{mini} \times \Delta kWh/yr_{mini}]$$

**DEFINITION OF TERMS**

**Table 2-8: Terms, Values, and References for Holiday Lights**

Parameter	Unit	Value	Source
LED <sub>mini</sub> , Wattage of LED mini bulbs	Watts/Bulb	0.08	1
INC <sub>mini</sub> , Wattage of incandescent mini bulbs	Watts/Bulb	0.4835	1
LED <sub>C7</sub> , Wattage of LED C7 bulbs	Watts/Bulb	0.4808	1
INC <sub>C7</sub> , Wattage of incandescent C7 bulbs	Watts/Bulb	6.95.25	1
LED <sub>C9</sub> , Wattage of LED C9 bulbs	Watts/Bulb	2.0.28	1
INC <sub>C9</sub> , Wattage of incandescent C9 bulbs	Watts/Bulb	7.0	1
% <sub>Mini</sub> , Percentage of holiday lights that are "mini"	%	50%	42
% <sub>C7</sub> , Percentage of holiday lights that are "C7"	%	25%	42
% <sub>C9</sub> , Percentage of holiday lights that are "C9"	%	25%	42
# <sub>Bulbs</sub> , Number of bulbs per strand	Bulbs/strand	EDC Data Gathering Default: 50 per strand Mini: 100 Default C7: 25 Default C9: 25	31
# <sub>Strands</sub> , Number of strands of lights per package	strands/Strands/package	EDC Data Gathering Default: 1 strand	31
HOU, Annual hours of operation	Hours/yr	150	42

**DEEMED DEFAULT SAVINGS**

The ~~deemed default~~ savings for installation of LED C9, C7, and mini lights is ~~37.525.2 kWh, 4119.4 kWh, and 34.1 kWh, respectively.~~ The weighted average savings are ~~2413.2 kWh per strand.~~ ~~There are no demand savings as holiday lights only operate at night. Since the lights do not operate in the summer, the coincidence factor for this measure is 0.0.~~

**EVALUATION PROTOCOL**

The most appropriate evaluation protocol for this measure is verification of installation coupled with assignment of stipulated energy savings. As these lights are used on a seasonal basis, verification

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must occur in the winter holiday season. Given the relatively small amount of impact evaluation risk that this measure represents, and given that the savings hinge as heavily on the actual wattage of the supplanted lights than the usage of the efficient LED lights, customer interviews should be considered as an appropriate channel for verification.

#### **SOURCES**

- 1) ~~The DSMore Sample of 180 holiday lights gathered from HomeDepot.com and Walmart.com. Accessed March 2024.~~
- 4)2) Michigan Database of Energy Efficiency Measures: ~~Based on spreadsheet calculations using collected data Database. Accessed January 2024. Weblink,~~
- 2) ~~<http://www.energyideas.org/documents/factsheets/HolidayLighting.pdf>~~
- 3) ~~Typical values of lights per strand and strands per package at Home Depot and other stores.~~

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## 2.2 HVAC

### 2.2.1 HIGH EFFICIENCY EQUIPMENT: ASHP, CAC, GSHP, PTAC, PTHP

Target Sector	Residential <del>Establishments</del>
Measure Unit	Central AC, ASHP, GSHP, PTAC or PTHP Unit
Measure Life	15 <sup>Source 1</sup>
Vintage	Early Replacement, Replace on Burnout, New Construction

This measure defines the methods for determining energy impact savings from installation of residential high-efficiency cooling and heating equipment. Input data to savings algorithms are based both on fixed assumptions and data supplied from the high-efficiency equipment AEPS application form or EDC data gathering.

~~The algorithms applicable for this program measure the energy savings directly related to the more efficient hardware installation.~~

Cooling savings may also be claimed under this measure for quality installation of properly sized new equipment.

Larger commercial air conditioning and heat pump applications are ~~dealt with~~ addressed in Section 3 of Volume 3: Commercial and Industrial Measures of this Manual, including GSHP systems over  $65 \frac{kBTU}{hr}$ .

#### ELIGIBILITY

This measure requires the purchase of a high-efficiency Central Air Conditioner (CAC), Air Source Heat Pump (ASHP), Ground Source Heat Pump (GSHP), Packaged Terminal Air Conditioner (PTAC) or Packaged Terminal Heat Pump (PTHP). Cooling and heating savings claimed from proper sizing requires Manual J calculations, following of ENERGY STAR HVAC Quality Installation procedures, or similar calculations. Residential ~~establishments~~ buildings with properly sized baseline equipment are excluded from claiming savings from proper sizing.

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**ALGORITHMS**

This algorithm is used for the installation of ~~new high efficiency air conditioners or heat pumps-ASHP and CAC measures:~~

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat} + \Delta kWh_{PSF}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool}}{SEER_{base}} - \frac{1}{SEER_{ee}} \right) \times EFLH_{cool}$$

$$\Delta kWh_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat}}{HSPF_{base}} - \frac{1}{HSPF_{ee}} \right) \times EFLH_{heat}$$

$$\Delta kWh_{PSF} = \frac{CAPY_{cool}}{SEER_{ee}} \times PSF \times EFLH_{cool} + \frac{CAPY_{heat}}{HSPF_{ee}} \times PSF \times EFLH_{heat}$$
  

$$\Delta kW_{summer\ peak} = \Delta kW_{cool} + \Delta kW_{PSF\ cool}$$

$$\Delta kW_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool}}{EER2_{base}} - \frac{1}{EER2_{ee}} \right) \times CF_{summer}$$

$$\Delta kW_{PSF\ cool} = \frac{CAPY_{cool}}{EER2_{ee}} \times PSF \times CF_{summer}$$
  

$$\Delta kW_{winter\ peak} = \Delta kW_{heat} + \Delta kW_{PSF\ heat}$$

$$\Delta kW_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat}}{COP_{base}} - \frac{1}{COP_{ee}} \right) \times \frac{1}{3.412 \frac{BTU}{Wh}} \times CF_{winter}$$

$$\Delta kW_{PSF\ heat} = \frac{CAPY_{heat}}{COP_{ee} \times 3.412 \frac{BTU}{Wh}} \times PSF \times CF_{winter}$$

This algorithm is used for the installation of GSHP, PTAC and PTHP measures:

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat} + \Delta kWh_{PSF}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool}}{SEER_{base}} - \frac{1}{SEER_{ee}} \right) \times EFLH_{cool}$$

$$\Delta kWh_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat}}{HSPF_{base}} - \frac{1}{HSPF_{ee}} \right) \times EFLH_{heat}$$

$$\Delta kWh_{PSF} = \frac{CAPY_{cool}}{SEER_{ee}} \times PSF \times EFLH_{cool} + \frac{CAPY_{heat}}{HSPF_{ee}} \times PSF \times EFLH_{heat}$$
  

$$\Delta kW = \Delta kW_{cool} + \Delta kW_{PSF}$$

$$\Delta kW_{summer\ peak} = \Delta kW_{cool} + \Delta kW_{PSF\ cool}$$

$$\Delta kW_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool}}{EER_{base}} - \frac{1}{EER_{ee}} \right) \times CF \left( \frac{OF_{cool}}{EER_{base}} - \frac{1}{EER_{ee}} \right) \times CF_{summer}$$

$$\Delta kW_{PSF\ cool} = \frac{CAPY_{cool}}{EER_{ee}} \times PSF \times CF_{summer}$$

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$$\frac{\Delta kW_{winter\ peak}}{\Delta kW_{heat}} = \Delta kW_{heat} + \Delta kW_{PSF\ heat}$$

$$\frac{\Delta kW_{heat}}{\Delta kW_{heat}} = CAPY_{heat} \times \left( \frac{OF_{heat}}{COP_{base}} - \frac{1}{COP_{ee}} \right) \times \frac{1}{3.412 \frac{BTU}{Wh}} \times CF_{winter}$$

$$\frac{\Delta kW_{PSF\ heat}}{\Delta kW_{heat}} = \frac{CAPY_{heat}}{COP_{ee} \times 3.412 \frac{BTU}{Wh}} \times PSF \times CF_{winter}$$

**Baseline: Room Air Conditioner(s)**

EDCs may collect information about the total capacity of the (kBtu/hr) of existing RACs ( $CAPY_{RAC}$ ) in use in the home to determine the replaced capacity. An oversizing factor is calculated from the ratio of baseline to qualifying capacity:

$$OF_{cool} = \frac{\sum CAPY_{RAC}}{CAPY_{cool}}$$

**Baseline: Spaceheater(s), Electric Baseboards**

EDCs may collect information about the capacity of the existing space heaters, electric furnaces, or electric baseboards. Capacity is determined using the total wattage of electric heat in use, where  $OF_{heat}$  is the ratio of the existing electric capacity to the capacity of the new equipment:

$$OF_{heat} = \frac{\sum kW_{spaceheat} \times 3.412 \frac{BTU}{Wh}}{CAPY_{Heat}}$$

**Qualifying: Ground Source Heat Pump**

GSHP efficiencies are typically calculated differently than air-source units, baseline and qualifying unit efficiencies should be converted as follows:

$$SEER = EER_g \times GSHPDF \times GSER$$

$$EER = EER_g \times GSPK$$

$$HSPF = COP_g \times GSHPDF \times 3.412 \frac{BTU}{Wh}$$

**Qualifying: Package Terminal Heat Pumps, Package Terminal Air Conditioners**

$$SEER = EER$$

$$HSPF = COP \times 3.412 \frac{BTU}{Wh}$$

**DEFINITION OF TERMS**

$$HSPF = COP_g \times 3.412 \frac{BTU}{Wh} \times GSOP$$

$$COP = COP_g$$

**Qualifying: Package Terminal Heat Pumps, Package Terminal Air Conditioners**

$$SEER = EER$$

$$HSPF = COP \times 3.412 \frac{BTU}{Wh}$$

**DEFINITION OF TERMS**

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**Table 2-9: Terms, Values, and References for High Efficiency Equipment: ASHP, CAC, GSHP, PTAC, PTHP**

Term	Unit	Value	Sources
$CAPY_{cool}$ , The cooling capacity of the equipment being installed <sup>9</sup>	<i>kBTU/hr</i>	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CAPY_{heat}$ , The heating capacity of the heat pump being installed <sup>10</sup> (Auxiliary electric resistance heat is not included)	<i>kBTU/hr</i>	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CAPY_{RAC}$ , The cooling capacity of the room AC for the RAC cooling baseline	<i>kBTU/hr</i>	EDC Data Gathering	EDC Data Gathering
$kW_{spaceheat}$ , The heating capacity of the space heaters in kilowatts.	<i>kW</i>	EDC Data Gathering	EDC Data Gathering
$SEER2_{base}$ , $SEER_{base}$ , Seasonal Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering, Default: see Table 2-10	2; EDC Data Gathering
		Default: see Table 2-10	2
$SEER2_{ee}$ , $SEER_{ee}$ , Seasonal Energy Efficiency Ratio of the qualifying unit being installed <sup>11</sup>	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$EER2_{base}$ , $EER_{base}$ , Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering, Default: see Table 2-10	3; EDC Data Gathering
		Default: see Table 2-10	2
$EER2_{ee}$ , $EER_{ee}$ , Energy Efficiency Ratio of the unit being installed <sup>12</sup>	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: $-0.0228 \times SEER^2 + 1.1522 \times SEER$	4; EDC Data Gathering; AEPS Application
		Default: $EER_{ee} = -0.02 \times SEER^2 + 1.12 \times SEER$	3.4
$EER_g$ , Energy Efficiency Ratio of a GSHP, this is measured differently than EER of an air source heat pump and must be converted	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	EDC Data Gathering
$HSPF2_{base}$ , $HSPF_{base}$ , Heating Seasonal Performance Factor of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering, Default: see Table 2-8	2; EDC Data Gathering
		Default: see Table 2-10	2
$HSPF2_{ee}$ , $HSPF_{ee}$ , Heating Seasonal Performance Factor of the unit being installed	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$PSF$ , Proper Sizing Factor or the assumed savings due to proper sizing and proper installation	<i>Proportion</i>	Not properly sized or properly sized baseline equipment: 0 Properly sized: 0.05	105

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<sup>9</sup> This data is obtained from the AEPS Application Form or EDC's data gathering based on the model number.

<sup>10</sup> Ibid. This refers to the capacity of the heat pump and not any auxiliary electric resistance heat.

<sup>11</sup> Ibid.

<sup>12</sup> Ibid.

Term	Unit	Value	Sources
<u><math>COP_{base}</math></u> , Coefficient of Performance of the baseline unit. This is a measure of the efficiency of a heat pump	<i>Proportion</i>	<u>EDC Data Gathering</u>	<u>EDC Data Gathering</u>
		<u>Default: see Table 2-10</u>	<u>2</u>
$COP_{ee}$ , Coefficient of Performance of the unit being installed. This is a measure of the efficiency of a heat pump	<i>Proportion</i>	EDC Data Gathering	AEPS Application; EDC Data Gathering
<u><math>OF_{cool}</math></u> , Oversize factor	<i>None</i>	<u>EDC Data Gathering;</u> <u>Default see Table 2-9</u>	<u>5EDC Data Gathering</u>
		<u>Default: see Table 2-12</u>	<u>6</u>
<u><math>OF_{heat}</math></u> , Oversize factor	<i>None</i>	<u>EDC Data Gathering;</u> <u>Default see Table 2-9</u>	<u>6EDC Data Gathering</u>
		<u>Default: see Table 2-12</u>	<u>7</u>
<u><math>GSER</math></u> , Factor used to determine convert $EER_q$ to the SEER equivalent HSPF of a GSHP based on its $EER_q$ an air-source unit to enable comparisons to the baseline unit	$\frac{BTU}{W \cdot h}$	<u>1.02</u> See Table 2-13	<u>78</u>
<u><math>GSPKGSOP</math></u> , Factor to convert $EER_q$ $COP_q$ to the equivalent $EERCOP$ of an air conditioner-source unit to enable comparisons to the baseline unit	<i>Proportion</i>	<u>0.8416</u> See Table 2-13	<u>78</u>
<u><math>GSHPDF</math></u> , Ground-Source-Heat-Pump-De-rate-Factor	<i>Proportion</i>	<u>0.885</u>	<u>8</u>
<u><math>EFLH_{cool}</math></u> , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See $EFLH_{cool}$ in Vol. 1, App. A	<u>9</u>
<u><math>EFLH_{heat}</math></u> , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See $EFLH_{heat}$ in Vol. 1, App. A	<u>9</u>
<u><math>CF_{summer}</math></u> , Demand Coincidence Factor during the summer months	<i>Proportion</i>	See $CF$ in Vol. 1, App. A	<u>9</u>
<u><math>CF_{winter}</math></u> , Demand Coincidence Factor during the winter months	<i>Proportion</i>	See $CF$ in Vol. 1, App. A	<u>9</u>

Note: Where appropriate, nameplate data collected for usage in savings calculations (i.e., SEER, EER, HSPF) should be converted to new efficiency metrics (i.e., SEER2, EER2, HSPF2) using conversion equations laid out in Vol. 1 App. A.

Table 2-10: Default Baseline Equipment Efficiency for High Efficiency Equipment

Baseline Equip.	Early Replacement				Replace on Burnout / New Construction			
	<u><math>SEER2_{base}</math></u>	<u><math>EER2_{base}</math></u>	<u><math>HSPF2_{base}</math></u>	<u><math>COP_{base}</math></u>	<u><math>SEER2_{base}</math></u>	<u><math>EER2_{base}</math></u>	<u><math>HSPF2_{base}</math></u>	<u><math>COP_{base}</math></u>

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Equipment	Early Replacement				Replace on Burnout / New Construction			
	SEER <sub>base</sub>	EER <sub>base</sub>	HSPF <sub>base</sub>	COP <sub>base</sub>	SEER <sub>base</sub>	EER <sub>base</sub>	HSPF <sub>base</sub>	COP <sub>base</sub>
ASHP (Split systems)					14.3	11.8 <sup>b</sup>	7.5	2.6
ASHP (Single-Package)	14.1 <sup>a</sup>	11.7 <sup>b</sup>	7.2	2.5 <sup>c</sup>	13.4	11.2 <sup>b</sup>	6.7	2.3
CAC (Split systems and Single-package)	13.2	11.1 <sup>b</sup>	=	=	13.4	11.2 <sup>b</sup>	=	=
ASHP	13.5	11.4	8.2	14	12.0	8.2		
CAC	12.1	10.6 <sup>a</sup>	–	13	11.3	8.2		
GSHP	15.0	16.6 <sup>a</sup>	10.9	14	12.0	8.2		
Elec. Baseboard		3.4424 <sup>d</sup>	–1.0					
Elec. Furnace <sup>13</sup>		3.2412 <sup>d</sup>	–0.95					
Space Heaters		3.4424 <sup>d</sup>	–1.0					
PTAC <sup>14,15,16</sup> / GSHP	EER <sub>base</sub> 10.9 (0.213 × CAPY <sub>cool</sub> )	EER <sub>base</sub> 14.0 (0.3 × CAPY <sub>cool</sub> )	–10.8%	18.7 <sup>h</sup>	18.0	10.2 <sup>i</sup>	3.7	
	Water-to-air, ground water	18.0 <sup>j</sup>						
Brine-to-air, ground loop				14.5 <sup>h</sup>	14.1	9.5 <sup>i</sup>	3.2	
	Water-to-water, ground water			3.7 <sup>f</sup>	PTHP 15.16, 17.2 <sup>g</sup>	EER <sub>base</sub> 10.8 (0.213 × CAPY <sub>cool</sub> )	3.412 <sup>h</sup> W/h (2.9 × 0.026 × CAPY <sub>cool</sub> )	EER <sub>base</sub> 14.0 (0.3 × CAPY <sub>cool</sub> )
Brine-to-water, ground loop								
				11.6 <sup>h</sup>	12.1	7.6 <sup>i</sup>	2.5	

<sup>13</sup> Using the relation  $HSPF = COP \times 3.412$ , where  $HSPF = 3.412$  for electric resistance heating. Electric furnace efficiency typically varies from 0.95 to 1.00, therefore a COP of 0.95 equates to an HSPF of 3.241.

<sup>14</sup> If the unit's capacity is less than 7 kBtu/hr, use 7 kBtu/hr in the calculation. If the unit's capacity is greater than 15 kBtu/hr, use 15 kBtu/hr in the calculation.

<sup>15</sup> "Early Replacement" is for nonstandard size packaged terminal air conditioners and heat pumps with existing sleeves having an external wall opening of less than 16 in. high or less than 42 in. wide and having a cross-sectional area less than 670 sq. in. Shall be factory labeled as follows: "Manufactured for nonstandard size applications only; not to be installed in new construction projects."

<sup>16</sup> "New Construction" is intended for applications with new, standard size exterior wall openings.

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Additional Information	PTAC <sup>i</sup>	$13.8 - (0.3 \times \text{CAPY}_{\text{cool}})$	=	=	$13.8 - (0.3 \times \text{CAPY}_{\text{cool}})$	=	=
	PTHP <sup>i</sup>	$14.0 - (0.3 \times \text{CAPY}_{\text{cool}})$	$3.412 \times (3.7 - 0.052 \times \text{CAPY}_{\text{cool}})$	$3.7 - (0.052 \times \text{CAPY}_{\text{cool}})$	$14.0 - (0.3 \times \text{CAPY}_{\text{cool}})$	$3.412 \times (3.7 - 0.052 \times \text{CAPY}_{\text{cool}})$	$3.7 - (0.052 \times \text{CAPY}_{\text{cool}})$

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<sup>a</sup> Disaggregated ASHP values from the 2023 Residential Baseline study  
<sup>b</sup> Value is calculated based on conversion equations laid out in Vol 1, Appendix A and  $\text{EER} = -0.02 \times \text{SEER}^2 + 1.12 \times \text{SEER}$   
<sup>c</sup> Value is calculated based on conversion equations laid out in Vol 1, Appendix A and  $\text{COP} = \text{HSPF} / 3.412$   
<sup>d</sup> Equipment COPs vary between 0.95 and 1.00. Using the formula  $\text{HSPF} = \text{COP} \times 3.412$ , a COP of 0.95 therefore equates to an HSPF of 3.241.  
<sup>e</sup> Value calculated using the average of the GSER values listed in Table 2-11 and the following formula:  $\text{SEER} = \text{EER} \times \text{GSER}$   
<sup>f</sup> Value is from 2023 Pennsylvania Statewide Act 129 Residential Baseline Study, but capped to current federal efficiency  
<sup>g</sup> Value calculated using the average of the GSOP values listed in Table 2-11 and the following formula:  $\text{HSPF} = \text{COP} \times 3.412 \times \text{GSOP}$   
<sup>h</sup> Value calculated using the corresponding GSER value listed in Table 2-11 and the following formula:  $\text{SEER} = \text{EER} \times \text{GSER}$   
<sup>i</sup> Value calculated using the corresponding GSOP value listed in Table 2-11 and the following formula:  $\text{HSPF} = \text{COP} \times 3.412 \times \text{GSOP}$   
<sup>j</sup> If the unit's capacity is less than 7 kBtu/hr, use 7 kBtu/hr in the calculation. If the unit's capacity is greater than 15 kBtu/h, use 15 kBtu/hr in the calculation.

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**Table 2-11: Proper Size Factors for High Efficiency Equipment**

Proper Size Factor	ASHP	CAC	PTAC	PTHP	GSHP
$\Delta \text{KW}_{\text{PSF cool}}$	0	0.05	0.05	0	0
$\Delta \text{KW}_{\text{PSF heat}}$	0.05	0	0	0.05	0.05

Note: The implicit assumption is that ASHP, GSHP and PTHP have been sized to meet the heating load of the residential establishment and standalone AC systems have been sized to meet the cooling load

**Table 2-12: Default Oversize Factors for High Efficiency Equipment**

Qualifying	Oversize Factor	Existing						
		ASHP	CAC	Electric Baseboard	Electric Furnace	GSHP	RAC	Space Heaters
CAC, PTAC	$OF_{cool}$	1	1	0	0	1	1	0
HP	$OF_{heat}$	1	1	1	1	1	0	0.6
	$OF_{cool}$	1	1	0	0	1	1	0

**Table 2-13: Conversion factors to derive Air-source equivalent metrics of a Ground source heat pump**

GSHP Type	GSER	GSOP
<u>Water-to-Air: Ground water</u>	<u>1.04</u>	<u>0.81</u>
<u>Brine-to-Air: Ground loop</u>	<u>1.03</u>	<u>0.87</u>
<u>Water-to-Water: Ground water</u>	<u>0.93</u>	<u>0.84</u>
<u>Brine-to-Water: Ground loop</u>	<u>0.96</u>	<u>0.89</u>

## EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with assignment of stipulated energy savings.

## SOURCES

- 1) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx> Accessed December 2018
- 1) For California Electronic Technical Reference Manual. "SEER Rated AC and HP HVAC Equipment, Residential". Accessed February 2024. Weblink
- 2) For early replacement ASHP/CAC: NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Sec 8.1.4 Table 87 and Sec 8.2.1 Table 97 and 98. Baseline findings are capped to current Federal Standards. Weblink  
For new construction ASHP/CAC: Federal Code of Regulations 10 CFR 430.32(c). Weblink  
For early replacement GSHP: existing systems were assumed to be two-thirds through an assumed 15 year equipment life. Therefore, the minimum required efficiency at the date of installation for an existing GSHP system is estimated to have been set by IECC 2015 requirements. The values in the table represent the minimum efficiency values from IECC 2015. Weblink  
For New Construction GSHP: IECC 2021 - Weblink Table 14  
All PTAC and PTHP: Standard sizing minimums, Federal Code of Regulations 10 CFR 431.97(c): Weblink  
As per IECC Residential code (Section R403.7), the requirements for all mechanical systems are stipulated to be federal minimums. Since there are no federal standards for Residential GSHP/PTAC/PTHPs, the C&I standards acts as a proxy.
- 2) Early Replacement ASHP, CAC: Pennsylvania Act 129 2018 Residential Baseline Study ([http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf)) For Early Replacement GSHP: the values represent the minimum efficiency values for GSHP in BEopt v2.8.0. For Replace on Burnout/New Construction ASHP, CAC, GSHP: Federal Code of Regulations 10 CFR 430.

- <https://www.gpo.gov/fdsys/pkg/CFR-2017-title10-vol3/pdf/CFR-2017-title10-vol3-sec430-32.pdf>. For PTAC and PTHP: standards are based on requirements of ASHRAE 90.1-2016, Energy Standard for Buildings Except Low-Rise Residential Buildings, Table 6.8.1-4, <https://www.ashrae.org/technical-resources/standards-and-guidelines/read-only-versions-of-ashrae-standards>.
- 3) Average EER for SEER 13 units as calculated by  $EER = -0.02 \times SEER^2 + 1.12 \times SEER$  based on Wassmer, M., (2003), "A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations" as cited in U.S. DOE Building America House Simulation Protocol, Revised 2010. <https://www.nrel.gov/docs/fy11osti/49246.pdf> Weblink
  - 4) "Methodology for Calculating Cooling and Heating Energy Input-Ratio (EIR) from the Rated Seasonal Performance Efficiency (SEER OR HSPF)" (Kim, Baltazar, Haberl). April 2013 Accessed December 2018. <http://oaktrust.library.tamu.edu/bitstream/handle/1969.1/152118/ESL-TR-13-04-01.pdf> Weblink
  - 5) [Northeast Energy Efficiency Partnerships, Inc., "Strategies to Increase Residential HVAC Efficiency in the Northeast", \(February 2006\): Appendix C Benefits of HVAC Contractor Training: Field Research Results 03-STAC-01, p. 4.](#)
  - 6) Based on REM/Rate modeling using models from the PA 2012 Potential Study. EFLH calculated from kWh consumption for cooling and heating. Models assume 50% over-sizing of air conditioners<sup>17</sup> and 40% oversizing of heat pumps.<sup>18</sup> and 40% oversizing of heat pumps. Thus assuming for most baseline oversize factors to be unitary. Neme, Proctor, Nadal, "National Energy Savings Potential From Addressing Residential HVAC Installation Problems". ACEEE, February 1, 1999. Weblink Confirmed also by *Central Air Conditioning in Wisconsin, a compilation of recent field research*. Energy Center of Wisconsin. May 2008, emended December 15, 2010. Weblink ACCA, "Verifying ACCA Manual S Procedures," Weblink
  - 7) Assumptions used to calculate a default value for de facto heating system OF: Four (4) 1500W portable electric space heaters in use in the home with capacity of  $4 \times 1.5kW \times 3412 \frac{BTU}{kWh} = 20,472 BTU$ , replaced by DHP with combined heating capacity of 36kBTU.  $OF = \frac{20,472}{36,000} \approx 0.6$
  - 7) VEIC estimate. Extrapolation of manufacturer data.
  - 8) McQuay Application Guide 31-008, Geothermal Heat Pump Design Manual, 2002. Engineering Estimate – See System Performance of Ground Source Heat Pumps
  - 8) Factors are derived from the conversion algorithms depicted in the Heat Pump – Water-to-air Ground Source (GSHP) Measure of the Version 11 of the NY TRM Weblink Substituting for defaults where applicable and borrowing current market data from the AHRI Database Weblink.
  - 9) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. <https://www.ecobee.com/donateyourdata/>
  - 10) [\(Weblink\) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals \(Northeast Energy Efficiency Partnerships, Inc., "Strategies to Increase Residential HVAC Efficiency in the Northeast", \(February 2006\): Appendix C Benefits of HVAC Contractor Training: Field Research Results 03-STAC-01, p. 4. \(2020\) \(Weblink\)](#)

<sup>17</sup> Neme, Proctor, Nadal, "National Energy Savings Potential From Addressing Residential HVAC Installation Problems". ACEEE, February 1, 1999.

<https://www.proctoreng.com/dnid/NationalEnergySavingsPotentialfromAddressingResidentialHVACInstallationProblems.pdf> Confirmed also by *Central Air Conditioning in Wisconsin, a compilation of recent field research*. Energy Center of Wisconsin. May 2008, emended December 15, 2010. <https://www.seventhwave.org/publications/central-air-conditioning-wisconsin-Compilation-recent-field-research>

<sup>18</sup> ACCA, "Verifying ACCA Manual S Procedures," <http://www.acca.org/wp-content/uploads/2014/01/Manual-S-Brochure-Final.pdf>

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**2.2.2 HIGH EFFICIENCY EQUIPMENT: DUCTLESS HEAT PUMPS WITH FOR MIDSTREAM DELIVERY OPTION: ASHP, CAC, PTAC, PTHP**

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	CAC, ASHP, PTAC or PTHP Unit
<b>Measure Life</b>	15 <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout, New Construction
<b>Measure Unit</b>	Ductless Heat Pump Unit
<b>Measure Life</b>	15 years <sup>Source-1</sup>
<b>Vintage</b>	Early Replacement, Replace on Burnout, New Construction

This protocol defines the methods for determining the annual electric energy and peak demand savings from installation of residential high-efficiency cooling and heating equipment that is sold to trade allies and customers through commercial channels such as HVAC distributors, dealers, supply houses, and direct relationships with manufacturers. This complements other delivery channels (such as downstream rebates to trade allies and customers) by providing incentives to encourage distributors to stock, promote, and sell more-efficient HVAC equipment. Input data to savings algorithms are based both on stipulated code minimum baselines and operating assumption in combination with actual equipment properties recorded by the participating distributors. EDCs, their implementation CSPs, and participating distributors are expected to collect AHRI reference numbers and use the AHRI rated capacity and efficiency metrics to calculate savings. The algorithms for this measure path assume a 1:1 installation of a high-efficiency unit in lieu of a code minimum piece of HVAC equipment with the same capacity. Larger commercial air conditioning and heat pump applications are dealt with in Section 3 of Volume 3: Commercial and Industrial Measures of the 2026 Technical Reference Manual.

**ELIGIBILITY**

This protocol requires the purchase of a high-efficiency Central Air Conditioner (CAC), Air Source Heat Pump (ASHP), Cold Climate Heat Pump (ccHP), Packaged Terminal Air Conditioner (PTAC) or Packaged Terminal Heat Pump (PTHP). To be eligible under this protocol, the qualifying equipment must be purchased through a commercial channel (such as an HVAC contractor or distributor) for installation in a residential setting. The distributor will need to collect information on the installation address for verification purposes.

For the purposes of the midstream protocol, the minimum efficiency levels for each eligible unit type are defined by ENERGY STAR version 6.1 requirements as follows: <sup>Source 2</sup>

- CAC: greater than or equal to 15.2 SEER2
- ASHP: Greater than or equal to 15.2 SEER2 or 7.8 HSPF2 (Split systems)/7.2 HSPF2 (Single package systems)
- ccHP: Greater than or equal to 15.2 SEER2 or 8.5 HSPF2 (Non-ducted split systems)/8.1 HSPF2 (All other systems)
- PTAC:  $EER \geq 14.0 - (0.3 \times CAPY_{cool})$
- PTHP:  $EER \geq 14.0 - (0.3 \times CAPY_{cool})$  or  $HSPF = 3.412 \times (3.7 - 0.052 \times CAPY_{cool})$

Heat pump equipment (ASHP and PTHP) must meet at least one of the cooling or heating minimum efficiencies. This will allow EDCs to incentivize equipment which are engineered for heating performance over cooling efficiency.

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**ALGORITHMS**

This algorithm is used for the installation of ASHP and CAC measures:

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool}}{SEER2_{base}} - \frac{1}{SEER2_{ee}} \right) \times EFLH_{cool}$$

$$\Delta kWh_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat}}{HSPF2_{base}} - \frac{1}{HSPF2_{ee}} \right) \times EFLH_{heat}$$

$$\Delta kW_{summer\ peak} = CAPY_{cool} \times \left( \frac{OF_{cool}}{EER2_{base}} - \frac{1}{EER2_{ee}} \right) \times CF_{summer}$$

$$\Delta kW_{winter\ peak} = CAPY_{heat} \times \left( \frac{OF_{cool}}{COP_{base}} - \frac{1}{COP_{ee}} \right) \times \frac{1}{3.412 \frac{BTU}{Wh}} \times CF_{winter}$$

This algorithm is used for the installation of PTAC and PTHP measures:

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool}}{SEER_{base}} - \frac{1}{SEER_{ee}} \right) \times EFLH_{cool}$$

$$\Delta kWh_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat}}{HSPF_{base}} - \frac{1}{HSPF_{ee}} \right) \times EFLH_{heat}$$

$$\Delta kW_{summer\ peak} = CAPY_{cool} \times \left( \frac{OF_{cool}}{EER_{base}} - \frac{1}{EER_{ee}} \right) \times CF_{summer}$$

$$\Delta kW_{winter\ peak} = CAPY_{heat} \times \left( \frac{OF_{cool}}{COP_{base}} - \frac{1}{COP_{ee}} \right) \times \frac{1}{3.412 \frac{BTU}{Wh}} \times CF_{winter}$$

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**Qualifying: Package Terminal Heat Pumps, Package Terminal Air Conditioners**

$$SEER = EER$$

$$HSPF = COP \times 3.412 \frac{BTU}{Wh}$$

**DEFINITION OF TERMS**

Table 2-14: Terms, Values, and References for High Efficiency Equipment: ASHP, ccHP, CAC, PTAC, PTHP

Term	Unit	Value	Sources
CAPY <sub>cool</sub> , The cooling capacity of the equipment being installed	kBTU/hr	Rated Value from AHRI Certificate • CAC, ASHP, ccHP: Cooling Capacity at 95 degrees (F) • PTAC, PTHP: Cooling Capacity	3. EDC Data Gathering

<u>Term</u>	<u>Unit</u>	<u>Value</u>	<u>Sources</u>
		at 230V if dual voltage	
<u>CAPY<sub>heat</sub></u> , The heating capacity of the heat pump being installed (Auxiliary electric heat resistance not included)	<i>kBTU/hr</i>	Rated Value from AHRI Certificate • <u>ASHP, ccHP</u> : Heating Capacity at 47 degrees (F) • <u>PTHP</u> : Heating Capacity at 230V if dual voltage	3, EDC Data Gathering
<u>SEER<sub>2base</sub></u> , <u>SEER<sub>base</sub></u> Seasonal Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	See Table 2-10	4
<u>SEER<sub>2ee</sub></u> , <u>SEER<sub>ee</sub></u> Seasonal Energy Efficiency Ratio of the qualifying unit being installed	$\frac{BTU}{W \cdot h}$	Rated Value from AHRI Certificate	3, EDC Data Gathering
<u>EER<sub>2base</sub></u> , <u>EER<sub>base</sub></u> Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	See Table 2-10	5
<u>EER<sub>2ee</sub></u> , <u>EER<sub>ee</sub></u> Energy Efficiency Ratio of the unit being installed	$\frac{BTU}{W \cdot h}$	Rated Value from AHRI Certificate. At • <u>CAC, ASHP, ccHP</u> : EER at 95 degrees (F) • <u>PTAC, PTHP</u> : EER at 230V if dual voltage	3; EDC Data Gathering
<u>HSPF<sub>2base</sub></u> , <u>HSPF<sub>base</sub></u> Heating Seasonal Performance Factor of the Baseline Unit	$\frac{BTU}{W \cdot h}$	See Table 2-10	4
<u>HSPF<sub>2ee</sub></u> , <u>HSPF<sub>ee</sub></u> Heating Seasonal Performance Factor of the unit being installed	$\frac{BTU}{W \cdot h}$	Rated Value from AHRI Certificate	3, EDC Data Gathering
<u>COP<sub>ee</sub></u> , Coefficient of Performance of the unit being installed. This is a measure of the efficiency of a PTHP	<i>Proportion</i>	Rated Value from AHRI Certificate	3, EDC Data Gathering
<u>EFLH<sub>cool</sub></u> , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See Table 2-15	6
<u>EFLH<sub>heat</sub></u> , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See Table 2-15	6
<u>CF<sub>summer</sub></u> , Demand Coincidence Factor during the summer months	<i>Proportion</i>	See Table 2-15	6
<u>CF<sub>winter</sub></u> , Demand Coincidence Factor during the winter months	<i>Proportion</i>	See Table 2-15	6

Note: Where appropriate, nameplate data collected for usage in savings calculations (i.e., SEER, EER, HSPF) should be converted to new efficiency metrics (i.e., SEER2, EER2, HSPF2) using conversion equations laid out in Vol. 1 App. A

**Table 2-15: EDC Climate Region Weighted Composite Factors**

EDC	EFLH <sub>cool</sub>	EFLH <sub>heat</sub>	Summer CF	Winter CF
Duquesne	670	1,262	0.37	0.36
Met-Ed	870	1,122	0.44	0.33
Penelec	612	1,321	0.33	0.38
Penn Power	657	1,283	0.35	0.37
West Penn Power	675	1,265	0.37	0.37
PECO	972	1,027	0.48	0.29
PPL	764	1,198	0.41	0.35

The composite factors in Table 2-15: *EDC Climate Region Weighted Composite Factors* are based on the climate dependent values from Appendix A of the 2026 Technical Reference Manual. Appendix A provides heating and cooling Equivalent Full Load Hours (EFLH) and Coincident Factors (CF) for each climate region, as well as climate region weights for each EDC, based on the overlap of the EDC territories and climate regions. EDCs are encouraged to use the factors for the installation location's climate region, if it is possible to identify the region based on the premise address. Otherwise, the composite factors can be used as the default value for each EDC. The composite factors were developed as a weighted average of the EFLH and CF climate region values and the EDC weights for each climate region.

**EVALUATION PROTOCOLS**

Midstream program delivery reduces the data collection requirements of EDCs, their implementation CSPs, and program participants. However, EDC evaluation contractors should validate the make and model of a statistically representative sample of program-supported equipment. The EDC evaluation contractor should also confirm that the installation premise is (a) served by the EDC that supplied the incentive (b) metered on a residential or master-metered multifamily electric tariff, using the installation address collected by the distributor. EDC evaluation contractors may also choose to recalculate the weighted average EFLH values in Table 2-15: *EDC Climate Region Weighted Composite Factors* based on actual program participation.

**SOURCES**

- 1) California Electronic Technical Reference Manual. "SEER Rated AC and HP HVAC Equipment, Residential". Accessed February 2024. Weblink
- 2) U.S. EPA. (2022). ENERGY STAR Program Requirements Product Specification for Central Air Conditioner and Heat Pump Equipment. Eligibility Criteria Version 6.1. Weblink
- 3) AHRI Institute Directory of Certified Product Performance. Weblink
- 4) For ASHP, CAC: Federal Code of Regulations 10 CFR 430.32(c). Federal Code of Regulations 10 CFR 430.32(c). Weblink  
 For PTAC/PTHPs: Federal Code of Regulations 10 CFR 431.97(c); Weblink  
 As per IECC Residential code (Section R403.7), the requirements for all mechanical systems are stipulated to be federal minimums. Since there are no federal standards for Residential GSHP/PTAC/PTHPs, the C&I standards act as a proxy.
- 5) Average EER for SEER 13 units as calculated by  $EER = -0.02 \times SEER^2 + 1.12 \times SEER$  based on Wassmer, M., (2003), "A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations" as cited in U.S. DOE Building America House Simulation Protocol, Revised 2010. Weblink

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6) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)

### 2.2.3 HIGH EFFICIENCY EQUIPMENT: DUCTLESS HEAT PUMPS WITH MIDSTREAM DELIVERY OPTION

<u>Target Sector</u>	<u>Residential</u>
<u>Measure Unit</u>	<u>Ductless Heat Pump Unit</u>
<u>Measure Life</u>	<u>15 years<sup>Source 1</sup></u>
<u>Vintage</u>	<u>Early Replacement, Replace on Burnout, New Construction</u>

5.0 ENERGY STAR Version 6.1 ductless “mini-split” heat pumps technology is typically used to convert an electric resistance heated home into an efficient single or multi-zonal ductless heat pump system. Equipment will be considered eligible if it meets the efficiency requirements in ENERGY STAR Version 6.1.<sup>Source 2</sup>

Cooling savings may also be claimed under this measure for quality installation of properly sized new equipment, though not for equipment delivered through midstream programs.

#### ELIGIBILITY

This protocol documents the energy savings attributed to ductless heat pumps. Eligible equipment must meet ENERGY STAR Version 6.1 requirements.

The baseline heating system could be:

- 1) Existing electric resistance heating
- 2) Electric space heaters used as the primary heating source when fossil fuel (other than natural gas) heating systems failed (referred to as de facto heating)
- 3) A lower-efficiency ductless heat pump system
- 4) A ducted heat pump
- 5) Electric furnace

Cooling savings may also be claimed under this measure for quality installation of properly sized new equipment, though not for equipment delivered through midstream programs.

#### ELIGIBILITY

This protocol documents the energy savings attributed to ductless heat pumps. Eligible equipment must meet ENERGY STAR Version 5.0 requirements. The baseline heating system could be:

- 1) Existing electric resistance heating
- 2) 1) Electric space heaters used as the primary heating source when fossil fuel (other than natural gas) heating systems failed (referred to as de facto heating)<sup>19</sup>
- 3) 1) A lower-efficiency ductless heat pump system
- 4) 1) A ducted heat pump
- 5) 1) Electric furnace
- 6) A non-electric fuel-based system. (Implicit assumption in the Midstream route that a non-electric fuel/no heat baseline will be replaced with a minimum efficiency electric system).

The baseline cooling system can be:

<sup>19</sup> This baseline is for participants with broken beyond-repair oil heating systems who are heating their homes with portable electric space heaters.

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- 1) A standard efficiency heat pump system
- 2) A central air conditioning system
- 3) A room air conditioner

~~For new construction or addition applications, the baseline assumption is a standard-efficiency ductless unit (See Table 2-16). DHP systems may be installed as the primary heating or cooling system for the house or as a secondary heating or cooling system for a single room. Cooling savings claimed from proper sizing requires Manual J calculations, following of ENERGY STAR HVAC Quality Installation procedures, or similar calculations. The baseline cooling system can be:~~

- 1) ~~A standard efficiency heat pump system~~
- 2) ~~1) A central air conditioning system~~
- 3) ~~1) A room air conditioner~~

~~For new construction or addition applications, the baseline assumption is a standard-efficiency ductless unit (Table 2-12). DHP systems may be installed as the primary heating or cooling system for the house or as a secondary heating or cooling system for a single room. Cooling savings claimed from proper sizing requires Manual J calculations, following of ENERGY STAR HVAC Quality Installation procedures, or similar calculations. Residential establishmentsbuildings with properly sized baseline equipment are excluded from claiming savings from proper sizing.~~

#### MIDSTREAM HVAC OVERVIEW

Residential ductless mini-split heat pumps midstream delivery programs will offer incentives on eligible products sold to trade allies and customers through residential sales channels such as distributors of HVAC products. This complements other delivery channels (such as downstream rebates to trade allies and customers) by providing incentives to encourage distributors to stock, promote, and sell more efficient systems. Midstream savings calculations rely on composite baseline information formulated by blending historical participant data from PECO's downstream programs for PY8 to PY9 and PPL's programs from PY8 to PY10Q1 with the existing PA TRM deemed values for the downstream incentive program. See "Midstream Composite Baseline Calculations" below. Cooling savings from proper sizing cannot be claimed under midstream delivery programs.

#### ALGORITHMS

The savings depend on three main factors: baseline condition, usage (primary or secondary heating system), and the capacity of the indoor unit. This algorithm is used for the installation of new high efficiency air conditioners or heat pumps. For non-midstream delivery methods, if there are multiple zones, each zone should be calculated separately. For midstream delivery, composite values are provided.

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat} + \Delta kWh_{PSF}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool} \times DLF}{SEER_{base}} - \frac{1}{SEER_{ee}} \right) \times EFLH_{cool,zone} \times n_{MS\ zones}$$

~~Note: Be sure to use EFLH<sub>cool</sub> of Room ACs for secondary cooling zones. See Table 2-11.~~

$$\Delta kWh_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat} \times DLF}{HSPF_{base}} - \frac{1}{HSPF_{ee}} \right) \times EFLH_{heat,HP,zone} \times n_{MS\ zones}$$

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$$\Delta kWh_{PSF} = \frac{CAPY_{cool}}{SEER_{ee}} \times PSF \times EFLH_{cool} + \frac{CAPY_{heat}}{HSPF2_{ee}} \times PSF \times EFLH_{heat}$$

$$\Delta kW = \Delta kW_{cool} + \Delta kW_{PSF}$$

$$\Delta kW_{summer\ peak} = \Delta kW_{cool} + \Delta kW_{PSF,cool}$$

$$\Delta kW_{cool} = CAPY_{cool} \times \left( \frac{OF_{cool} \times DLF}{EER_{base}} - \frac{1}{EER_{ee}} \right) \times CF \times n_{MS\ zones}$$

$$\Delta kW_{PSF,cool} = \frac{CAPY_{cool}}{EER_{ee}} \times PSF \times CF$$

Note: Be sure to use  $EFLH_{heat}$  of Secondary HP for secondary heating zones. See Table 2-11.

$$\Delta kW_{winter\ peak} = \Delta kW_{heat} + \Delta kW_{PSF,heat}$$

$$\Delta kW_{heat} = CAPY_{heat} \times \left( \frac{OF_{heat} \times DLF}{COP_{base}} - \frac{1}{COP_{ee}} \right) \times \frac{1}{3.412 \frac{BTU}{Wh}} \times CF_{winter} \times n_{MS\ zones}$$

$$\Delta kW_{PSF,heat} = \frac{CAPY_{heat}}{COP_{ee}} \times PSF \times CF$$

#### Baseline: Room Air Conditioner(s)

EDCs may collect information about the capacity of existing RACs ( $W_{RAC}$ ) in use in the home to determine the replaced capacity. An oversizing factor is calculated from the ratio of baseline to qualifying capacity:

$$OF_{cool} = \frac{\sum CAPY_{RAC}}{CAPY_{cool}}$$

#### Baseline: Spaceheater(s), Electric Baseboards

EDCs may collect information about the capacity of the existing space heaters, electric furnaces, or electric baseboards. Capacity is determined using the total wattage of wattage of electric heat in use, where  $OF_{heat}$  is the ratio of the existing electric capacity to the capacity of the new equipment:

$$OF_{heat} = \frac{\sum kW_{spaceheat} \times 3.412 \frac{BTU}{Wh}}{CAPY_{heat}}$$

### DEFINITION OF TERMS

Table 2-16: Terms, Values, and References for High Efficiency Equipment: Ductless Heat Pump

Term	Unit	Value	Sources
$CAPY_{cool}$ , The cooling capacity of the central air conditioner or heat pump being installed <sup>20</sup>	kBTU/hr	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CAPY_{heat}$ , The heating capacity of the heat pump being installed <sup>21</sup>	kBTU/hr	EDC Data Gathering	AEPS Application; EDC Data Gathering

<sup>20</sup> This data is obtained from the AEPS Application Form or EDC's data gathering based on the model number.

<sup>21</sup> Ibid.

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Term	Unit	Value	Sources
$CAPY_{RAC}$ , The cooling capacity of the room AC. Used only for the RAC cooling baseline	$kBTU/hr$	EDC Data Gathering	EDC Data Gathering
$kW_{spaceheat}$ , The heating capacity of the space heaters in watts.	$kW$	EDC Data Gathering	EDC Data Gathering
$SEER_{base}SEER_{2base}$ , Seasonal Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: Table 2-18 or Table 2-10 in Sec. 2.2.1 Midstream: <u>12.413.6</u>	EDC Data Gathering; <u>2,3</u> , 10
$SEER_{ee}SEER_{2ee}$ , Seasonal Energy Efficiency Ratio of the qualifying unit being installed <sup>22</sup>	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$EER_{base}EER_{2base}$ , Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Table 2-18 or Table 2-10 in Sec. 2.2.1 <u>Table 2-12</u> Midstream: <u>11.4</u>	EDC Data Gathering; 3, <u>4, 5</u>
$EER_{ee}EER_{2ee}$ , Energy Efficiency Ratio of the unit being installed <sup>23</sup>	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default $EER_{ee}$ : $-0.022802 \times SEER_{ee}^2 + 1.152212 \times SEER_{ee}$	EDC Data Gathering; AEPS Application; 4, <u>5</u>
$HSPF_{base}HSPF_{2base}$ , Heating Seasonal Performance Factor of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: Table 2-18 or Table 2-10 in 2.2.1 Midstream: <u>6.70</u>	EDC Data Gathering; <u>2,3</u> , 10
$HSPF_{ee}HSPF_{2ee}$ , Heating Seasonal Performance Factor of the unit being installed <sup>24</sup>	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$PSF$ , Proper Sizing Factor or the assumed savings due to proper sizing and proper installation	<i>Proportion</i>	Midstream Delivery, properly size baseline equipment, or not properly sized: 0 Properly sized: 0.05	11

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<sup>22</sup> Ibid.

<sup>23</sup> Ibid.

<sup>24</sup> This data is obtained from the AEPS Application Form or EDC's data gathering.

Term	Unit	Value	Sources
$OF_{cool}$ , Oversize factor	None	EDC Data Gathering Default: Table 2-19 Midstream: 1.40	EDC Data Gathering; 56
$OF_{heat}$ , Oversize factor	None	EDC Data Gathering Default: Table 2-19 Midstream: 1.30	EDC Data Gathering; 67
$DLF$ , "Duct Leakage Factor" accounts for the fact that a % of the energy is lost to duct leakage and conduction for ducted systems, but not ductless ones	None	Depends on baseline & efficient conditions: Table 2-19 Midstream, cooling: 1.02 Midstream, heating: 1.0402	7, 8, 10
$zone$ , Primary or secondary usage level of a space, this affects $EFLH_{cool}$ and $EFLH_{heat}$ . For midstream delivery, use provided composite $EFLH$ values.	None	See Table 2-17	
$nMS_{zones}$ , Average number of heating and cooling zones per site. Note: this factor applies to mid-stream delivery only.	None	1.18	10
$EFLH_{cool}$ , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See $EFLH_{cool}$ in Vol. 1, App. A Use Room AC hours for secondary zones. Midstream: Table 2-24	89
$EFLH_{heat,HP}$ , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See $EFLH_{heat}$ in Vol. 1, App. A Use Secondary HP for secondary zones. Midstream: Table 2-24: Midstream DHP – Composite EFLH Values	89
$CF_{summer}$ , Demand Coincidence Factor during the summer months	Proportion	See $CF$ in Vol. 1, App. A	89
$CF_{winter}$ , Demand Coincidence Factor during the winter months	Proportion	See $CF$ in Vol. 1, App. A	9

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Note: Where appropriate, nameplate data collected for usage in savings calculations (i.e., SEER, EER, HSPF) should be converted to new efficiency metrics (i.e., SEER2, EER2, HSPF2) using conversion equations laid out in Vol. 1 App. A

**Table 2-17: Ductless Heat Pump Usage Zones**

Usage Zone	Definition
Primary	Dining room Family room House hallway Living room Kitchen areas Recreation room
Secondary	Basement Bathroom Bedroom Laundry/Mudroom Office/Study Storage room Sunroom/Seasonal room

**Table 2-18: Default Ductless Heat Pump Efficiencies**

Baseline Equip	Early Replacement			Replace on Burnout/New Construction		
	$SEER_{baseSEE}$ $R2_{base}$	$EER_{baseEE}$ $R2_{base}$	$HSPF_{baseHSP}$ $F2_{base}$	$SEER_{baseSEE}$ $R2_{base}$	$EER_{baseEE}$ $R2_{base}$	$HSPF_{baseHSP}$ $F2_{base}$
Ductless	13-14.3	11.3	8-27.5	14.3	12-11.7	8-27.5

Note: Early replacement defaults, though stemming from the Baseline study, have been capped to New construction/Replace on Burnout values (Federal standards)

**Table 2-19: Oversize and Duct Leakage Factors for High Efficiency Equipment**

Factors	ASHP	CAC	Ductless	Electric Baseboard	Electric Furnace	New Construction	RAC	Space Heaters
DLF	1.15	1.15	1	1	1.15	1	1	1
$OF_{heat}$	1.4	0	1	1.4	1.4	1	0	0.6
$OF_{cool}$	1.4	1.5	1	0	0	1	1	0

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**MIDSTREAM COMPOSITE BASELINE CALCULATIONS**

The Midstream-Delivery-Program This measure estimates the baseline system using composite values calculated from historical participant data. The composite

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SEER2, EER2, and HSPF2 values of the baseline inputs (SEER, EER, OF, DLF, and HSPF) are based on the PA TRM values Table 2-8 new construction/replace on burnout vintages, and baseline heating and cooling system splits from historical PECO PY8 to PY9 and PPL PY8 to PY10Q1 data. the 2023 Residential Baseline Study for early replacement vintages. Source 3

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The composite EFLH values assume a 50/50 split between primary and secondary installations and are a weighted average of EFLH values in Appendix A: Climate Dependent Values. Table 2-14 through Table 2-18

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Table 2-20: Midstream DHP – SEER2 and EER2 Baseline Splits through Table 2-24: Midstream DHP – Composite EFLH Values show the inputs for the calculation of each composite baseline value. The composite baseline values will be updated as needed from the downstream program participation data set. The split represents the approximate percentage of projects in the PECO and PPL territories that have the indicated Cooling Type. The split is calculated by dividing the number of projects with the indicated

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Cooling Type by the total number of projects in PECO PY8 to PY9 and PPL PY8 to PY10Q1 historical data set. The split is rounded to the nearest percent.

The composite value represents the weighted average of the system type based on the relative system splits.

For “No existing cooling” and “Room AC Cooling” Types, we make the assumption that the customer was initially upgrading to a Central Air Conditioning system and is incentivized to upgrade to a DHP. Similarly, for “No existing or non-electric heating” and “Standard DHP” types, the assumption is that the customer was upgrading to an “Air Source Heat Pump.”

**Table 2-20: Midstream DHP – SEERSEER2 and EEREER2 Baseline Splits**

Cooling Type	SEER <sub>base</sub> SEER2 <sub>base</sub>	EER <sub>base</sub> EER2 <sub>base</sub>	Split <sup>25</sup>
Central AC	13.04	11.32	4%
DHP or ASHP	14.03	12.011.8	8%
No existing cooling for primary space	13.04	11.32	29%
No existing cooling for secondary space	14.313.4	9.811.2	30%
Room AC	14.313.4	9.811.2	30%
Composite <sup>26</sup>	12.413.6	10.511.4	100%

**Table 2-21: Midstream DHP – HSPFHSPF2 Baseline Splits**

Heating Type	HSPF <sub>base</sub> HSPF2 <sub>base</sub>	Split
ASHP	8.27.5	3%
Electric furnace	3.2.7	1%
Electric resistance or de facto space heaters	3.42.9	32%
No existing or non-electric heating	8.27.5	57%
Standard DHP	8.27.5	8%
Composite	6.70	100%

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<sup>25</sup> The split represents the approximate percentage of projects in the PECO and PPL territory that have the indicated Cooling Type. The split is calculated by dividing the number of projects with the indicated Cooling Type by the total number of projects in PECO PY8 to PY9 and PPL PY8 to PY10Q1 historical data set. The split is rounded to the nearest percent.

<sup>26</sup> The composite value represents the weighted average of the system type based on the relative system splits. The computed average is rounded to the nearest tenth.

Table 2-22: Midstream DHP – DLF<sub>cool</sub> and OF<sub>cool</sub> Baseline Splits

Cooling Type	DLF <sub>cool</sub>	OF <sub>cool</sub>	Split
Central AC	1.15	1.50	8%
Central ASHP	1.15	1.40	5%
Ductless Heat Pump	1.00	1.0	19%
Room AC	1.00	1.0	69%
Composite	1.02	1.40	100%

Table 2-23: Midstream DHP – DLF<sub>heat</sub> and OF<sub>heat</sub> Baseline Splits

Heating Type	DLF <sub>heat</sub>	OF <sub>heat</sub>	Split
Central ASHP	1.15	1.40	6%
De facto Space Heaters	1.00	0.6	5%
Ductless Heat Pump	1.00	1.0	26%
Electric Baseboard	1.00	1.40	62%
Electric Furnace	1.15	1.40	1%
Composite	1.0402	1.30	100%

Table 2-24: Midstream DHP – Composite EFLH Values

Reference City	ZoneClimate Region	Composite EFLH <sub>cool</sub>	Composite EFLH <sub>heat</sub>
Allentown	C	377497	40401,008
Binghamton, NY	A	248253	42771,305
Bradford	G	435201	44451,325
Erie	I	307410	42431,131
Harrisburg	E	479562	4429959
Philadelphia	D	542637	906850
Pittsburgh	H	356439	40731,069
Scranton	B	340427	44431,089
Williamsport	F	366433	40851,083

**EVALUATION PROTOCOLS**

**EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of installation coupled with assignment of stipulated energy savings.

**SOURCES**

- 1) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020,

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<http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>.  
Accessed December 2018.

- 2) Federal Code of Regulations 10 CFR 430. <https://www.gpo.gov/fdsys/pkg/CFR-2017-title10-vol3/pdf/CFR-2017-title10-vol3-sec430-32.pdf>
- 3) Average EER for SEER 13 units as calculated by  $EER = -0.02 \times SEER^2 + 1.12 \times SEER$  based on Wassmer, M., (2003), "A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations" as cited in U.S. DOE Building America House Simulation Protocol, Revised 2010. <https://www.nrel.gov/docs/fy11osti/49246.pdf>

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## SOURCES

- 1) California Electronic Technical Reference Manual. "Ductless Heat Pump, Residential". Accessed February 2024 Weblink
- 2) U.S. EPA. (2022). ENERGY STAR Program Requirements Product Specification for Central Air Conditioner and Heat Pump Equipment. Eligibility Criteria Version 6.1. Weblink
- 3) For Early Replacement: NMR Group for the Pennsylvania Public Utility Commission. (Year, Month). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section/Chapter, pages, table reference. Weblink  
For new Construction: Federal Code of Regulations 10 CFR 430: Weblink
- 4) Average EER for SEER 13 units as calculated by  $EER = -0.02 \times SEER^2 + 1.12 \times SEER$  based on Wassmer, M., (2003), "A Component-Based Model for Residential Air Conditioner and Heat Pump Energy Calculations" as cited in U.S. DOE Building America House Simulation Protocol, Revised 2010. Weblink
- 4)5) "Methodology for Calculating Cooling and Heating Energy Input-Ratio (EIR) from the Rated Seasonal Performance Efficiency (SEER OR HSPF)" (Kim, Baltazar, Haberl). April 2013 Accessed December 2018.  
<http://oaktrust.library.tamu.edu/bitstream/handle/1969.1/152118/ESL-TR-13-04-01.pdf> Weblink
- 5)6) Based on REM/Rate modeling using models from the PA 2012 Potential Study<sup>27</sup>, Models assume 50% over-sizing of air conditioners<sup>27</sup> and 40% oversizing of heat pumps.<sup>28</sup>  
[Neme, Proctor, Nadal, "National Energy Savings Potential From Addressing Residential HVAC Installation Problems". ACEEE, February 1, 1999. Weblink](#)  
[Central Air Conditioning in Wisconsin, a compilation of recent field research. Energy Center of Wisconsin. May 2008, emended December 15, 2010. Weblink](#)  
[ACCA, "Verifying ACCA Manual S Procedures." Weblink](#)
- 6)7) Assumptions used to calculate a default value for de facto heating system OF: Four (4) 1500W portable electric space heaters in use in the home with capacity of  $4 \times 1.5kW \times 3412 \frac{BTU}{kWh} = 20,472 BTU$ , replaced by DHP with combined heating capacity of 36kBTU.  $OF = \frac{20,472}{36,000} \approx 0.6$
- 7)8) Assumption used in Illinois 2014 TRM, Ductless Heat Pumps Measure, p. 531, footnote 877. Reasonable Engineering judgement: Conservative assumption when compared for duct leakage to [http://www.energystar.gov/index.cfm?c=home\\_improvement.hm\\_improvement\\_ducts](http://www.energystar.gov/index.cfm?c=home_improvement.hm_improvement_ducts) and be around 15%. ENERGY STAR. "Duct Sealing". Accessed March 2024. CIEE/PG&E. (2002, May). Residential HVAC and

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<sup>27</sup> Neme, Proctor, Nadal, "National Energy Savings Potential from Addressing Residential HVAC Installation Problems. ACEEE, February 1, 1999. Confirmed also by [Central Air Conditioning in Wisconsin, a compilation of recent field research. Energy Center of Wisconsin. May 2008, emended December 15, 2010. http://ecw.org/sites/default/files/2411\\_0.pdf](#)

<sup>28</sup> ACCA, "Verifying ACCA Manual S Procedures." <http://www.acca.org/wp-content/uploads/2014/01/Manual-S-Brochure-Final.pdf>



Distribution Research Implementation, Berkeley Labs, May, 2002, p. Page 6.  
<http://epb.lbl.gov/publications/pdf/lbnl-47214.pdf> Weblink

- 8) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. <https://www.ecobee.com/donateyourdata/>
- 9) ~~Assumptions used to calculate a default value for de facto heating system OF: Four (4) 1500 W portable electric space heaters in use in (Weblink) and updated based on the home with capacity of  $1500 \times 3.412 \times 4 = 20,472$  BTU, replaced by DHP with combined heating capacity of 36,000 BTU. OF =  $20,472 / 36,000 = 0.6$ . latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)~~
- 10) PECO PY8 to PY9 Program Participation Data and PPL PY8 to PY10Q1 Program Participation Data
- 11) Northeast Energy Efficiency Partnerships, Inc., "Strategies to Increase Residential HVAC Efficiency in the Northeast", (February 2006): Appendix C Benefits of HVAC Contractor Training: Field Research Results 03-STAC-01, p. 4.

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**2-2-32.2.4 ECM CIRCULATION FANS**

<b>Target Sector</b>	Residential <del>Establishments</del>
<b>Measure Unit</b>	ECM Circulation Fan
<b>Measure Life</b>	155 years <sup>Source 1</sup>
<b>Measure Vintage</b>	Early Replacement, Replace on Burnout

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This protocol covers energy and demand savings associated with retrofit of permanent-split capacitor (PSC) evaporator fan motors in an air handling unit with an electronically commutated motor (ECM).

**ELIGIBILITY**

This measure is targeted to residential customers whose air handling equipment currently uses a standard low-efficiency permanent split capacitor (PSC) fan motor rather than an ECM.

The targeted fan can supply heating or cooling only, or both heating and cooling. A default savings option is offered if motor input wattage is not known. However, these parameters should be collected by EDCs for greatest accuracy.

Acceptable baseline conditions are an existing circulating fan with a PSC fan motor.

Efficient conditions are a circulating fan with an ECM.

**ALGORITHMS**

This algorithm is used for the installation of new high efficiency circulating fans, or air handler replacement that includes a high efficiency fan.

$$\Delta kWh_{heat} = ECM_{kW} \times EFLH_{heat}$$

$$\Delta kWh_{cool} = ECM_{kW} \times EFLH_{cool}$$

$$\Delta kWkW_{summer\ peak} = ECM_{kW} \times CF_{summer}$$

$$\Delta kW_{winter\ peak} = ECM_{kW} \times CF_{winter}$$

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**DEFINITION OF TERMS**

Table 2-25: Terms, Values, and References for ECM Furnace Fan

Term	Unit	Value	Sources
<i>ECM<sub>kW</sub></i> , Reduced energy demand of the efficient ECM vs. baseline PSC motor.	kW	EDC Data Gathering, Default: 0.116	2, EDC Data Gathering
<i>EFLH<sub>cool</sub></i> , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See <i>EFLH<sub>cool</sub></i> in Vol. 1, App. A	3
<i>EFLH<sub>heat</sub></i> , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See <i>EFLH<sub>heat</sub></i> in Vol. 1, App. A	3
<i>CF<sub>summer</sub></i> , Demand Coincidence Factor during the summer months	Proportion	See CF in Vol. 1, App. A	3
<i>CF<sub>winter</sub></i> , Demand Coincidence Factor during the winter months	Proportion	See CF in Vol. 1, App. A	3

## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

- 1) ~~“Energy Savings from Efficient Furnace Fan Air Handlers in Massachusetts,” ACEEE, Sachs and Smith, 2003. For the purpose of calculating the total Resource Cost Test for Act 129, measure cannot claim savings for more than fifteen years.~~
- 1) California Electronic Technical Reference Manual. “Brushless Fan Motor Replacement”. Residential. Accessed January 2024. Weblink
- 2) Cadmus (for the Public Service Commission of Wisconsin); (2014, November). “Focus on Energy Evaluated Deemed Savings Changes”, November 2014, Table 3 Description of Variables for Furnaces with ECM. <https://focusonenergy.com/sites/default/files/FoE-Deemed-WriteUp%20CY14%20Final.pdf> Weblink
- 3) ~~Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/>.~~
- 3) Weblink Updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020). Weblink

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**2.2.42.2.5 GSHP DESUPERHEATERS**

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	GSHP Desuperheater
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

**ELIGIBILITY**

<b>Measure Life</b>	15 years
<b>Vintage</b>	Retrofit

**ELIGIBILITY**

Installation of a desuperheater on ~~an~~ new or existing Ground Source Heat Pump to replace any type of electric water heater.

**ALGORITHMS**

This algorithm is used for the installation of a desuperheater for a GSHP unit.

$$\Delta kWh = \frac{EF_{SH}}{UEF_{Base}} \times HW \times 365 \frac{days}{yr} \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{hot} - T_{cold})$$

$$3,412 \frac{BTU}{kWh}$$

~~$\Delta kW$~~  =  $\Delta kWh \times ETDf$

$\Delta kW_{summer\ peak\_} = \Delta kWh \times ETDf_{summer}$

$\Delta kW_{winter\ peak} = 0$

**DEFINITION OF TERMS**

Table 2-26: Terms, Values, and References for GSHP Desuperheater

Term	Unit	Value	Sources
$EF_{SH}$ , Energy Factor per desuperheater	None	0.17	1, 2, 3
$HW$ , Daily hot water use	Gallons/Day	45.5	7
$T_{hot}$ , Hot Water Temperature	°F	119	34
$T_{cold}$ , Cold Water Temperature	°F	52	45
$UEF_{base}$ , Uniform Energy Factor of Electric Water Heater	None	EDC Data Gathering, Default: 1.030.92	EDC Data Gathering, 56

Term	Unit	Value	Sources
<del>ETDF</del> , <del>ETDF</del> <sub>summer</sub> Energy to Demand Factor	<del>kW/kWh/year</del> None	0.00008047 Table 2-27	68

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**Table 2-27: Energy to Demand Factor for GSHP Desuperheater**

Building Type	<i>ETDF<sub>summer</sub></i>
Mobile Home	0.0001011
Multi-Family with 2 - 4 Units	0.0001006
Multi-Family with 5+ Units	0.0001007
Single-Family Attached	0.0001026
Single-Family Detached	0.0001070

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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**SOURCES**

- 1) NY TRM (October 2023, V11) Heat PUMP – Water-to-Air Ground Source (GSHP) Appendix P, Effective Useful Life (EUL, Single and Multi-Family Residential Measures, Heat Pump – Ground Source Weblink.  
 The Desuperheater is assumed to have an equal EUL of a GSHP (25 Years). With the rulings of Act 129 the EUL for this measure will be capped at 15 years.
- 2) "Residential Ground Source Heat Pumps with Integrated Domestic Hot Water Generation: Performance Results from Long-Term Monitoring", U.S. Department of Energy, November 2012.
- 3) Desuperheater Study, New England Electric System, 1998 42 U.S.C.A 6295(i) (West Supp. 2011) and 10 C.F.R. 430.32 (x) (2011).
- 4) Pennsylvania Statewide Residential End-Use and Saturation Study, 2014, Weblink.

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**USING ROCK SPRING, PA (SITE 2036) AS A PROXY, THE MEAN OF SOIL TEMPERATURE AT 40 INCH DEPTH IS 51.861. CALCULATED USING DAILY SCAN STANDARD - PERIOD OF RECORD DATA FROM APRIL 1999 TO DECEMBER 2018 FROM THE NATURAL RESOURCE CONSERVATION SERVICE DATABASE. WEBLINK.. METHODOLOGY FOLLOWS MISSOURI TRM 2017 VOLUME 2: COMMERCIAL AND INDUSTRIAL MEASURES. P. 78. EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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**DEFAULT SAVINGS**

Default savings are 446.7 kWh and 0.036 kW demand savings.

**SOURCES**

- 1) ~~“Residential Ground Source Heat Pumps with Integrated Domestic Hot Water Generation: Performance Results from Long-Term Monitoring”, U.S. Department of Energy, November 2012.~~
- 2) ~~1) Desuperheater Study, New England Electric System, 1998 42 U.S.C.A. 6295(i) (West Supp. 2011) and 10 C.F.R. 430.32 (x) (2011).~~
- 3) ~~1) Pennsylvania Statewide Residential End Use and Saturation Study, 2014,  
[http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014\\_PA\\_Statewide\\_Act129\\_Residential\\_Baseline\\_Study.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014_PA_Statewide_Act129_Residential_Baseline_Study.pdf).~~
- 4) ~~5) Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40 inch depth is 51.861. Calculated using Daily SCAN Standard – Period of Record data from April 1999 to December 2018 from the Natural Resource Conservation Service Database.  
[https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\\_scan\\_por&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily_scan_por&state=PA). Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p. 78.  
<https://energy.mo.gov/sites/energy/files/MOITRM2017Volume2.pdf> Weblink.~~
- 5) ~~The default value of 1.030\_92 UEF includes both standard and heat pump for electric water heaters. heater is from NMR Group for the Pennsylvania Act 129 2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf).~~
- 6) ~~Straub, Mary and Switzer, Sheldon. "Using Available Information for Efficient Evaluation of Demand Side Management Programs". Study by BG&E. The Electricity Journal, Aug/Sept. 2011. p. 95. <http://www.sciencedirect.com/science/article/pii/S1040619011001941>~~
- 7) ~~6) “Public Utility Commission. (Year, Month). 2023 Pennsylvania Statewide Act 129 Residential End Uses of Water, Version 2.” Baseline Study. Section/Chapter, pages, table reference. Weblink [Water Research Foundation. \(Apr 2016\), p. 5. https://www.circleofblue.org/wp-content/uploads/2016/04/WRF\\_REU2016.pdf](https://www.circleofblue.org/wp-content/uploads/2016/04/WRF_REU2016.pdf)~~
- 7) ~~“Residential End Uses of Water, Version 2.” *Water Research Foundation*. (Apr 2016), p. 5. Weblink.~~
- 8) ~~Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink~~

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## 2-2.52.2.6 AIR CONDITIONER & HEAT PUMP MAINTENANCE

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Central A/C, ASHP, Ductless Mini-Split HP, GSHP, PTAC or PTHP Unit
<b>Measure Life</b>	3 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

This algorithm is used for measures providing services to maintain, service or tune-up refrigerant-driven Central A/C and heat pump units. The tune-up must include the following at a minimum:

- Check refrigerant charge level and correct as necessary
- Clean filters as needed
- Inspect and lubricate bearings
- Inspect and clean condenser and, if accessible, evaporator coil

### ELIGIBILITY

An existing central A/C, air source heat pump, ground source heat pump, ductless mini-split heat pump, PTAC, or PTHP unit.

### ALGORITHMS

This algorithm is used for the maintenance of ASHP, DHP and CAC measures:

$$\Delta kWh = \Delta \Delta kWh_{cool} + \Delta \Delta kWh_{heat}$$

$$\Delta kWh_{cool} = \frac{CAPY_{cool}}{SEER_{base}} \times MF \times EFLH_{cool}$$

$$\Delta kWh_{heat}^{29} = \frac{CAPY_{heat}}{HSPF_{base}} \times MF \times EFLH_{heat,HP}$$

$$\Delta kW_{summer\ peak} = \frac{CAPY_{cool}}{EER2_{base}} \times MF \times CF_{summer}$$

$$\Delta kW_{winter\ peak} = \frac{CAPY_{heat}}{COP_{base}} \times \frac{1}{3.412 \frac{BTU}{W \cdot h}} \times MF \times CF_{winter}$$

This algorithm is used for the maintenance of GSHP, PTAC and PTHP measures:

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{cool} = \frac{CAPY_{cool}}{SEER_{base}} \times MF \times EFLH_{cool}$$

$$\Delta kWh_{heat} = \frac{CAPY_{heat}}{HSPF_{base}} \times MF \times EFLH_{heat,HP}$$

$$\Delta kW_{summer\ peak} = \frac{CAPY_{cool}}{EER_{base}} \times MF \times GFCF_{summer}$$

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<sup>29</sup> Does not apply for CAC or PTAC.



### Ground-Source Heat Pumps (GSHP)

GSHP efficiencies are typically calculated differently than air-source units and

$$\Delta KW_{winter\ peak} = \frac{CAPY_{hea}}{COP_{base}} \times \frac{1}{3.412 \frac{BTU}{Wh}} \times MF \times CF_{winter}$$

#### Qualifying: Ground Source Heat Pump

GSHP efficiencies are typically calculated differently than air-source units, baseline and qualifying unit efficiencies should be converted as follows:

$$\cancel{SEER}_{base} SEER = EER_g \times \cancel{GSHPDF} \times \cancel{GSER}$$

$$\cancel{EER}_{base} EER = EER_g \times \cancel{GSPK}$$

$$\cancel{HSPF}_{base} = \cancel{HSPF} = COP_g \times \cancel{GSHPDF} \times 3.412 \frac{BTU}{Wh} \times \cancel{GSOP}$$

#### PTAC and PTHP

$$\cancel{COP} = COP_g$$

#### PTAC and PTHP

$$\cancel{SEER}_{base} = EER_{base}$$

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**DEFINITION OF TERMS**

**Table 2-28: Terms, Values, and References for Air Conditioner & Heat Pump Maintenance**

Term	Unit	Value	Sources
$CAPY_{cool}$ , The cooling capacity of the central air conditioner or heat pump being installed <sup>30</sup>	<i>kBTU/hr</i>	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CAPY_{heat}$ , The heating capacity of the heat pump being installed <sup>31</sup>	<i>kBTU/hr</i>	EDC Data Gathering	AEPS Application; EDC Data Gathering
$MF_{\rightarrow}$ , Maintenance Factor or assumed savings due to completing recommended maintenance on installed cooling equipment	<i>Proportion</i>	0.05	2
$EFLH_{cool}$ , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See $EFLH_{cool}$ in Vol. 1, App. A	3
$EFLH_{heat,HP}$ , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See $EFLH_{heat}$ in Vol. 1, App. A	3
$SEER_{base}$ , Seasonal Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: See Early Replacement values in Table 2-8 in Sec. 2.2.4	EDC Data Gathering 4
		Default: See Early Replacement values in Table 2-10	4
$HSPF_{base}$ , Heating Seasonal Performance Factor of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: See Early Replacement values in Table 2-8 in Sec. 2.2.4	EDC Data Gathering 4
		Default: See Early Replacement values in Table 2-10	4
$EER_g$ , Energy Efficiency Ratio of a GSHP, this is measured differently than EER of an air source heat pump and must be converted	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: 16.6	4EDC Data Gathering 4
		Default: 16.6	4
$EER_{base}$ , Energy Efficiency Ratio of the Baseline Unit	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: See Early Replacement values in Table 2-8 in Sec. 2.2.4	EDC Data Gathering 4
		Default: See Early Replacement values in Table 2-10	4
$COP_g$ , Coefficient of Performance. This is a measure of the efficiency of a ground source heat pump	<i>None</i>	EDC Data Gathering Default: 3.6	AEPS Application; EDC Data Gathering
		Default: 3.6	4

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<sup>30</sup> This data is obtained from the AEPS Application Form or EDC's data gathering based on the model number.  
<sup>31</sup> Ibid.

Term	Unit	Value	Sources
GSEER, Factor used to determine the SEER of a GSHP based on its EER <sub>g</sub>	$\frac{BTU}{W \cdot h}$	1.02 See Table 2-13	5
GSPKGSOP, Factor to convert EER <sub>g</sub> COP <sub>g</sub> to the equivalent EERCOP of an air conditioner-source unit to enable comparisons to the baseline unit	Proportion	0.8416 See Table 2-13	5
GSHPDF, Ground Source Heat Pump De-rate Factor $CF_{summer}$ , Demand Coincidence Factor during the summer months	Proportion	0.885 See CF in Vol. 1, App. A	63
GFCF <sub>winter</sub> , Demand Coincidence Factor during the winter months	Proportion	See CF in Vol. 1, App. A	3

Note: Where appropriate, nameplate data collected for usage in savings calculations (i.e., SEER, EER, HSPF) should be converted to new efficiency metrics (i.e., SEER2, EER2, HSPF2) using conversion equations laid out in Vol. 1 App. A

### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

- 4) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.
- 1) California Electronic Technical Reference Manual. "Refrigerant Charge – Residential" and "Clean Condenser Coils – Residential" listed in the CPUC Support Table "Effective Useful Life and Remaining Useful Life". Accessed December 2023. Weblink
- 2) Energy Center of Wisconsin, (2008, May). "Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research", May-2008. Weblink
- 3) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. <https://www.ecobee.com/donateyourdata/> (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)

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- 4) ~~4) Pennsylvania-NMR Group for the Pennsylvania Public Utility Commission. (2023, March). 2023 Pennsylvania Statewide Act 129 2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Weblink. Due to small sample size for GSHP in Pennsylvania Act 129 20182023 Residential Baseline Study this value is lowest efficiency value from BEopt v2.8v3.0. PTAC and PTHP standards1.0.~~
- 4) ~~4) Factors are based on requirements of ASHRAE 90.1-2016, Energy Standard for Buildings Except Low-Rise Residential Buildings, Table 6.8.1-4, <https://www.ashrae.org/technical-resources/standards-and-guidelines/read-only-versions-of-ashrae-standards>.~~
- 5) ~~5) VEIC estimate. Extrapolation of manufacturer data.~~
- 6) ~~6) McQuay Application Guide 31-008, Geothermal derived from the conversion algorithms depicted in the Heat Pump Design Manual, 2002. Engineering Estimate – See System Performance of – Water-to-air Ground Source Heat Pumps~~

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**2.2.6 FUEL SWITCHING: ELECTRIC HEAT TO GAS/PROPANE/OIL HEAT**

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Gas, Propane, or Oil Heater
<b>Measure Life</b>	15 years
<b>Vintage</b>	Replace on Burnout

This protocol documents the energy savings attributed to converting from an existing electric heating system to a new natural gas, propane, or oil furnace or boiler in a residential home.

The baseline for this measure is an existing residential home with an electric primary heating source. The heating source can be electric baseboards, electric furnace, or electric air source heat pump.

**ELIGIBILITY**

The target sector primarily consists of single-family residences.

EDCs may provide incentives for equipment with efficiencies greater than or equal to the applicable ENERGY STAR requirement per the following table.

Equipment	Energy Star Requirements
Gas Furnace <sup>Source 1</sup>	AFUE rating of 95% or greater Furnace fan must have electronically commutated fan motor (ECM) Less than or equal to 2.0% air leakage
Oil Furnace <sup>Source 1</sup>	AFUE rating of 85% or greater Furnace fan must have electronically commutated fan motor (ECM) Less than or equal to 2.0% air leakage
Gas Boiler <sup>Source 2</sup>	AFUE rating of 90% or greater
Oil Boiler <sup>Source 2</sup>	AFUE rating of 87% or greater

(GSHP) Measure of

**ALGORITHMS**

The energy savings are the full energy consumption of the electric heating source minus the energy consumption of the fossil fuel furnace blower motor. EDCs may use billing analysis using program participant data to claim measure savings, in lieu of the defaults provided in this measure protocol. The energy savings are obtained through the following formulas:

**Heating savings with electric furnace (assumes 95% efficiency):<sup>32</sup>**

$$\Delta kWh = EFLH_{heat, non-HP} \times \frac{CAPY_{elec}}{3.241 \frac{BTU}{Wh}}$$

<sup>32</sup> Using the relation  $HSPF = COP \times 3.412$ , where  $HSPF = 3.412$  for electric resistance heating. Electric furnace efficiency typically varies from 0.95 to 1.00, therefore a COP of 0.95 equates to an HSPF of 3.241.

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**Heating savings with electric baseboards (assumes 100% efficiency):**

$$\Delta kWh = EFLH_{heat,non-HP} \times \left( \frac{CAPY_{elec}}{3.412 \frac{BTU}{Wh}} - \frac{HP_{motor} \times 0.746 \frac{kW}{hp}}{\eta_{motor}} \right)$$

**Heating savings with electric air source heat pump:**

$$\Delta kWh = \frac{EFLH_{heat,HP} \times CAPY_{HP,heat}}{HSPF} - \frac{EFLH_{heat,non-HP} \times HP_{motor} \times 0.746 \frac{kW}{hp}}{\eta_{motor}}$$

For boilers, the annual pump energy consumption is negligible (<50 kWh per year) and not included in this calculation.<sup>33</sup>

There are no peak demand savings as it is a heating-only measure.

Although there is a significant electric savings, there is also an associated increase in natural gas energy consumption:

$$\Delta MMBTU = -\Delta kWh \times 0.003412 \frac{MMBTU}{kWh}$$

**DEFINITION OF TERMS**

The default values for each term are shown in the table below:

**Table 2-22: Terms, Values, and References for Fuel Switching: Electric Heat to Gas Heat**

Term	Units	Value	Source
$CAPY_{elec}$ , Total heating capacity of existing electric baseboards or electric furnace	$\frac{kBTU}{hr}$	EDC Data Gathering	EDC Data Gathering
$CAPY_{HP,heat}$ , Total heating capacity of existing electric ASHP	$\frac{kBTU}{hr}$	EDC Data Gathering	EDC Data Gathering
$EFLH_{heat,HP}$ , Equivalent Full Load Heating hours for Air Source Heat Pumps	$\frac{hours}{yr}$	See $EFLH_{heat,HP}$ values in Vol. 1, App. A	3
$EFLH_{heat,non-HP}$ , Equivalent Full Load Heating hours for furnaces, boilers, and electric baseboards	$\frac{hours}{yr}$	See $EFLH_{heat,non-HP}$ values in Vol. 1, App. A	3
$HSPF$ , Heating Seasonal Performance Factor for existing heat pump	$\frac{BTU}{Wh-hr}$	EDC Data Gathering or Default = 8.2	EDC Data Gathering 4
$AFUE_{fuel-heat}$ , Annual Fuel Utilization Efficiency for the new gas or oil furnace or boiler	%	EDC Data Gathering or Defaults: NG/LPG furnace = 95% NG/LPG boiler = 90% Oil furnace = 85% Oil boiler = 87%	EDC Data Gathering 1,2
$HP_{motor}$ , Furnace blower motor horsepower	hp	EDC Data Gathering or Default = 1/2	EDC Data Gathering

<sup>33</sup> Pump motors are typically 1/25 HP. With 1,000-hour runtime and 80% assumed efficiency, this translates to 37 kWh.

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Term	Units	Value	Source
$\eta_{motor}$ , Efficiency of furnace blower motor	%	EDC Data Gathering or Default = 50%	5 EDC Data Gathering Typical efficiency of 1/2 HP blower motor

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### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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### SOURCES

- 1) ENERGY STAR Program Requirements: Product Specification for Boilers, v3.0.  
<https://www.energystar.gov/sites/default/files/specs//private/Boilers%20Program%20Requirements%20Version%203%200.pdf>
- 2) ENERGY STAR Program Requirements: Product Specification for Furnaces, v4.1-NY TRM.  
<https://www.energystar.gov/sites/default/files/Furnaces%20Version%204.1%20Program%20Requirements%200.pdf#webLink>
- 3) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. <https://www.ecobee.com/donateyourdata/>
- 4) Pennsylvania Act 129 2018 Residential Baseline Study,  
[http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf).
- 5) Average blower motor capacity for gas furnace, typical range = 1/4 to 3/4 HP.

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**ENERGY STAR**



### 2.2.7 ROOM AIR CONDITIONERS

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Room Air Conditioner
<b>Measure Life</b>	9 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout

#### ELIGIBILITY

This measure relates to the purchase and installation of a room air conditioner meeting ENERGY STAR Version 4.1 exceeding efficiency criteria prescribed by federal standards.

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#### ALGORITHMS

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of room air conditioners. The number of room air conditioners will be determined using market assessments and market tracking.

As of June 1, 2014 RAC units have are rated using a CEER rating as well as an EER. CEER is the (Combined Energy Efficiency Ratio), which incorporates standby power into the calculation. This will be the value used in the savings algorithm.

$$\Delta kW_h = CAPY \times \left( \frac{1}{CEER_{base}} - \frac{1}{CEER_{ee}} \right) \times EFLH_{RAC}$$

$$\Delta kW_{peak} = kW_{summer peak} = CAPY \times \left( \frac{1}{CEER_{base}} - \frac{1}{CEER_{ee}} \right) \times CF_{CF_{summer}}$$

$$\Delta kW_{winter peak} = 0$$

#### DEFINITION OF TERMS

#### DEFINITION OF TERMS

Table 2-29: Terms, Values, and References for ENERGY STAR Room AC

Term	Unit	Value	Sources
CAPY, The cooling capacity of the room air conditioner (RAC) being installed	$\frac{kBTU}{h}$	EDC Data Gathering Default = 7.5	5 EDC Data Gathering
		Default = 7.2	2
CEER <sub>base</sub> , Combined Energy Efficiency ratio of the baseline unit	$\frac{BTU}{W \cdot h}$	Federal Standard Values in Table 2-24, Table 2-25, or Table 2-26 Federal Standard Values Table 2-30: RAC (without reverse cycle) Federal Minimum CEER Standards Table 2-30	23

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		Table 2-31, or Table 2-32 Table 2-32 Default = 416.0	
$CEER_{ee}$ , Combined Energy efficiency ratio of the RAC being installed	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default = ENERGY STAR values in in Table 2-24, Table 2-25, or Table 2-26	3EDC Data Gathering
$EFLH_{RAC}$ , Equivalent full load hours of the RAC being installed	$\frac{hours}{year}$	See $EFLH_{RAC}$ in Vol. 1, App. A	4
$CF_{summer}$ , Demand coincidence factor during the summer months	Proportion	See $CF$ in Vol. 1, App. A	4

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Table 2-30: RAC (without reverse cycle) Federal Minimum CEER Standards Table 2-30 lists the minimum federal efficiency standards as of October 2018 and minimum ENERGY STAR efficiency standards May 2026 for RAC units of various capacity ranges and with and without louvered sides. Units without louvered sides are also referred to as “through the wall” units or “built-in” units. Note that the new federal standards are based on the Combined Energy Efficiency Ratio metric (CEER), which is a metric that incorporates energy use in all modes, including standby and off modes.

Table 2-30: RAC (without reverse cycle) Federal Minimum Efficiency and ENERGY STAR Version 4.1 CEER Standards

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Capacity (kBtu/h)	Federal Standard Minimum CEER, with louvered sides	ENERGY STAR CEER, with louvered sides	Federal Standard CEER, without louvered sides	ENERGY STAR CEER, without louvered sides
	With Louvered Sides	Without Louvered Sides		
<6	11.0	13.1	10.0	11.0
6<8	13.7	12.4		
8<11	10.9	12.6	10.6	
11<14		13.9	10.5	
14<20		10.3	11.8	9.3
20<28	9.4	13.8	9.4	10.3
≥28	9.0	13.2	9.4	10.3

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Table 2-31 lists the minimum federal efficiency standards and minimum ENERGY STAR efficiency standards for casement-only and casement-slider RAC units. Casement-only refers to a RAC designed for mounting in a casement window with an encased assembly with a width of 14.8 inches or less and a height of 11.2 inches or less. Casement-slider refers to a RAC with an encased assembly designed for mounting in a sliding or casement window with a width of 15.5 inches or less.

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**Table 2-31: Casement-Only and Casement-Slider RAC Federal Minimum Efficiency and ENERGY STAR Version 4.1 CEER Standards**

Casement	Federal Standard Minimum CEER	ENERGY STAR CEER
Casement-only	13.95	10.5
Casement-slider	10.4153	11.4

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Table 2-26 Table 2-32 Table 2-32 lists the minimum federal efficiency standards and minimum ENERGY STAR efficiency standards for reverse-cycle RAC units.

**Table 2-32: Reverse-Cycle RAC Federal Minimum Efficiency CEER Standards and ENERGY STAR Version 4.1 Standards**

Capacity (kBTU/h)	Federal Standard Minimum CEER, with Louvered Sides	ENERGY STAR CEER, with Louvered Sides	Federal Standard CEER, without Louvered Sides	ENERGY STAR CEER, without Louvered Sides
	With Louvered Sides	Without Louvered Sides		
< 14	n/a	n/a	13.7	9.3, 10.2
≥ 14		12.8	8.7	9.6
< 20	9.8, 14.4	10.8	n/a	n/a
≥ 20	9.3, 13.7	10.2		

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

**DEFAULT SAVINGS**

Default energy savings values assume a CAPY=7.5 kBTU/hr<sup>Source 5</sup>, louvered sides, no reverse cycle unit (CEER<sub>base</sub> = 11.0, CEER<sub>re</sub> = 12.1).

**Table 2-27: Deemed EFLH and Default Energy Savings**

Climate Region	Reference City	$\Delta kWh/yr$	$\Delta kW_{peak}$
C	Allentown	11.0	0.022
A	Binghamton, NY	6.4	0.016
G	Bradford	4.0	0.014
I	Erie	9.0	0.016
E	Harrisburg	14.1	0.028
D	Philadelphia	15.0	0.026
H	Pittsburgh	10.5	0.023
B	Scranton	9.1	0.020
F	Williamsport	10.7	0.024

- 1) California Electronic Technical Reference Manual. "Room Air Conditioner, Residential". Accessed August 2023. Weblink.
- 2) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Sec 8.2.2 Table 104. Statewide average for all housing types. Weblink
- 3) Federal code of regulation. Room air conditioners. 10 C.F.R. § 430.32 (b)(2). Weblink

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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- 1) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.
- 2) Federal standards: U.S. Department of Energy. Code of Federal Regulations. 10 CFR, part 430.32(b). Effective June 1, 2014. [http://www1.eere.energy.gov/buildings/appliance\\_standards/product.aspx/productid/41](http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/41)
- 3) ENERGY STAR Program Requirements Product Specification for Room Air Conditioners, Eligibility Criteria Version 4.1. October 26, 2015. [https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%204.1%20Room%20Air%20Conditioners%20Specification\\_0.pdf](https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%204.1%20Room%20Air%20Conditioners%20Specification_0.pdf)
- 4) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/>.
- 5) Statewide average for all housing types (Weblink) and updated based on the latest CDD and HDD values from Pennsylvania Act 129 2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). NOAA's 15-year annual climate Normals (2006–2020) (Weblink)

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### 2.2.8 ROOM AC (RAC) RETIREMENT

### 2.2.82.1.1 ROOM AC (RAC) RETIREMENT

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Room A/C
<b>Measure Life</b>	3 years <sup>Source 1</sup>
<b>Vintage</b>	Early Retirement, Early Replacement
<b>Measure Life</b>	3 years <sup>Source-1</sup>
<b>Vintage</b>	Early Retirement, Early Replacement

This measure is defined as retirement and recycling ~~without replacement~~ of an operable but older and inefficient room AC (RAC) unit that would not have otherwise been recycled. The assumption is that these units will be permanently removed from the grid rather than handed down or sold for use in another location by another EDC customer, and furthermore that they would not have been recycled without this program. This measure is quite different from other energy-efficiency measures in that the energy/demand savings is not the difference between a pre- and post-configuration, but is instead the result of complete elimination of the existing RAC.

#### ELIGIBILITY

The savings are *not* attributable to the customer that owned the RAC, but instead are attributed to a hypothetical user of the equipment had it not been recycled. Energy and demand savings is the estimated energy consumption of the retired unit over its remaining useful life (RUL).

#### ALGORITHMS

~~Although this is a fully deemed approach, any of these values can and should be evaluated and used to improve the savings estimates for this measure in subsequent TRM revisions.~~

#### Retirement-Only

All EDC programs are currently operated under this scenario. For this approach, impacts are based only on the existing unit, and savings apply *only for the remaining useful life (RUL) of the unit*.

$$\Delta kWh = \left( \frac{CAPY}{EER_{RetRAC}} \right) \times EFLH_{RAC}$$

$$\Delta kW_{peak} kW_{summer\ peak} = \left( \frac{CAPY}{EER_{RetRAC}} \right) \times GFCF_{summer}$$

$$\Delta kW_{winter\ peak} = 0$$

#### Replacement and Recycling

For this approach, the ~~ENERGY STAR~~ efficient RAC upgrade measure would have to be combined with recycling via a turn-in event at a retail appliance store, where the old RAC is turned in at the same time that a new one is purchased. Unlike the retirement-only measure, the savings here are attributed to the customer that owns the retired RAC, and are based on the old unit and original unit being of the same size and configuration. In this case, two savings calculations would be needed. One would be applied over the remaining life of the recycled unit, and another would be used for the rest of the effective useful life, as explained below.

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For the remaining useful life (RUL) of the existing RAC: The baseline value is the EER of the retired unit.

$$\Delta kWh = CAPY \times \left( \frac{1}{EER_{RetRAC}} - \frac{1}{EER_{ee}} \right) \times EFLH_{RAC}$$

$$\Delta kWh_{summer\ peak} = CAPY \times \left( \frac{1}{EER_{RetRAC}} - \frac{1}{EER_{ee}} \right) \times CFCF_{summer}$$

$$\Delta kWh_{winter\ peak} = 0$$

**After the RUL for (EUL-RUL) years:** The baseline EER would revert to the minimum Federal appliance standard CEER. RAC units have a “CEER” rating in addition to an “EER”. CEER is the “Combined Energy Efficiency Ratio”, which incorporates standby power into the calculation. This will be the value used in the  $\Delta kWh$  calculation.

$$\Delta kWh = CAPY \times \left( \frac{1}{CEER_{base}} - \frac{1}{CEER_{ee}} \right) \times EFLH_{RAC}$$

$$\Delta kWh_{summer\ peak} = CAPY \times \left( \frac{1}{CEER_{base}} - \frac{1}{CEER_{ee}} \right) \times CFCF_{summer}$$

$$\Delta kWh_{winter\ peak} = 0$$

**DEFINITION OF TERMS**

**DEFINITION OF TERMS**

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**Table 2-33: Terms, Values, and References for Room AC Retirement**

Term	Unit	Value	Sources
$EFLH_{RAC}$ , Equivalent Full-Load Hours of operation for the installed measure. In actuality, the number of hours and time of operation can vary drastically depending on the RAC location (living room, bedroom, home office, etc.).	$\frac{hours}{yr}$	See $EFLH_{RAC}$ in Vol. 1, App. A	4
$CAPY$ , Rated cooling capacity (size) of the RAC unit.	$\frac{kBTU}{h}$	EDC Data Gathering Default: 7.5	3
$EER_{RetRAC}$ , The Energy Efficiency Ratio of the unit being retired-recycled. <sup>34</sup>	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: 9.8	4
$EER_{eet}$ , The Energy Efficiency Ratio for an ENERGY STAR RAC	$\frac{BTU}{W \cdot h}$	12.1	6
$CEER_{base}$ , (for a 8,000-BTU/h unit), The Combined Energy Efficiency Ratio of a RAC that meets the minimum federal appliance standard efficiency.	$\frac{BTU}{W \cdot h}$	11.0	5
$CEER_{eet}$ , (for a 8,000-BTU/h unit), The Combined Energy Efficiency Ratio for an ENERGY STAR RAC.	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default=12.1	5
$CF$ , Demand Coincidence Factor	Proportion	See CF in Vol. 1, App. A	2

**Table 2-29: RAC Retirement-Only EFLH and Energy Savings by City**

Climate Region	Reference City	Energy Impact (kWh)	Demand Impact (kW)
C	Allentown	136.2	0.271
A	Binghamton, NY	78.8	0.203
G	Bradford	49.0	0.167
I	Erie	111.0	0.203
E	Harrisburg	173.7	0.345
D	Philadelphia	185.2	0.324
H	Pittsburgh	129.3	0.282
B	Scranton	112.5	0.249
F	Williamsport	132.4	0.299

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

<sup>34</sup>Note that this value is the EER value, as CEER were introduced later.

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<u>CAPY</u> , Rated cooling capacity (size) of the RAC unit.	$\frac{kBTU}{h}$	EDC Data Gathering Default: 7.2	EDC Data Gathering 2
<u>EER<sub>RetRAC</sub></u> , The Energy Efficiency Ratio of the unit being retired-recycled	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: 9.8	EDC Data Gathering 2
<u>EFLH<sub>RAC</sub></u> , Equivalent Full Load Hours of operation for the installed measure. In actuality, the number of hours and time of operation can vary drastically depending on the RAC location (living room, bedroom, home office, etc.).	$\frac{hours}{yr}$	See <u>EFLH<sub>RAC</sub></u> in Vol. 1, App. A	3
<u>CF<sub>Summer</sub></u> , Demand Coincidence Factor during the summer months	Proportion	See <u>CF</u> in Vol. 1, App. A	3
<u>EER<sub>ee</sub></u> , The Energy Efficiency Ratio for an energy efficient RAC	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	EDC Data Gathering
<u>CEER<sub>base</sub></u> , Combined Energy Efficiency ratio of the baseline unit	$\frac{BTU}{W \cdot h}$	Federal Standard Values in Table 2-30: RAC (without reverse cycle) Federal Minimum CEER Standards Table 2-30, Table 2-31, or Table 2-32 Default = 16.0	4
<u>CEER<sub>ee</sub></u> , Combined Energy efficiency ratio of the RAC being installed	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	EDC Data Gathering

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### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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### SOURCES

- 1) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.
- 1) California Electronic Technical Reference Manual. "Room Air Conditioner, Residential". Accessed August 2023. Weblink
- 2) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study, Sec 8.2.2 Table 104. Statewide average for all housing types. Weblink

- 2)3) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/Weblink>, and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)
- 3) ~~Mid Atlantic TRM Version 7.0, May, 2017. Prepared by Vermont Energy Investment Corporation. An adjustment to the ES RAC EFLHs of 31% was used for the "Window A/C" measure. The average ratio of EFLH for Room AC provided in RLW Report: Final Report Coincidence Factor Study Residential Room Air Conditioners, June 23, 2008 ([http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117\\_RLW\\_CF\\_%20Res%20RAC.pdf](http://www.puc.nh.gov/Electric/Monitoring%20and%20Evaluation%20Reports/National%20Grid/117_RLW_CF_%20Res%20RAC.pdf)) to FLH for Central Cooling for the same location (provided by AHRI: [http://www.energystar.gov/ia/business/bulk\\_purchasing/bpsavings\\_calc/Calc\\_CAC.xls](http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/Calc_CAC.xls) is 31%. This factor was applied to the EFLH for Central Cooling provided for PA cities and averaged to come up with the assumption for EFLH for Room AC." [https://neep.org/sites/default/files/resources/Mid\\_Atlantic\\_TRM\\_V7\\_FINAL.pdf](https://neep.org/sites/default/files/resources/Mid_Atlantic_TRM_V7_FINAL.pdf)~~
- 4) ~~Statewide average capacity of RAC units, Pennsylvania Act 129-2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf).~~
- 4) ~~Minimum Federal Standard for most common room AC type (8000-14,999 capacity range with louvered sides) per federal standards from 10/1/2000 to 5/31/2014. Note that this value is the EER value, as CEER were introduced later. Federal code of regulation. Room air conditioners. 10 C.F.R. § 430.32 (b)(2). Weblink~~

### 2.2.9 WINDOW HEAT PUMP

- 5) \_\_\_\_\_
- 6) ~~ENERGY STAR Program Requirements Product Specification for Room Air Conditioners, Eligibility Criteria Version 4.1. October 26, 2015.  
[https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%204.1%20Room%20Air%20Conditioners%20Specification\\_0.pdf](https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%204.1%20Room%20Air%20Conditioners%20Specification_0.pdf)~~

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### 2.2.9 DUCT SEALING & DUCT INSULATION

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Window Heat Pump
<b>Measure Life</b>	9 years <sup>Source 1</sup>
<b>Vintage</b>	Early Replacement

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Window heat pumps for single-room applications could provide an energy-and-cost saving alternative to built-in or portable electric resistance heating in the residential market. Window heat pumps are more energy-efficient than resistance heaters because of their ability to extract thermal energy from the environment that is freely available.

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#### ELIGIBILITY

This protocol documents the energy savings attributed to window heat pumps. Eligible equipment must meet direct-install requirements. The baseline heating system could be:

- 1) Existing electric resistance heating
- 2) Electric space heaters used as the primary heating source when fossil fuel (other than natural gas) heating systems failed (referred to as de facto heating)
  - a. This baseline is for participants with broken-beyond-repair oil heating systems who are heating their homes with portable electric space heaters.
- 3) Electric furnace

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Cooling savings may be claimed if the window heat pump exceeds efficiency criteria prescribed by federal standards.

#### ALGORITHMS

The energy savings algorithms depend on three main factors: baseline condition, usage (secondary heating system), and the capacity of the unit.

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{heat} = CAPY_{heat} \times \frac{1}{3.412} \times \left( \frac{OF_{hea}}{COP_{base}} - \frac{1}{COP_{ee}} \right) \times EFLH_{heat,HP}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \left( \frac{1}{CEER_{base}} - \frac{1}{CEER_{ee}} \right) \times EFLH_{RAC}$$

$$\Delta kW_{peak\ summer} = CAPY_{cool} \times \left( \frac{1}{CEER_{base}} - \frac{1}{CEER_{ee}} \right) \times CF_{summer}$$

$$\Delta kW_{peak\ winter} = 0$$

#### Baseline: Spaceheater(s), Electric Baseboards

EDCs may collect information about the capacity of the existing space heaters, electric furnaces, or electric baseboards. Capacity is determined using the total wattage of electric heat in use, where  $OF_{heat}$  is the ratio of the existing electric capacity to the capacity of the new equipment:

$$OF_{heat} = \frac{\sum kW_{spaceheat} \times 3.412 \frac{BTU}{Wh}}{CAPY_{Heat}}$$

#### DEFINITION OF TERMS

**Table 2-34: Terms, Values, and References for Window Heat Pumps**

Term	Unit	Value	Sources
$CAPY_{heat}$ , The heating capacity of the heat pump being installed	$kBTU/hr$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CAPY_{cool}$ , The cooling capacity of the heat pump being installed	$kBTU/hr$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CEER_{base}$ , Combined Energy Efficiency ratio of the baseline unit	$\frac{BTU}{W \cdot h}$	Federal Standard Values in Table 2-37	2
$CEER_{ee}$ , Combined Energy efficiency ratio of the window heat pump (WHP) being installed	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	EDC Data Gathering
$COP_{base}$ , Heating Seasonal Performance Factor of the Baseline Unit	Proportion	EDC Data Gathering	EDC Data Gathering
		Default: Table 2-35	3
$COP_{ee}$ , Heating Seasonal Performance Factor of the unit being installed	Proportion	EDC Data Gathering	AEPS Application; EDC Data Gathering
$OF_{heat}$ , Oversize factor	None	EDC Data Gathering	EDC Data Gathering
		Default: Table 2-36	4
$EFLH_{RAC}$ , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See $EFLH_{cool}$ in Vol. 1, App. A	5
$EFLH_{heat,HP}$ , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See Table 2-38	6
$CF_{summer}$ , Demand Coincidence Factor during the summer months	Proportion	See CF in Vol. 1, App. A	5
$CF_{winter}$ , Demand Coincidence Factor during the winter months	Proportion	See CF in Vol. 1, App. A	5

**Table 2-35: Default Baseline Equipment Efficiency**

	Early Replacement
Baseline Equip.	$COP_{base}$
Elec. Baseboard	1.00
Elec. Furnace	0.95
Space Heaters	1.00

**Table 2-36: Oversize Factors for High Efficiency Equipment**

	Electric Baseboard	Electric Furnace	Space Heaters
$OF_{heat}$	1.0	1.0	0.5

**Table 2-37: Reverse-Cycle RAC Federal Minimum Efficiency Standards**

Capacity (kBTU/h)	Federal Standard CEER, with louvered sides	Federal Standard CEER, without louvered sides
< 14	n/a	13.7
≥ 14		12.8
< 20	14.4	n/a
≥ 20	13.7	

**Table 2-38: EFLH<sub>heat,HP</sub> for Window Heat Pumps**

Climate Region	Reference City	EFLH <sub>heat,HP</sub>
C	Allentown	219
A	Binghamton, NY	171
G	Bradford	164
I	Erie	209
E	Harrisburg	238
D	Philadelphia	257
H	Pittsburgh	211
B	Scranton	201
F	Williamsport	208

**DEFAULT SAVINGS**

There are no default savings for this measure.

**EVALUATION PROTOCOLS**

For most installation, the appropriate evaluation protocol is to verify installation coupled with assignment of stipulated energy savings. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- 1) California Electronic Technical Reference Manual. "Room Air Conditioner, Residential". Accessed March 2024. Weblink.
- 2) Federal code of regulation. Room air conditioners. 10 C.F.R. § 430.32 (b)(2). Weblink
- 3) Using the relation  $HSPF=COP \times 3.412$ , where  $HSPF = 3.412$  for electric resistance heating. Electric furnace efficiency typically varies from 0.95 to 1.00, therefore a COP of 0.95 equates to an HSPF of 3.241.
- 4) Assumptions used to calculate a default value for de facto heating system oversize factor: A 1500W portable electric space heater in use in the home with capacity of  $1.5kW \times 3412 \frac{BTU}{kWh} = 5,118 BTU/h$ , replaced by window heat pump with heating capacity of 10,000 Btu/h,  $OF = \frac{5,118}{10,000} \approx 0.5$ .

- 5) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)
- 6) At outdoor air temperatures below 40°F, window heat pumps switch from heat pump heating to electric resistance heating. (Weblink).  $EFLH_{heat,HP}$  values are calculated by multiplying Secondary HP  $EFLH_{heat}$  values presented in Volume 1 Appendix A by the ratio of annual heating degree hours (base 65°F) during times when outdoor air temperature is between 40°F and 65°F and the annual heating degree hours (base 65°F) during all times when outdoor air temperature is below 65°F.



**2.2.10 DUCT SEALING & DUCT INSULATION**

<b>Target Sector</b>	<u>Residential</u>
<b>Measure Unit</b>	Duct Sealing and/or Insulation Project
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

This measure describes evaluating the savings associated with performing duct sealing using mastic sealant or metal tape to the distribution system of homes with either central air conditioning or a ducted heating system. The measure also applies to insulating ductwork in unconditioned and semi-conditioned spaces of residential buildings.

If duct insulation is involved with the improvement, the first method, "Evaluation of Distribution Efficiency," must be used to estimate energy savings.

- 1) **Evaluation of Distribution Efficiency** – this methodology requires the evaluation of three duct characteristics below, and use of the Building Performance Institute’s (BPI) "Guidance on Estimating Distribution Efficiency",<sup>Source 2</sup> which are summarized in ~~Table 2-31~~Table 2-40 and ~~Table 2-41~~ for convenience.
  - a. Duct location, including percentage of duct work found within the conditioned space
  - b. Duct leakage evaluation. The duct leakage assessment values are based on an assumption of 6.5% of assumed air handler flow (tight); 21% (average); or 35% (leaky).<sup>Source 7</sup>~~Source 6~~
  - c. Duct insulation evaluation
- 2) **RESNET Test 380 4.4.2** – this method involves the pressurization of the house to 25 Pascals with reference to outside and a simultaneous pressurization of the duct system to reach equilibrium with the envelope or inside pressure of zero Pascals. A blower door is used to pressurize the building to 25 Pascals with reference to outside, when that is achieved the duct blaster is used to equalize the pressure difference between the duct system and the house. The amount of air required to bring the duct system to zero Pascals with reference to the building is the amount of air leaking through the ductwork to the outside. This technique is described in detail in section 4.4.2 of the ANSI/RESNET/ICC 380 - 2016 Standards: <http://www.resnet.us/professional/standards>

Field Code Changed

**ELIGIBILITY**

The efficient condition is sealed duct work throughout the unconditioned space in the home. The existing baseline condition is leaky duct work within the unconditioned space in the home.

**ALGORITHMS**

**Methodology 1: Evaluation of Distribution Efficiency**

Determine Distribution Efficiency by evaluating duct system before and after duct sealing using Building Performance Institute "Guidance on Estimating Distribution Efficiency" or the values reproduced from that document in ~~Table 2-31~~Table 2-40 that match the duct system, and if the majority of the duct system is in conditioned space add the matching value from Table 2-41, not to exceed 100%.

$$\Delta kWh_{cooling} = \frac{\left(\frac{DE_{post(cool)}}{DE_{pre(cool)}} - \frac{DE_{pre(cool)}}{DE_{post(cool)}}\right) \left(1 - \frac{DE_{pre(cool)}}{DE_{post(cool)}}\right) \times EFLH_{cool} \times CAPY_{cool}}{SEER-SEER2}$$

$$\Delta kWh_{heating} = \frac{\left(\frac{DE_{post(heat)}}{DE_{pre(heat)}} - \frac{DE_{pre(heat)}}{DE_{post(heat)}}\right) \times EFLH_{heat} \left(1 - \frac{DE_{pre(heat)}}{DE_{post(heat)}}\right) \times EFLH_{heat} \times CAPY_{heat}}{HSPFHSPF2}$$

**Methodology 2: RESNET Test 803.7**

- a) Determine Duct Leakage rate before and after performing duct sealing

$$\Delta CFM_{25DB} = CFM_{25BASE} - CFM_{25EE}$$

- b) Calculate Energy Savings

$$\Delta kWh/yr_{cooling} = \frac{\left(\frac{\Delta CFM_{25DB}}{CAPY_{cool} \times TCFM} \times EFLH_{cool} \times CAPY_{cool}\right)}{SEERSEER2}$$

$$\Delta kWh/yr_{heating} = \frac{\left(\frac{\Delta CFM_{25DB}}{CAPY_{heat} \times TCFM} \times EFLH_{heat} \times CAPY_{heat}\right)}{HSPFHSPF2}$$

**Summer Coincident Peak Demand Savings**

$$\Delta kW_{summer\ peak} = \frac{\Delta kWh_{cooling}}{EFLH_{cool}} \times CF_{summer} \times \frac{\Delta kWh_{cooling}}{EFLH_{cool}} \times CF_{summer}$$

$$\Delta kW_{winter\ peak} = \frac{\Delta kWh_{heating}}{EFLH_{heat}} \times CF_{winter}$$

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**DEFINITION OF TERMS**

Table 2-39: Terms, Values, and References for Duct Sealing

Term	Unit	Value	Source
$CF_{summer}$ , Demand Coincidence Factor during the summer months	Proportion	See CF in Vol. 1, App. A	4
$CF_{winter}$ , Demand Coincidence Factor during the winter months	Proportion	See CF in Vol. 1, App. A	4
$CFM_{25BASE}$ , Standard Duct Leakage test result at 25 Pascal pressure differential of the duct system prior to sealing, calculated from the duct blaster fan flow chart	$\frac{ft^3}{min}$	EDC Data Gathering	3
$CFM_{25DB}$ , Cubic feet per minute of air leaving the duct system at 25 Pascals	$\frac{ft^3}{min}$	EDC Data Gathering	3

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Term	Unit	Value	Source
$CFM_{25SE}$ , Standard Duct Leakage test result at 25 Pascal pressure differential of the duct system after sealing, calculated from the duct blaster fan flow chart	$\frac{ft^3}{min}$	EDC Data Gathering	3
$CAPY_{cool}$ , Capacity of Air Cooling System	$kBTU/hr$	EDC Data Gathering	EDC Data Gathering
$CAPY_{heat}$ , Capacity of Air Heating System	$kBTU/hr$	EDC Data Gathering	EDC Data Gathering
$TCFM$ , Conversion from tons of cooling to CFM	$\frac{CFM}{ton}$	400	<a href="#">5Conversion factor</a>
<a href="#">SEER2</a> , $SEER$ , Efficiency of cooling equipment	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: See Early Replacement values in Table 2-10 in Sec. 2.2.1	<a href="#">65</a>
<a href="#">HSPF2</a> , $HSPF$ , Efficiency of Heating Equipment	None	EDC Data Gathering Default: See Early Replacement values in Table 2-10 in Sec. 2.2.1	<a href="#">65</a>
$EFLH_{cool}$ , Cooling equivalent full load hours	$\frac{hours}{year}$	See $EFLH_{cool}$ in Vol. 1, App. A	4
$EFLH_{heat}$ , Heating equivalent full load hours	$\frac{hours}{year}$	See $EFLH_{heat}$ in Vol. 1, App. A	4
$DE_{post}$ , Distribution efficiency after duct sealing and insulation	None	<a href="#">Table 2-31, Table 2-32</a> Table 2-40, Table 2-41 Not to exceed 100%	2
$DE_{pre}$ , Distribution efficiency before duct sealing and insulation	None	<a href="#">Table 2-31, Table 2-32</a> Table 2-40, Table 2-41 Not to exceed 100%	2

Note: Where appropriate, nameplate data collected for usage in savings calculations (i.e., SEER, EER, HSPF) should be converted to new efficiency metrics (i.e., SEER2, EER2, HSPF2) using conversion equations laid out in Vol. 1 App. A

**Table 2-40: Distribution Efficiency by Climate Zone; Conditioned Air Type; Duct Location, Leakage & Insulation**

Insulation	Location	Attic				Basement				Vented Crawl			
	HVAC Type	Heat		Cool		Heat		Cool		Heat		Cool	
	Leakage \ CZ*	4&5	6	4&5	6	4&5	6	4&5	6	4&5	6	4&5	6
R-0	Leaky	69%	64%	61%	61%	93%	92%	81%	92%	74%	71%	76%	90%
	Average	73%	68%	64%	66%	94%	94%	87%	95%	78%	74%	83%	93%
	Tight	77%	73%	73%	74%	95%	95%	94%	98%	82%	78%	91%	97%
R-2	Leaky	76%	73%	65%	67%	94%	94%	83%	92%	80%	78%	78%	91%
	Average	82%	79%	74%	75%	96%	95%	88%	95%	85%	83%	85%	94%
	Tight	87%	85%	84%	85%	97%	97%	95%	98%	90%	88%	93%	97%
R-4+	Leaky	79%	76%	67%	70%	95%	95%	83%	93%	82%	80%	79%	91%
	Average	84%	82%	77%	78%	96%	96%	89%	95%	87%	85%	86%	94%
	Tight	90%	89%	87%	88%	98%	98%	95%	98%	92%	91%	94%	97%
R-8+	Leaky	80%	78%	69%	71%	95%	95%	83%	93%	84%	82%	79%	91%
	Average	86%	84%	79%	80%	97%	97%	89%	95%	89%	87%	87%	94%
	Tight	92%	91%	90%	90%	98%	98%	95%	98%	94%	93%	94%	98%

\* Climate Regions A and G correspond to IECC Climate Zone 6, the rest of the state is IECC Climate Zone 4 or 5.

**Table 2-41: Distribution Efficiency Adders for Cond. Space (%) by Conditioned Air; Duct Location, Leakage & Insulation**

Location	Attic				Basement				Vented Crawl			
HVAC Type	Heat		Cool		Heat		Cool		Heat		Cool*	
Insulation \ Conditioned	50%	80%	50%	80%	50%	80%	50%	80%	50%	80%	50%	80%
R-0	6%	41%	14%	9%	2%	32%	23%	3%	6%	31%	13%	5%
R-2	4%	56%	65%	7%	1%	1%	1%	2%	3%	25%	52%	3%
R-4+	3%	34%	43%	5%	1%	1%	1%	1%	2%	44%	41%	3%
R-8+	3%	23%	32%	3%	1%	1%	1%	1%	2%	42%	21%	2%

\* In Climate Zone 6 (Climate Regions A & G), the cooling adder is fixed at 1% for ductwork in 80% conditioned space.

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- ~~1) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020. <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018. Limited to Act 129 maximum of 15 years.~~
- 1) California Electronic Technical Reference Manual. "Duct Sealing". Residential. Accessed August 2023. (Capped at 15 years in accordance with Act 129) Weblink
- 2) Building Performance Institute. (n.d.). Distribution Efficiency Table. <http://www.bpi.org/sites/default/files/Guidance%20on%20Estimating%20Distribution%20Efficiency.pdf>Weblink. (Reproduced by permission.)

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- 3) ~~Resnet Energy Services Network, (2012, May 12). Standard for Testing Airtightness of Building, Dwelling Unit, and Sleeping Unit Enclosures: Airtightness of Heating and Cooling Air Distribution Systems; and Airflow of Mechanical Ventilation Systems Standards for Performance Testing, <http://www.resnet.us/blog/wp-content/uploads/2016/01/ANSI-RESNET-ICC-380-2016-posted-Weblink>~~
- 3)4) ~~Based on website 6- the Phase III SWE team's analysis of regional HVAC runtime data collected from Ecobee's Donate Your Data research service. Weblink Updated based on the latest CDD and HDD values from NOAA's 15-16.pdf year annual climate Normals (2006–2020). Weblink~~
- 4) ~~Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/>~~
- 5) ~~Heating, Air conditioning & Refrigeration Distributors International <https://energy.mo.gov/sites/energy/files/61-why-400-cfm-per-ton.pdf>~~
- 6)5) ~~Pennsylvania Act 129-2018 Residential Baseline Study, <http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3-Res-Baseline-Study-Rpt021219.pdf>. NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Sec 8.1.4 Table 87 and Sec 8.2.1 Table 97 & 98. Baseline findings are capped to current Federal Standards. Weblink (Due to small sample sizes, GSHP is lowest efficiency value from BEopt v2.8.0, and PTAC and PTHP are minimum federal standard efficiencies.)~~
- 7)6) ~~Communication with Building Performance Institute.~~

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### 2.2.102.2.11 AIR HANDLER FILTER WHISTLES

Target Sector	Residential Establishments
Measure Unit	Filter whistle (to promote regular filter change-out)
Measure Life	5 years <sup>Source 61</sup>
Vintage	Retrofit

Dirty air handler filters increase electricity consumption for the circulating fan. Filter whistles attach to the filter in the air handler, and make a sound when it is time to replace the filter.<sup>Source 72</sup>

#### ELIGIBILITY

Savings estimates are based on reduced blower fan motor power requirements for winter and summer use of the blower fan motor. This air handler filter whistle measure applies to central forced-air furnaces, central AC and heat pump systems. Where homes do not have A/C or heat pump systems for cooling, only the annual heating savings will apply.

#### ALGORITHMS

$$\Delta kWh = \Delta kWh_{heat} + \Delta kWh_{cool}$$

$$\Delta kWh_{heat} = kW_{motor} \times EFLH_{heat} \times EI \times ISR$$

$$\Delta kWh_{cool} = kW_{motor} \times EFLH_{cool} \times EI \times ISR$$

$$\Delta kWh_{summer\ peak} = \Delta kWh_{cool} \div EFLH_{cool} \times CF_{summer}$$

$$\Delta kWh_{winter\ peak} = \Delta kWh_{heat} \div EFLH_{heat} \times CF_{winter}$$

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#### DEFINITION OF TERMS

Table 2-42: Terms, Values, and References for Air Handler Filter Whistle

Term	Unit	Value	Sources
$kW_{motor}$ , Average motor full load electric demand	$kW$	0.377	43
$EFLH_{heat}$ , Estimated Full Load Hours (Heating)	$\frac{hours}{yr}$	See $EFLH_{heat}$ in Vol. 1, App. A	54
$EFLH_{cool}$ , Estimated Full Load Hours (Cooling)	$\frac{hours}{yr}$	See $EFLH_{cool}$ in Vol. 1, App. A	54
$EI$ , Efficiency Improvement	%	15%	2, 4, 5, 6
$ISR$ , In-service Rate	%	EDC Data Gathering Default = 157%	37
$CF_{summer}$ , Demand Coincidence Factor during the summer months	Proportion	See $CF$ in Vol. 1, App. A	54
$CF_{winter}$ , Demand Coincidence Factor during the winter months	Proportion	See $CF$ in Vol. 1, App. A	4

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**DEFAULT SAVINGS**

The following table presents the assumptions and the results of the deemed savings for each reference location.

Table 2-43: Default Air Handler Filter Whistle Savings

Climate Region	Reference City		Heating		Cooling		
			ASHP kWh	Furnace kWh	ASH P kWh Winter kWh	Summer kWh	
C	Allentown	7.7	10.5	4.975	3.27	3.01	0.0017
A	Binghamton, NY			9.86.00	12.74.63	1.53	0.0020.010
G	Bradford			6.12	11.4.71	1.721	0.0020.009
I	Erie			8.95.27	12.13.74	2.48	0.0020.012
E	Harrisburg			8.54.53	11.23.10	3.40	0.0040.017
D	Philadelphia			6.54.07	9.2.70	3.85	0.0040.019
H	Pittsburgh			8.05.00	10.83.51	2.65	0.0030.015
B	Scranton			8.5.09	11.43.59	2.58	0.0030.014
F	Williamsport			7.95.06	10.93.60	2.62	0.0030.016

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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**SOURCES**

- 1) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020
- 2) Your Filter Connection, "What is a Furnace Filter Whistle?". Weblink. Accessed December, 2018.
- 3) Typical blower motor capacity for gas furnace is 1/4 to 3/4 HP, 1/2 HP x 0.746 <sup>kW</sup>/<sub>hp</sub> = 0.377kW.

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with

verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

- 1) Typical blower motor capacity for gas furnace is  $\frac{1}{4}$  to  $\frac{3}{4}$  HP,  $\frac{1}{2}$  HP  $\times$   $0.746 \frac{\text{kW}}{\text{HP}} = 0.377 \text{kW}$ .
- 4) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)
- 5) US DOE Office of Energy Efficiency and Renewable Energy – "Energy Savers" publication – "Clogged air filters will reduce system efficiency by 30% or more." Savings estimates assume the 30% quoted is the worst case and typical households will be at the median or 15% that is assumed to be the efficiency improvement when furnace filters are kept clean.
- 3) The In Service Rate is the average of values reported by FirstEnergy EDCs for kits including an air handler furnace whistle for PY9. See [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/electric\\_distribution\\_company\\_act\\_129\\_reporting\\_requirements.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/electric_distribution_company_act_129_reporting_requirements.aspx)
- 6) Energy.gov. "Maintaining Your Air Conditioner". Accessed 7/16/2014. Says that replacing a dirty air filter with a clean one can lower total air conditioner energy consumption by 5-15%. Since the algorithms in this measure only take into account the blower fan energy use, a 15% savings seems reasonable.
- 5) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected weighted average of ISRs from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/>.
- 6) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.
- 7) Your Filter Connection, "What is a Furnace Filter Whistle?" <https://yourfilterconnection.com/blogs/help/what-is-a-furnace-filter-whistle>. Accessed December, 2018 surveys of FirstEnergy customers that received air handler filter whistles in kits in PY13 and PY14.

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**2-2.112.2.12 ENERGY STAR® CERTIFIED CONNECTED THERMOSTATS**

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<b>Target Sector</b>	Residential Homes, including single or multifamily in-unit spaces
<b>Measure Unit</b>	Residential Thermostat
<b>Measure Life</b>	11.9 years <sup>Source 61</sup>
<b>Vintage</b>	Retrofit, Replace on Burnout, or <del>new construction</del> <u>New Construction</u>

ENERGY STAR®-certified connected thermostats (CT) save heating and cooling energy by operating residential HVAC systems more efficiently. CTs that meet the ENERGY STAR® ~~specification~~specification<sup>Source 2</sup> will have functions that are located in the home and on the Internet (the cloud). Homes must have Wi-Fi to enable full operating capabilities.

ENERGY STAR®-certified connected thermostats may replace either a manual thermostat or a conventional programmable thermostat. The energy savings assume an existing ducted HVAC system with either an air source heat pump, fossil fuel heating with central AC, or an electric furnace with central AC. Electric resistance baseboard heating as the primary heating system is not eligible for savings to be claimed through this measure protocol because CTs are low voltage thermostats, which use 24 volts. Electric baseboard heating requires line-voltage thermostats, which can be either 120 or 240 volts.

**ELIGIBILITY**

This measure documents the energy savings resulting from the following product installations:

- ENERGY STAR®-certified connected thermostat (CT)

Savings are assessed in this protocol for three different installation scenarios:

- 1) **Customer self-installation of CT (no education).**  
 Under this scenario, customers purchase and install the CT on their own without any education on installing and operating the thermostat (aside from any manufacturer instructions included in the CT box at the time of purchase). This scenario applies to upstream programs where EDCs discount the device cost at the point of purchase.
- 2) **Customer self-installation with education on installation and operation of CT.**  
 Under this scenario, customers purchase the program-qualified CT and, in order to receive the incentive, certify in the incentive application that they have completed the specified education on how to install and operate the thermostat. The education may consist of viewing of videos and/or completion of a short online training module on the installation and operational details of the thermostat.
- 3) **Professional installation with instructions on operating the CT.**  
 For professional installation with operational instructions, the thermostat must be installed by a utility representative, ICSP, or program affiliated trade ally, at the time of the installation, the installer must explain the operational details of the thermostat to the customer. It is important to note that professional installation by contractors unaffiliated with the program may not focus on the energy savings capabilities of the device and would not produce higher savings. For example, an electrician might only focus on the wiring needs and provide little or no direction to the homeowner on how to leverage device capabilities for energy savings.

**Table 2-44: Installation Classification**

Installation Scenario	Installation Cost Paid By	Installation Type	Capacity Term(s)
Thermostat installed by EDC contractor during audit or other visit	EDC	Professional	EDC Data Gathering, Default
Thermostat installed by contractor affiliated with EDC program (ICSP or trade ally)	EDC or Participant	Professional	EDC Data Gathering, Default
Thermostat installed by licensed electrical or HVAC contractor - invoice, work order, etc. provided	Participant	Professional	EDC Data Gathering, Default
Thermostat installed by homeowner or friend/family who certifies receiving education on operating the thermostat at the time of applying for the rebate.	Participant	Self-Installation + Education	Default
Thermostat installed by licensed electrical or HVAC contractor - no invoice, work order or other documentation supplied	Participant	Self-Installation + Education	Default
Thermostat installed by homeowner or friend/family	Participant	Self-Installation	Default

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Finally, energy saving factor (ESF) values are specified based on whether the thermostat is installed by the customer (self-installation), the customer with education (self-installation + education), or by a professional contractor/utility representative (professional installation). A peak demand saving factor (PDSF) is applied to the  $ESF_{cool}$  [assumption](#) and  $ESF_{heat}$  [assumptions](#) so the peak demand savings values per thermostat also vary by installation type.

**ALGORITHMS**

**Energy Savings**

Total savings are calculated as a combination of heating and cooling season savings. The heating savings calculation varies depending on whether heat is provided by a heat pump, electric furnace, or gas furnace. There are no heating savings for boilers.

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{cool} = CAPY_{cool} \times \frac{EFLH_{cool}}{SEER \times Eff_{duct}} \times \frac{EFLH_{cool}}{SEER2 \times Eff_{duct}} \times ESF_{cool}$$

$$\Delta kWh_{heat,HP} = CAPY_{HP} \times \frac{EFLH_{heat,HP}}{HSPF \times Eff_{duct}} \times \frac{EFLH_{heat,HP}}{HSPF2 \times Eff_{duct}} \times ESF_{heat}$$

$$\Delta kWh_{heat,elecurn} = CAPY_{elecurn} \times \frac{EFLH_{heat,non-HP}}{3.412 \frac{Btu}{Wh} \times Eff_{duct}} \times \frac{EFLH_{heat,non-HP}}{HSPF \times Eff_{duct}} \times ESF_{heat}$$

$$ESF_{heat} \times DF$$

$$\Delta kWh_{heat,fueurn} = \frac{HP_{motor} \times 0.746 \frac{kW}{HP}}{\eta_{motor}} \times EFLH_{heat,non-H} \times ESF_{heat}$$

**Derate Factor**

Heating ESF estimates are largely based on results from studies looking at connected thermostats applied to natural gas furnaces. However, it is likely that customers with electric furnaces are already more conscious of managing their energy consumption than those with gas furnaces due to the higher cost of electric resistance heat, thus savings from a gas furnace study may be overstated if not adjusted.

**Blended Baseline**

The ESF value applied in the equations above is determined based on the type of thermostat being replaced (manual, programmable, or unknown baseline), the existing heating and/or cooling HVAC equipment in the home, and the program design type. When a known blended baseline of manual and programmable thermostats is present, the following equation may be used to find the appropriate ESF value for the blended baseline.

$$ESF_{connected\ over\ mixed} = (ESF_{connected\ over\ manual} \times \%Manual) + (ESF_{connected\ over\ prog.} \times \%Programmable)$$

**Demand Savings**

Savings from connected thermostats installed in systems with ducted air conditioning and/or heating have been shown to generally follow cooling and/or heating load, however the percent reduction during the system peak hours is expected to be lower than during off-peak hours. The PDSF term reduces the  $ESF_{cool}$  value and  $ESF_{heat}$  values used to calculate energy savings by 50%. Peak demand savings are a function of the system size, efficiency, installation type, and coincidence factor.

$$\Delta kW_{peak} = \frac{kW_{summer\ peak}}{EER \times Eff_{duct}} \times \frac{CAPY_{cool}}{EER2 \times Eff_{duct}} \times PDSF \times GFCF_{summer}$$

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For Heat Pumps:

$$\Delta kW_{winter\ peak} = \frac{\Delta kW h_{heat,HP}}{EFLH_{heat,HP}} \times PDSF \times CF_{winter}$$

For Non-heat Pumps:

$$\Delta kW_{winter\ peak} = \frac{\Delta kW h_{heat,elec\ furn/fuel\ furn}}{EFLH_{heat,non-HP}} \times PDSF \times CF_{winter}$$

**DEFINITION OF TERMS**

Table 2-45: Residential Electric HVAC Calculation Assumptions

Term	Unit	Value	Sources
CAPY <sub>cool</sub> , Capacity of air conditioning unit	$\frac{kBTU}{h}$	EDC Data Gathering of Nameplate data	EDC Data Gathering
		Default = 3031.9 / unit	43
CAPY <sub>HP</sub> , Normal heat capacity of Heat Pump System.	$\frac{kBTU}{h}$	EDC Data Gathering of Nameplate Data	EDC Data Gathering
		Default = 3231.9 / unit	43
CAPY <sub>electurn</sub> , Normal heat capacity of Electric Furnace systems	$\frac{kBTU}{h}$	EDC Data Gathering of Nameplate data	EDC Data Gathering
		Default = 60,24978.1 / unit	43
SEERSEER <sub>2</sub> , Seasonal Energy Efficiency Ratio	$\frac{BTU}{W \cdot h}$	EDC Data Gathering of Nameplate data	EDC Data Gathering

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Term	Unit	Value	Sources
		Default: <del>CAC = 12.4</del> <del>Heat Pump = 13.5</del> see Table 2-10	<del>43</del>
<del>EER</del> <del>EER<sub>2</sub></del> , Energy Efficiency Ratio	<del>BTU</del> <del>W · h</del>	EDC Data Gathering of Nameplate data Default: <del>CAC = 10.6</del> <del>Heat Pump = 11.4</del> see Table 2-10	EDC Data Gathering <del>43</del>
<del>HSPF</del> <del>heat pump</del> <del>HSPF<sub>2</sub></del> , <del>HSPF</del> , Heating Seasonal Performance Factor of Heat Pump	<del>BTU</del> <del>W · h</del>	EDC Data Gathering of Nameplate data <del>Heat Pump</del> Default = <del>8.2</del> see Table 2-10	EDC Data Gathering <del>43</del>
<del>Eff<sub>duct</sub></del> , Duct System Efficiency	<del>None</del>	<del>0.883</del>	<del>34</del>
<del>EFLH<sub>cool</sub></del> , Equivalent Full Load Hours for Cooling	<del>hours</del> <del>yr</del>	See <del>EFLH<sub>cool</sub></del> in Vol. 1, App. A	<del>45</del>
<del>EFLH<sub>heat,HP</sub></del> , Equivalent Full Load Hours for ASHP Systems	<del>hours</del> <del>yr</del>	See <del>EFLH<sub>heat,HP</sub></del> in Vol. 1, App. A	<del>45</del>
<del>EFLH<sub>heat,non-HP</sub></del> , Equivalent Full Load Hours for Electric or Gas Furnaces	<del>hours</del> <del>yr</del>	See <del>EFLH<sub>heat,non-HP</sub></del> in Vol. 1, App. A	<del>45</del>
<del>HP<sub>motor</sub></del> , Gas furnace blower motor horsepower	<del>Hp</del> <del>HP</del>	EDC Data Gathering Default = ½ Nameplate	Average blower motor capacity for gas furnace (typical range = ¼ hp to ¾ hp) EDC Data Gathering
<del>η<sub>motor</sub></del> , Efficiency of furnace blower motor	<del>%</del>	EDC Data Gathering Default = 50%	Typical efficiency of ½ hp blower motor
<del>%Programmable</del> , % central AC systems with a programmable thermostat	<del>None</del>	EDC Data Gathering Forced Air Default = <del>5868</del> %	EDC Data Gathering <del>43</del>
<del>%Manual</del> , % central AC systems with a manual thermostat	<del>None</del>	EDC Data Gathering Forced Air Default = <del>4232</del> %	EDC Data Gathering <del>43</del>
<del>ESF<sub>cool</sub></del> , cooling energy saving factor	<del>None</del>	<del>See Table 2-37</del> See Table 2-46	Composite of multiple sources
<del>ESF<sub>heat</sub></del> , heating energy saving factor	<del>None</del>	<del>See Table 2-38</del> See Table 2-47	Composite of multiple sources
<del>PDSF</del> , peak demand savings factor relative to <del>ESF<sub>cool</sub></del>	<del>None</del>	EDC Data Gathering Default = 50%	<del>436</del>

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Term	Unit	Value	Sources
<u><i>CF<sub>CF,summer</sub></i></u> , Demand Coincidence Factor during the summer months	<i>Proportion</i>	See CF in Vol. 1, App. A	144
<u><i>CF<sub>CF,winter</sub></i></u> , Demand Coincidence Factor during the winter months	<i>Proportion</i>	See CF in Vol. 1, App. A	4
DF, Derate Factor for Electric Resistance Heating Systems	None	0.85	Professional Judgement

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Table 2-37 and Table 2-38Note: Where appropriate, nameplate data collected for usage in savings calculations (i.e., SEER, EER, HSPF) should be converted to new efficiency metrics (i.e., SEER2, EER2, HSPF2) using conversion equations laid out in Vol. 1 App. A

Table 2-46 and Table 2-47 show ESF values for cooling and heating (percentage of heating or cooling consumption saved by thermostat type, installation type, and HVAC system type). Each value taken from a secondary literature study has a footnote with its corresponding reference. All other ESF values (without footnotes) were calculated from the referenced value to find ESF values for different baselines.

**Table 2-46: Cooling Energy Savings Factors (ESF<sub>cool</sub>)**

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Installation Type	Baseline	ASHP Cooling	CAC Cooling
Upstream buy-down (Customer Self-Installation)	Unknown Mix Default	4.8% <sup>a</sup>	4.8% <sup>a</sup>
Customer Self-Installation with Education	Unknown Mix Default	7.54% <sup>b</sup>	7.54% <sup>b</sup>
Professional Installation	Manual	11.3% <sup>c</sup>	11.3% <sup>c</sup>
	Conventional Programmable	9.3% <sup>d</sup>	9.3% <sup>d</sup>

<sup>a</sup> Source 67

<sup>b</sup> Cooling savings are based on average of savings from unknown mix default with customer self-installation and average of professional installation savings from manual and programmable thermostats. In this case,  $7.54\% = ((11.3\% \times 0.4232 + 9.3\% \times 0.5868) + 4.8\%) / 2$

<sup>c</sup> Average of cooling savings estimates from multiple studies. Sources: 2, 78, 9, 42, 10, 11

<sup>d</sup> The ESF value is applied here subtracts the assumed savings value from values are for programmable thermostats in the 2016 Pennsylvania TRM (2.0%) from the manual thermostat baseline ESF based of DEER 2005's cooling savings for climate zone 16.

**Table 2-47: Heating Energy Savings Factors (ESF<sub>heat</sub>)**

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Program Type	Baseline	Air Source Heat Pump	Furnace/Boiler Heating (Electric or Fossil)
Upstream buy-down (Customer Self-Installation)	Unknown Mix Default	6.4% <sup>a</sup>	6.4% <sup>a</sup>
Customer Self-Installation with Education	Unknown Mix Default	7.97% <sup>b</sup>	7.97% <sup>b</sup>
Professional Installation	Manual	11.5% <sup>c</sup>	11.5% <sup>c</sup>
	Conventional programmable	7.9% <sup>d</sup>	7.9% <sup>d</sup>

<sup>a</sup> Average of heating estimates from two studies. Sources: 9, 11, 10, 12

<sup>b</sup> Heating savings are based on average of savings from unknown mix default with customer self-installation and average of professional installation savings from manual and programmable thermostats. In this case,  $7.97\% = ((11.5\% \times 0.4232 + 7.9\% \times 0.5868) + 6.4\%) / 2$

<sup>c</sup> Average of four heating savings estimates from four multiple studies. Sources: 7, 10, 129, 11, 13

<sup>d</sup> The ESF value are for a is applied here as an estimate until information becomes available showing different programmable thermostats based of DEER 2005's cooling savings incented through a direct install program for climate zone 16.

**DEFAULT SAVINGS**

Table 2-39 through Table 2-41 Table 2-48 through Table 2-50 provide deemed energy savings values by program type, HVAC system type, and baseline thermostat style using statewide average EFLH values. Table 2-42 Table 2-51 provides deemed peak demand savings by program type, HVAC system type, and baseline thermostat style using statewide average CF values. If an EDC wishes to calculate default savings specific to their service territory, the climate region weights in Table 1-6 and the EFLH values in Table 1-8 can be used with the algorithms and assumptions in this protocol. The values in Table 1-6 and Table 1-8 are also included in the MS Excel Appendix A

calculator (Climate Dependent Values). In an upstream program delivery model, an EDC may not be able to collect the HVAC system type for each participating household. Table 2-43 Table 2-52 provides default HVAC system type shares, by EDC, from the 2018/2023 Residential Baseline Study which can be used to derive EDC-specific default savings values for upstream program delivery.

**Table 2-48: Default Statewide Cooling Savings (kWh/yr)**

Program Type	Baseline	ASHP Cooling	CAC Cooling
Upstream buy-down (Customer Self-Installation)	Unknown Mix Default	6986	7792
Customer Self-Installation with Education	Unknown Mix Default	408132	420141
Professional Installation	Manual	463202	482215
	Conventional programmable	434166	450177

**Table 2-49: Default Statewide Heating Savings (kWh/yr)**

Program Type	Baseline	ASHP with Electric Auxiliary Heating	Electric Furnace	Fossil Fuel Furnace (Fan Only)
Upstream buy-down (Customer Self-Installation)	Unknown Mix Default	420440	1,213476	4844
Customer Self-Installation with Education	Unknown Mix Default	519529	1,499775	6053
Professional Installation	Manual	756791	2,480651	8779
	Conventional programmable	519543	1,498821	6054

**Table 2-50: Default Statewide Total Heating and Cooling Savings (kWh/yr)**

Program Type	Baseline	ASHP with Electric Aux	CAC w/ Electric Furnace	CAC w/ Gas (Fan)
Upstream buy-down (Customer Self-Installation)	Unknown Mix Default	490526	1,290567	425136
Customer Self-Installation with Education	Unknown Mix Default	627661	1,649916	480194
Professional Installation	Manual	918992	2,362867	268295

	Conventional programmable	653709	1,647999	209232
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Table 2-51: Default Statewide Peak Demand Savings (kW/yr)

Program Type	Baseline	ASHP Cooling		CAC Coolingw/ Electric Furnace		CAC w/ Gas Furnace (Fan Only)	
		Summer Peak	Winter Peak	Summer Peak	Winter Peak	Summer Peak	Winter Peak
Upstream buy-down (Customer Self-Installation)	Unknown Mix Default	0.0269028	0.0289064	0.030	0.301	0.030	0.009
Customer Self-Installation with Education	Unknown Mix Default	0.0418044	0.0450077	0.046	0.362	0.046	0.011
Professional Installation	Manual	0.0633067	0.0680116	0.070	0.541	0.070	0.016
	Conventional programmable	0.0524055	0.0560079	0.058	0.372	0.058	0.011

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Table 2-52: HVAC System Type Shares by EDC for Upstream Program Delivery

EDC	ASHP with Electric Aux	CAC w/ Electric Furnace	CAC w/ Gas
PECO	43.75%	0.00%	56.25%
PPL	50.00%	0.00%	50.00%
Duquesne	9.52%	4.76%	85.71%
FE: Met-Ed	19.05%	9.52%	71.43%
FE: Penelec	22.22%	0.00%	77.78%
FE: Penn Power	13.64%	4.55%	81.82%
FE: West Penn	29.41%	0.00%	70.59%

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. Evaluation contractors may choose to propose independent assessments of the ESF factors to the SWE in their EM&V plans. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- 1)  ~~Pennsylvania Act 129 2018 Residential Baseline Study, <http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3-Res-Baseline-Study-Rpt021219.pdf>.~~



- 2) ~~EnerNOC, Xcel Energy: In-Home Smart Device Pilot. Public Service Company of Colorado," March, 2014, <https://www.xcelenergy.com/staticfiles/xcel/Regulatory/Regulatory%20PDFs/CO-DSM/CO-2014-IHSD-Pilot-Evaluation.pdf>~~
- 3) ~~New York Standard Approach for Estimating Energy Savings from Energy Efficiency Measures in Commercial and Industrial Programs, September 1, 2009. [http://www3.dps.ny.gov/W/PSCWeb.nsf/96f0fec0b45a3c6485257688006a701a/766a83dce56eca35852576da006d79a7/\\$FILE/90\\_day\\_CI\\_manual\\_final\\_9-1-09.pdf](http://www3.dps.ny.gov/W/PSCWeb.nsf/96f0fec0b45a3c6485257688006a701a/766a83dce56eca35852576da006d79a7/$FILE/90_day_CI_manual_final_9-1-09.pdf)~~
- 4) ~~Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/>~~
- 5) ~~California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.~~
- 1) ~~Navigant Consulting, Inc., "California Electronic Technical Reference Manual. "Smart Thermostat Residential". Accessed August 2023 Weblink~~
- 6) ~~ENERGY STAR Illinois Smart Thermostat – Annual and Seasonal kWh Savings – Impact Findings," February 26, 2016. [http://ilsagfiles.org/SAG\\_files/Technical\\_Reference\\_Manual/Version\\_5/Illinois\\_Smart\\_Thermostat\\_Electric\\_Impact\\_Findings\\_2016-02-26.pdf](http://ilsagfiles.org/SAG_files/Technical_Reference_Manual/Version_5/Illinois_Smart_Thermostat_Electric_Impact_Findings_2016-02-26.pdf)~~
- 7) ~~The Cadmus Group, Inc., "Vectren: Evaluation of 2013–2014 Programmable and Smart Thermostat Program," January 2014, [http://www.cadmusgroup.com/wp-content/uploads/2015/06/Cadmus\\_Vectren\\_Nest\\_Report\\_Jan2015.pdf?submissionGuid=664af99c-7ff7-4afe-a8e6-b6c7acc4d9cb](http://www.cadmusgroup.com/wp-content/uploads/2015/06/Cadmus_Vectren_Nest_Report_Jan2015.pdf?submissionGuid=664af99c-7ff7-4afe-a8e6-b6c7acc4d9cb)~~
- 8) ~~2) Energy Star Program Requirements for Connected Thermostat Products <https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Program%20Requirements%20for%20Connected%20Thermostats%20Version%201.0.pdf> Weblink V1.0 12/23/2016~~
- 9) ~~Apex Analytics LLC, "Energy Trust of Oregon Nest Thermostat Smart Thermostat Pilot Evaluation," March 1, 2016, [https://www.energytrust.org/wp-content/uploads/2016/12/Smart\\_Thermostat\\_Pilot\\_Evaluation\\_Final\\_wSR.pdf](https://www.energytrust.org/wp-content/uploads/2016/12/Smart_Thermostat_Pilot_Evaluation_Final_wSR.pdf)~~
- 10) ~~Apex Analytics LLC, "Energy Trust of Oregon Nest Thermostat Heat Pump Control Pilot Evaluation," October 10, 2014, <https://nest.com/downloads/press/documents/energy-trust-of-oregon-pilot-evaluation-whitepaper.pdf>~~
- 11) ~~Navigant Consulting, Inc., "Residential Smart Thermostats: Impact Analysis – Gas Preliminary Findings," December 16, 2015. [http://ilsagfiles.org/SAG\\_files/Meeting\\_Materials/2015/December\\_2015\\_Meetings/Presentations/Smart\\_Thermostat\\_Preliminary\\_Gas\\_Impact\\_Findings\\_2015-12-08\\_to\\_IL\\_SAG.pdf](http://ilsagfiles.org/SAG_files/Meeting_Materials/2015/December_2015_Meetings/Presentations/Smart_Thermostat_Preliminary_Gas_Impact_Findings_2015-12-08_to_IL_SAG.pdf)~~
- 12) ~~The Cadmus Group, Inc., "Wi-Fi Programmable Controllable Thermostat Pilot Program Evaluation, September 2012, <http://ma-eeac.org/wordpress/wp-content/uploads/Wi-Fi-Programmable-Controllable-Thermostat-Pilot-Program-Evaluation-Part-of-the-Massachusetts-2011-Residential-Retrofit-Low-Income-Program-Area-Study.pdf>~~
- 13) ~~Illinois TRM version 8.0 Volume 3: Residential Measures, effective January 1, 2020. [https://ilsag.s3.amazonaws.com/IL-TRM\\_Effective\\_01-01-20\\_v8.0\\_Vol\\_3\\_Res\\_10-17-19\\_Final.pdf](https://ilsag.s3.amazonaws.com/IL-TRM_Effective_01-01-20_v8.0_Vol_3_Res_10-17-19_Final.pdf)~~
- 3) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study Weblink.~~
- 4) ~~Better Duct Systems for Home Heating and Cooling, U.S. Department of Energy. Assuming for an improved duct system with insulation levels at R-8 and leakage at 5% of the system fan flow Weblink~~

- 14)5) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service - <https://www.ecobee.com/donateyourdata/> (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink).
- 6) Engineering judgement with data referenced from Guidehouse's econometric analysis in optimizing Connected Thermostats placed in the Illinois Statewide Technical Reference Manual. (2023, version 11.0). Weblink
- 7) Navigant Consulting, Inc. for the Illinois Stakeholder Advisory Group. (2016). Illinois Smart Thermostat – Annual and Seasonal kWh Savings – Impact Findings
- 8) EnerNOC for Xcel Energy. (2014). In-Home Smart Devices Pilot Program Impact Evaluation Results, 2012-2013. Weblink
- 9) The Cadmus Group, Inc. for Vectren Corporation. (2015). Evaluation of the 2013–2014 Programmable and Smart Thermostat Program. Weblink
- 10) Apex Analytics LLC for Energy Trust of Oregon. (2016). Energy Trust of Oregon Smart Thermostat Pilot Evaluation. Weblink
- 11) The Cadmus Group, Inc. for The Electric and Gas Program Administrators of Massachusetts. (2012). Wi-Fi Programmable Controllable Thermostat Pilot Program Evaluation. Weblink
- 12) Navigant Consulting, Inc. for the Illinois Stakeholder Advisory Group. (2015). Residential Smart Thermostats: Impact Analysis – Gas Preliminary Findings. Weblink
- 13) Apex Analytics LLC for Energy Trust of Oregon. (2014). Energy Trust of Oregon Nest Thermostat Heat Pump Control Pilot Evaluation. Weblink

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**2-2.122.2.13 FURNACE MAINTENANCE**

<b>Target Sector</b>	Residential <del>Establishments</del>
<b>Measure Unit</b>	Per Furnace
<b>Measure Life</b>	23 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

Regular preventative maintenance of residential furnaces provides numerous potential benefits including increased efficiency, increased comfort, reduced repairs and increased safety. This protocol covers the calculation of energy savings associated with preventative maintenance of a residential furnace.

**ELIGIBILITY**

The measure requires that an approved technician inspect, clean and adjust the furnace. This service must include the following:

- Measure combustion efficiency and temperature rise with flue analyzer
- Check and replace filter if necessary
- Clean burners, pilot and pilot tube, flame baffle, heat exchanger and blower
- Check and adjust gas pressure to manufacturer’s recommendation
- Inspect the condition of the heat exchanger(s)
- Check that flue and venting are operating properly
- Check fan belt and replace if necessary
- Inspect wiring for loose connections
- Check for correct line and load voltage and amperage
- Check safety locks for proper operation

The algorithms and savings are valid for servicing once every two years. If serviced more frequently, the energy savings factor (ESF) will need to be re-evaluated.

**ALGORITHMS**

The annual energy savings are obtained through the following formula. There are no demand savings for this measure.

$$\Delta kWh = kW_{motor} \times EFLH_{heat,non-HP} \times ESF$$

**DEFINITION OF TERMS**

Table 2-53: Terms, Values, and References for Furnace Maintenance

Term	Unit	Values	Source
$kW_{motor}$ , Average motor full load electric demand	kW	0.377	2
$EFLH_{heat,non-HP}$ , Equivalent full load heating hours	Hours/year	See $EFLH_{heat,non-HP}$ in Vol. 1, App. A	3
$ESF$ , Energy savings factor	None	2%	4

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## DEFAULT SAVINGS

Table 2-54: Default Savings per Input kBTU/h for Furnace Maintenance

Climate Region	Reference City	Energy Savings (kWh per 1 input kBTU/h)
C	Allentown	6.822
A	Binghamton, NY	8.782
G	Bradford	10.28.98
I	Erie	7.913
E	Harrisburg	7.5.90
D	Philadelphia	5.714
H	Pittsburgh	7.16.68
B	Scranton	7.56.84
F	Williamsport	7.06.85

## EVALUATION PROTOCOLS

~~For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.~~

## SOURCES

- 1) ~~Act on Energy Commercial Technical Reference Manual No. 2010-4, 9.2.3 Gas Forced-Air Furnace Tune-up.~~

## EVALUATION PROTOCOLS

~~For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.~~

## SOURCES

- 1) Engineering judgement based off other HVAC Tune up measures.
- 2) Average blower motor capacity for gas furnace (typical range = ¼ hp to ¾ hp). Converted to kW with 1 HP = 0.7547 kW.
- 3) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/> (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)
- 4) State of Minnesota, Technical Reference Manual for Energy Conservation Improvement Programs, Version 2.0. <http://mn.gov/commerce-stat/pdfs/mn-trm-v2.0-041616.pdf>Weblink

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### 2.2.14 ENERGY STAR BATHROOM EXHAUST FAN

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Exhaust Fan Unit
<b>Measure Life</b>	15 years <sup>Source1</sup>
<b>Vintage</b>	Replace on Burnout, New Construction

This measure is for the purchase and installation of a bathroom exhaust fan meeting ENERGY STAR eligibility criteria. The amount of energy savings depends on whether the fan is used for spot ventilation or for continuous mechanical ventilation due to reduced air-infiltration from a tighter building shell. This measure assumes fan capacities between 10 and 200 CFM rated at a sound level of less than 2.0 sones at 0.1 inches of water column static pressure. When claiming savings associated with continuous operation, eligible installations should be sized to provide the mechanical ventilation rate indicated by ASHRAE 62.2.

#### ELIGIBILITY

This protocol documents the energy savings attributed to purchasing an exhaust-only bathroom ventilation fan meeting ENERGY STAR eligibility criteria instead of a bathroom ventilation fan that does not meet ENERGY STAR criteria. For continuous ventilation, the fan shall be rated for and providing continuous ventilation in accordance with ASHRAE 62.2.<sup>35</sup> ENERGY STAR specifications are provided below.<sup>Source 2</sup>

Table 2-55: ENERGY STAR Eligibility Criteria for Bathroom Exhaust Fans

Fan Capacity (CFM)	Minimum Efficacy (CFM/Watt)	Maximum Sound Level (sones)
10-89	2.8	2.0
90-200	3.5	2.0

#### ALGORITHMS

The energy savings algorithms are shown below. The key variables affecting the energy savings are the rated size (CFM) and efficiencies.

$$\Delta kWh = \left( CFM \times \frac{\frac{1}{\eta_{Baseline} \frac{CFM}{W}} - \frac{1}{\eta_{Efficient} \frac{CFM}{W}}}{1,000} \right) \times Hours$$

$$\Delta kWh_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kWh_{winter\ peak} = \Delta kWh \times ETDF_w$$

<sup>35</sup> ASHRAE 62.2 recommends a minimum of 20 CFM for continuous bathroom ventilation. Weblink

**DEFINITION OF TERMS**

**Table 2-56: Terms, Values, and References for ENERGY STAR Bathroom Exhaust Fan**

Term	Unit	Values	Source
<u>CFM</u> , Fan flow rate	<u>CFM</u>	<u>Table 2</u>	<u>3, 4</u>
<u>Hours</u> , Hours of operation	<u>Hours/year</u>	<u>Continuous = 8,760</u> <u>Spot = EDC Data Gathering or 840</u>	<u>5</u>
<u>ηBaseline</u> , <u>Baseline fan efficacy</u>	<u>CFM/W</u>	<u>Table 2</u>	<u>4</u>
<u>ηEfficient</u> , <u>Efficient fan efficacy</u>	<u>CFM/W</u>	<u>EDC Data Gathering or Table 2</u>	<u>EDC Data Gathering, 3, 4</u>
<u>ETDF<sub>s</sub></u> , <u>Summer energy to Demand Factor</u>	<u>kW</u> <u>kWh</u>	<u>Continuous = 0.0001142</u> <u>Spot = 0.0001113</u>	<u>6</u>
<u>ETDF<sub>w</sub></u> , <u>Winter energy to Demand Factor</u>	<u>kW</u> <u>kWh</u>	<u>Continuous = 0.0001142</u> <u>Spot = 0.0001790</u>	<u>6</u>

**Table 2-57: Assumptions for ENERGY STAR Bathroom Exhaust Fan**

Usage Profile	CFM Range	CFM	ηBaseline	ηEfficient
<u>Spot</u>	<u>≤89</u>	<u>71.3</u>	<u>1.7</u>	<u>5.3</u>
<u>Spot</u>	<u>90-200</u>	<u>115.9</u>	<u>2.7</u>	<u>5.9</u>
<u>Continuous</u>	<u>n/a</u>	<u>43.8</u>	<u>1.8</u>	<u>9.5</u>

**DEFAULT SAVINGS**

Default savings are as follows, with unknown usage defaulting to spot usage based on fan capacity (CFM):

**Table 2-58: Default Bathroom Exhaust Fan Energy Savings**

Usage Profile	CFM Range	ΔkWh/yr	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
<u>Spot or Unknown</u>	<u>≤89</u>	<u>23.9</u>	<u>0.0027</u>	<u>0.0043</u>
<u>Spot or Unknown</u>	<u>90-200</u>	<u>19.6</u>	<u>0.0022</u>	<u>0.0035</u>
<u>Continuous</u>	<u>n/a</u>	<u>172.8</u>	<u>0.0197</u>	<u>0.0197</u>

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate

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evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

#### **SOURCES**

- 1) Estimate based on 25 years for whole-house fans and 19 for thermostatically-controlled attic fans from GDS Associates for The New England State Program Working Group. (2007, June). Residential and Commercial/Industrial Lighting and HVAC Measures. Weblink. Limited to PA Act 129 maximum of 15 years.
- 2) U.S. EPA. (2015). ENERGY STAR Program Requirements Product Specification for Residential Ventilating Fans Eligibility Criteria Version 4.2. Weblink
- 3) Guidehouse analysis reviewing average CFM and fan efficacy for ENERGY STAR-rated bathroom ventilation fans at the lowest setting in the 10-200 CFM range. Weblink accessed 2/9/22.
- 4) Guidehouse analysis reviewing average CFM and fan efficacy for units both eligible and ineligible for ENERGY STAR qualification. Weblink accessed 2/9/22.
- 5) Spot operation hours per year are assumed to coincide with lighting HOU for bathrooms (2.3 hours per day \* 365.25 days per year). Statewide Evaluation Team for Pennsylvania Public Utilities Commission (2014, January). 2014 Commercial & Residential Light Metering Study. Weblink
- 6) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

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## **2.3 DOMESTIC HOT WATER**

### **2.3.1 HEAT PUMP WATER HEATERS**

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## 2.32.1 DOMESTIC HOT WATER

### 2.3.12.1.1 HEAT PUMP WATER HEATERS

Target Sector	Residential Establishments
Target Sector	Residential
Measure Unit	Water Heater
Measure Life	10 years <sup>Source 1</sup>
Vintage	Replace on Burnout

Heat Pump Water Heaters take heat from the surrounding air and transfer it to the water in the tank, unlike conventional water heaters, which use either gas (or sometimes other fuel) burners or electric resistance heating coils to heat the water.

#### ELIGIBILITY

This protocol documents the energy savings attributed to heat pump water heaters with Uniform Energy Factors meeting Energy Star Criteria Version 3.2.<sup>Source 2</sup> The target sector primarily consists of single-family residences.

#### ALGORITHMS

The energy savings calculation utilizes average performance data for available residential heat pump and standard electric resistance water heaters and typical water usage for residential homes. The algorithms take into account interactive effects between the water heater and HVAC system when installed inside conditioned space. The energy savings are obtained through the following formula:

$$\Delta kWh = \frac{\left(\frac{1}{UEF_{base}} - \frac{1}{UEF_{ee} \times F_{derate}}\right) \times HW \times 365 \frac{days}{yr} \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in})}{3412 \frac{BTU}{kWh}} + \frac{\Delta kWh_{ie,cool} \left(\frac{1}{UEF_{base}} - \frac{1}{UEF_{ee} \times F_{derate}}\right) \times HW \times 365 \times 8.3 \times (T_{out} - T_{in})}{3412} + \Delta kWh_{ie,cool} - \Delta kWh_{ie,hea}$$

Include below interactive effects calculations only when water heater is installed inside conditioned space with electric heating and cooling.

- If either electric heating or electric cooling is absent, then the respective interactive effect will equal zero.
- When installed outside of conditioned space, both interactive effects will equal zero, and the appropriate  $F_{derate}$  in Table 2-48 Table 2-62 will account for reduced performance due to cooler annual temperatures.
- If installation location is unknown (such as with midstream delivery programs), use the 'Default/Unknown' value for  $F_{derate}$  in Table 2-62 and both interactive effects will equal zero.

$$\Delta kWh_{ie,cool} = \frac{HW \times \frac{8.3 BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in}) \times EFLH_{cool}}{24 \frac{hrs}{day} \times SEER \times 1000 \frac{W}{kW}} - \frac{HW \times 8.3 \times (T_{out} - T_{in}) \times EFLH_{cool}}{24 \times SEER2 \times 1000}$$

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$$\Delta kW_{h_{ie,heat}} = \frac{HW \times \frac{8.3 \text{ Btu}}{\text{gal} \cdot \text{°F}} \times (T_{out} - T_{in}) \times EFLH_{heat}}{24 \frac{\text{hrs}}{\text{day}} \times HSPF \times 1000 \frac{\text{W}}{\text{kW}}} = \frac{HW \times 8.3 \times (T_{out} - T_{in}) \times EFLH_{heat}}{24 \times HSPF2 \times 1000}$$

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For heat pump water heaters, demand savings result primarily from a reduced connected load. However, since the interactive effects during the heating season have no effect on the peak demand, the heating season interactive effects are subtracted from the total kWh savings before the ETDf is applied. The demand reduction is taken as the annual energy savings multiplied by the ratio of the average demand between 2 PM and 6 PM on summer weekdays to the total annual energy usage.

$$\Delta kW_{peak} = ETDf \times (\Delta kWh - \Delta kWh_{ie,heat})$$

ETDF (Energy to Demand Factor) is defined below:

$$ETDF = \frac{\text{Average Demand}_{\text{summer WD 2-6 PM}}}{\text{Annual Energy Usage}}$$

The ratio of the average demand between 2 PM and 6 PM on summer weekdays to the total annual energy usage is taken from an electric water heater metering study performed by BG&E. <sup>Source 19</sup>

### DEFINITION OF TERMS

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDf_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDf_w$$

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### DEFINITION OF TERMS

Table 2-59: Terms, Values, and References for Heat Pump Water Heater

Term	Unit	Values	Source
<b>Heat Pump Water Heater</b>			
<i>UEF<sub>base</sub></i> , Uniform Energy Factor of baseline water heater	None	See Table 2-47 Default: 0.92 (50 gal., medium draw)	3
<i>UEF<sub>act</sub></i> , Uniform Energy Factor of proposed efficient water heater	None	EDG Data Gathering Default ≤55 Gals: 2.00 Default >55 Gal: 2.20	2
<i>HW</i> , Hot water used per day in gallons	$\frac{\text{gallons}}{\text{day}}$	45.5	4
<i>UEF<sub>base</sub></i> , Uniform Energy Factor of baseline water heater	Proportion	See Table 2-61 Default: 0.92 (50 gal., medium draw)	3

<u><math>UEF_{ec}</math>, Uniform Energy Factor of proposed efficient water heater</u>	<u>Proportion</u>	<u>EDC Data Gathering</u> <u>Default Integrated HPWH: 3.30</u> <u>Default Integrated HPWH, 120 Volt, 15 Amp Circuit: 2.20</u> <u>Default Split-system HPWH: 2.20</u>	<u>2</u>
<u><math>F_{derate}</math>, COP De-rating factor</u>	<u>Proportion</u>	Table 2-62	<u>9, and discussion below</u>
<u><math>HW</math>, Hot water used per day in gallons</u>	<u><math>\frac{\text{gallons}}{\text{day}}</math></u>	<u>45.5</u>	<u>5</u>
<u><math>V_r</math>, Rated storage volume of baseline water heater</u>	<u>gallons</u>	EDC Data Gathering	EDC Data Gathering
<u><math>T_{out}</math>, Temperature of hot water</u>	<u><math>^{\circ}F</math></u>	119	<u>57</u>
<u><math>T_{in}</math>, Temperature of cold water supply</u>	<u><math>^{\circ}F</math></u>	<u>52.53</u>	<u>68</u>
<u><math>F_{derate}</math>, COP De-rating factor-<math>EFLH_{cool}</math>, Equivalent Full Load Hours for cooling</u>	<u><math>\frac{\text{hours}}{\text{yr}}</math></u> <u>Proportion</u>	Table 2-48 See <u><math>EFLH_{cool}</math> in Vol. 1, App. A</u>	<u>7, and discussion below</u> <u>10</u>
<u><math>EFLH_{cool}</math>, Equivalent Full Load Hours for cooling</u>	<u><math>\frac{\text{hours}}{\text{yr}}</math></u>	See <u><math>EFLH_{cool}</math>, <math>EFLH_{heat}</math> in Vol. 1, App. A</u>	<u>810</u>
<u><math>EFLH_{heat}</math>, Equivalent Full Load Hours for heating</u>	<u><math>\frac{BTU \cdot \text{hours}}{W \cdot h \cdot \text{yr}}</math></u>	See <u><math>EFLH_{heat}</math> in Vol. 1, App. A</u> EDC Data Gathering <u>Default see Table 2-60</u>	<u>86</u>
<u><math>HSPF</math>, Heating Seasonal Performance Factor of heating equipment</u>	<u><math>\frac{BTU}{W \cdot h}</math></u>	EDC Data Gathering Default see <u>Table 2-45</u> Table 2-60	<u>96</u>
<u><math>SEER</math>, Seasonal Energy Efficiency Ratio of cooling equipment</u>	<u><math>\frac{kW \cdot BTU}{kWh \cdot W \cdot h}</math></u>	EDC Data Gathering Default see <u>Table 2-45</u> 0.0001057	<u>911</u>
<u><math>ETDF</math>, Energy to Demand Factor (defined above)</u>	<u><math>\frac{kWh}{yr}</math></u>	0.00098047	<u>1011</u>

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Table 2-60: Default Cooling and Heating System Efficiencies

Type	<u>SEER</u> <u>SEER2</u>	<u>HSPF</u> <u>HSPF2</u>
Central Air Conditioner	<u>12.1</u> <u>13.2</u>	N/A
Room Air Conditioner Room Air Conditioner	<u>10.6</u> <u>11.4</u>	N/A

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Air-Source Heat Pump	<u>13.514.1</u>	<u>87.2</u>
Ground-Source Heat Pump	<u>15.018.5</u>	<u>10.98</u>
Ductless Mini-Split	<u>14.917.6</u>	<u>8.96</u>
Electric Resistance	N/A	3.412

<sup>a</sup>CEER

**Table 2-61: Minimum Baseline Uniform Energy Factors Based on Rated Storage Volume and Draw Pattern**

The current Federal Standards for electric water heater Uniform Energy Factors (UEF) vary based on rated storage volume and draw pattern. This standard, which went into effect at the end of 2016, replaces the old federal standard equal to  $0.96 - (0.0003 \times \text{Rated Storage in Gallons})$  for tanks equal to or smaller than 55 gallons and  $2.057 - (0.00113 \times \text{Rated Storage})$  for tanks larger than 55 gallons. Table 2-47 shows the formulas to calculate the minimum UEF for various tanks sizes using both the new standard with draw patterns, and the pre-draw pattern standard, which will likely be more common in replacements through 2021. Pre-calculated UEF values are provided for common tank sizes. Draw patterns are defined in the Federal Standard test procedures for water heaters as illustrated in Table 2-46. <sup>Source-12</sup>

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**Table 2-48: Draw Pattern Definitions**

Type Rated Storage Volume (gallons)	Draw Pattern	Max. Daily Hot Water Draw (gallons) UEF Calculation	First Hour Rating (FHR) (gallons)
Storage $\geq 20$ gal and $\leq 55$ gal	Very Small	<u>19</u>	$0 \leq FHR < 180.8808 - (0.0008 \times V_r)$
	Low	$380.9254 - (0.0003 \times V_r)$	$18 \leq FHR < 54$
	Medium	$550.9307 - (0.0002 \times V_r)$	$54 \leq FHR < 75$
	High	$840.9349 - (0.0001 \times V_r)$	$FHR \geq 75$
$> 55$ gal and $\leq 120$ gal	Very Small	$1.9236 - (0.0011 \times V_r)$	
	Low	$2.0440 - (0.0011 \times V_r)$	
	Medium	$2.1171 - (0.0011 \times V_r)$	
	High	$2.2418 - (0.0011 \times V_r)$	

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**Table 2-49: Minimum Baseline Uniform Energy Factors Based on Rated Storage Volume and Draw Pattern**

Rated Storage Volume (gallons)	Draw Pattern	UEF Calculation	Minimum UEF
$\geq 20$ gal and $\leq 55$ gal	Pre-2017	$0.9600 - (0.0003 \times V_r)$	
	Very-Small	$0.8808 - (0.0008 \times V_r)$	
	Low	$0.9254 - (0.0003 \times V_r)$	

Rated Storage Volume (gallons)	Draw Pattern	UEF Calculation	Minimum UEF
	Medium	$0.9307 - (0.0002 \times V_r)$	
	High	$0.9349 - (0.0001 \times V_r)$	
>55-gal and <=120 gal	Pre-2017	$0.9600 - (0.0003 \times V_r)$	
	Very Small	$0.8808 - (0.0008 \times V_r)$	
	Low	$0.9254 - (0.0003 \times V_r)$	
	Medium	$0.9307 - (0.0002 \times V_r)$	
	High	$0.9349 - (0.0001 \times V_r)$	
40	Pre-2017	$0.9600 - (0.0003 \times V_r)$	0.95
	Very Small	$0.8808 - (0.0008 \times V_r)$	0.85
	Low	$0.9254 - (0.0003 \times V_r)$	0.91
	Medium	$0.9307 - (0.0002 \times V_r)$	0.92
	High	$0.9349 - (0.0001 \times V_r)$	0.93
50	Pre-2017	$0.9600 - (0.0003 \times V_r)$	0.95
	Very Small	$0.8808 - (0.0008 \times V_r)$	0.84
	Low	$0.9254 - (0.0003 \times V_r)$	0.91
	Medium	$0.9307 - (0.0002 \times V_r)$	0.92
	High	$0.9349 - (0.0001 \times V_r)$	0.93
65	Pre-2017	$2.057 - (0.00113 \times V_r)$	1.98
	Very Small	$1.9236 - (0.0011 \times V_r)$	1.85
	Low	$2.0440 - (0.0011 \times V_r)$	1.97
	Medium	$2.1171 - (0.0011 \times V_r)$	2.05
	High	$2.2418 - (0.0011 \times V_r)$	2.17
80	Pre-2017	$2.057 - (0.00113 \times V_r)$	1.97
	Very Small	$1.9236 - (0.0011 \times V_r)$	1.84
	Low	$2.0440 - (0.0011 \times V_r)$	1.96
	Medium	$2.1171 - (0.0011 \times V_r)$	2.03
	High	$2.2418 - (0.0011 \times V_r)$	2.15
120	Pre-2017	$2.057 - (0.00113 \times V_r)$	1.92
	Very Small	$1.9236 - (0.0011 \times V_r)$	1.79
	Low	$2.0440 - (0.0011 \times V_r)$	1.91
	Medium	$2.1171 - (0.0011 \times V_r)$	1.99
	High	$2.2418 - (0.0011 \times V_r)$	2.11

**HEAT PUMP WATER HEATER UEF DE-RATING FACTOR**

The Uniform Energy Factors (UEF) are determined from a DOE testing procedure that is carried out at 67.5°F dry bulb and 56°F wet bulb temperatures. However, the average dry and wet bulb

temperatures in PA are in the range of 50-56°F DB and 45-50°F WB<sup>36</sup>. The heat pump performance is temperature and humidity dependent, ~~therefor~~therefore the location and type of installation is significant. To account for this, a UEF de-rating factor ( $F_{derate}$ ) has been adapted from a 2013 NEEA HPWH field study.<sup>Source 74</sup> The results used are for “Heating Zone 1”, which is comprised of Olympia, WA and Portland, OR and have average dry and wet bulb temperatures (51°F DB, 47°F WB and 55°F DB, 49°F WB, respectively)<sup>37</sup> comparable to Pennsylvania. Average temperatures are based on average weather data from weatherbase.com for the climate reference cities referenced elsewhere in this TRM.

Table 2-62: UEF De-rating Factor for Various Installation Locations

Installation Location	$F_{derate}$ <sup>38</sup>
Inside Conditioned Space	0.98
Unconditioned Garage	0.85
Unconditioned Basement	0.72
Default <sup>39</sup> Unknown <sup>Source 4</sup>	0.87

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#### DEFAULT SAVINGS

Default savings for the installation of heat pump water heaters *not located inside conditioned space or for which installation location is unknown* are calculated using the formulas provided below.

$$\Delta kWh = \left( \frac{1}{UEF_{base}} - \frac{1}{UEF_{se} \times F_{derate}} \right) \times 2706.75 \frac{kWh}{yr}$$

$$\Delta kW_{peak} = \frac{\Delta kWh}{12426.83 \frac{kWh}{kW}}$$

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<sup>36</sup> Based on average weather data from weatherbase.com for the climate reference cities referenced elsewhere in this TRM

<sup>37</sup> Ibid

<sup>38</sup> Calculated by dividing the COP in each location from Figure 15 by the rated Energy Factor (2.35) of the unit tested in the study (AirGenerate-AT166).

<sup>39</sup> Weighted average of values for water heater locations for all space heating fuel types in Table 107 of Northwest Energy Efficiency Alliance 2011 Residential Building Stock Assessment: Single Family Characteristics and Energy Use. Published September 18, 2012. Online at <https://neea.org/resources/2011-rbsa-single-family-characteristics-and-energy-use>

**Table 2-63: Default Savings for Heat Pump Water Heaters Located in Unconditioned or Unknown Space**

Installation Location	Efficient Water Heater Type	ΔkWh	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
Unconditioned Garage	Integrated HPWH	1,948	0.2058652	0.3429788
	Integrated HPWH, 120 Volt 15 Amp Circuit	1,472	0.1556275	0.2592811
	Split-system HPWH	1,472	0.1556275	0.2592811
Unconditioned Basement	Integrated HPWH	1,776	0.1877238	0.3127546
	Integrated HPWH, 120 Volt 15 Amp Circuit	1,215	0.1284155	0.2139448
	Split-system HPWH	1,215	0.1284155	0.2139448
Unknown	Integrated HPWH	1,969	0.2081750	0.3468270
	Integrated HPWH, 120 Volt 15 Amp Circuit	1,505	0.1590922	0.2650533
	Split-system HPWH	1,505	0.1590922	0.2650533

#### EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with calculation of energy and demand savings using above algorithms.

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- 1) California Electronic Technical Reference Manual. “Heat Pump Water Heater, Residential”. Accessed January 2024. Weblink
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- 3) “Residential End Uses of Water, Version 2.” ~~Water Research Foundation. (Apr 2016), p. 5-10~~ CFR 430.32(d). Weblink.
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- 4) ~~Water Research Foundation. ([https://www.circleofblue.org/wp-content/uploads/2016/04/WRF\\_REU2016.pdf](https://www.circleofblue.org/wp-content/uploads/2016/04/WRF_REU2016.pdf)~~
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- 5) 2016). Residential End Uses of Water, Version 2. Pg 5. Weblink

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- 6) [NMR Group for the Pennsylvania Public Utility Commission. \(2024, March\). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Pg 115, table 97, pg. 120, table 103. Weblink . Air source heat pump and ductless mini-split efficiencies calculated using 2023 Pennsylvania Residential Baseline Study data. Federal minimum efficiencies for GSHP due to small sample size for GSHP in baseline study.](#)
- 7) [Pennsylvania Act 129 2014 Residential Baseline Study. Section 4.6.1, pg 60, Table 4-64. Weblink](#)
- 8) [Using Rock Spring, PA \(Site 2036\) as a proxy, the mean of soil temperature at 40-inch depth is 54.86152.502. Calculated using Daily SCAN Standard - Period of Record data from April 1999 to December 2003 to December 2018 from the Natural Resource Conservation Service Database. \[https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\\\_scan\\\_por&state=PA\]\(https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\_scan\_por&state=PA\)Weblink. Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p.\(2017, March\). "2.6.1 Water Heater". Pg 78. <https://energy.mo.gov/sites/energy/files/MOTRM2017Volume2.pdf>Weblink](#)
- 9) [NEEA Heat Pump Water Heater Field Study Report. Prepared by Fluid Market Strategies, 2013. \[https://rpsc.energy.gov/tech-solutions/sites/default/files/attachments/NEEA\\\_HPWH\\\_Field\\\_Study\\\_Report\\\_October\\\_2013.pdf\]\(https://rpsc.energy.gov/tech-solutions/sites/default/files/attachments/NEEA\_HPWH\_Field\_Study\_Report\_October\_2013.pdf\)Fluid Market Strategies for NEEA. \(2013, October\). NEEA Heat Pump Water Heater Field Study Report. Weblink Values for Fderate are calculated by dividing the COP in each location from Figure 15 by the rated Energy Factor \(2.35\) of the unit tested in the study \(AirGenerate ATI66\). \(Note: when this source discusses "ducted" versus "non-ducted" systems it refers to the water heater's heat pump exhaust, not to the HVAC ducts.\)](#)
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- 10) [Straub, Mary and Switzer, Sheldon. "Using Available Information for Efficient Evaluation of Demand Side Management Programs". Study by BG&E. The Electricity Journal, Aug/Sept. 2011. p. 95. <http://www.sciencedirect.com/science/article/pii/S1040619011001941>](#)
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### 2.3.2 SOLAR WATER HEATERS

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Water Heater
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

Solar water heaters utilize solar energy to heat water, which reduces electricity required to heat water.

#### ELIGIBILITY

This protocol documents the energy savings attributed to solar water in PA. The target sector is single-family residences with an existing electric water heater.

#### ALGORITHMS

The energy savings calculation utilizes average performance data for available residential solar and standard water heaters and typical water usage for residential homes. The energy savings are obtained through the following formula:

$$\Delta kWh = \frac{\left( \frac{1}{UEF_{base}} - \frac{1}{UEF_{ee}} \right) \times HW \times 365 \frac{days}{yr} \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in})}{3412 \frac{BTU}{kWh}} \left( \frac{1}{UEF_{base}} - \frac{1}{UEF_{ee}} \right) \times HW \times 365 \times 8.3 \times (T_{out} - T_{in})$$

The demand reduction is taken as the annual energy usage of the *baseline* water heater multiplied by the ratio of the average demand between 2PM and 6PM on summer weekdays to the total annual energy usage. Note that this is a different formulation than the demand savings calculations for other water heaters. This modification of the formula reflects the fact that a solar water heater's capacity is subject to seasonal variation, and that during the peak summer season, the water heater is expected to fully supply all domestic hot water needs.

$$\Delta kWh_{peak} = ETDF \times kWh_{base}$$

Where:

$$kWh_{base} = \frac{\frac{1}{UEF_{base}} \times HW \times 365 \frac{days}{yr} \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in})}{3412 \frac{BTU}{kWh}}$$

ETDF (Energy to Demand Factor) is defined below:

$$ETDF = \frac{Average\ Demand_{Summer\ WD\ 2\ PM\ -\ 6\ PM}}{Annual\ Energy\ Usage}$$

$$\Delta kWh_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kWh_{winter\ peak} = \Delta kWh \times ETDF_w$$

The ratio of the average demand between 2 PM and 6 PM on summer weekdays to the total annual energy usage is taken from an electric water heater metering study performed by BG&E.<sup>Source 2</sup>

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**DEFINITION OF TERMS**

**Table 2-64: Terms, Values, and References for Solar Water Heater**

Term	Unit	Values	Source
$UEF_{base}$ , Uniform Energy Factor of baseline electric water heater	<i>Proportion</i>	EDC Data Gathering Default = 0.9092	EDC Data Gathering 43
$UEF_{es}$ , Year-round average Uniform Energy Factor of proposed solar water heater	<i>Proportion</i>	EDC Data Gathering Default = 2.62	EDC Data Gathering 2
$HW$ , Hot water used per day in gallons	$\frac{gallons}{day}$	45.5	54
$T_{out}$ , Temperature of hot water	$^{\circ}F$	119	65
$T_{in}$ , Temperature of cold water supply	$^{\circ}F$	52.53	76
$ETDF, ETDF_s$ , Summer Energy to Demand Factor (defined above)	$\frac{kW}{kWh/yr}, \frac{kW}{kWh}$	0.000080470001057	37
$ETDF_w$ , Winter Energy to Demand Factor	$\frac{kW}{kWh}$	0.0001761	7

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**DEFAULT SAVINGS**

Default energy and demand savings are as follows:

$\Delta kWh = 1,974.41880.5$  kWh

$\Delta kW_{summer\ peak} = 0.24201988$  kW

$\Delta kW_{winter\ peak} = 0.3312$  kW

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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**SOURCES**

- 1) California Electronic Technical Reference Manual. "Solar Thermal Water Heating System, Residential". Accessed Jan 2024. Weblink

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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- 7) ~~Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40-inch depth is 51.86+52.502. Calculated using Daily SCAN Standard - Period of Record data from April 1999December 2003 to December 20182023 from the Natural Resource Conservation Service Database. [https://wcc.sc.egov.usda.gov/nwcc/rgprt?report=daily\\_scan\\_por&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgprt?report=daily_scan_por&state=PA) Weblink-. Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p. 78. <https://energy.mo.gov/sites/energy/files/MOTRM2017Volume2.pdf>~~

**2.3.36) Fuel Switching: Electric Resistance to Fossil Fuel (2017, March). "2.6.1 Water Heater". Pg 78. Weblink**

7) [Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink](#)

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### 2.3.3 WATER HEATER TANK WRAP

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Water Heater Tank
<b>Measure Life</b>	Gas: 11 years <sup>Source 1</sup> Propane: 11 years <sup>Source 1B</sup>
<b>Vintage</b>	Replace on Burnout

#### ELIGIBILITY

This protocol documents the energy savings attributed to converting from a standard electric resistance water heater to an ENERGY STAR Version 3.2 natural gas or propane water heater. If a customer submits a rebate for a product that has applied for ENERGY STAR Certification but has not yet been certified, the savings will be counted for that product contingent upon its eventual certification as an ENERGY STAR measure. If at any point the product is rejected by ENERGY STAR, the product is then ineligible for the program and savings will not be counted.

The target sector primarily consists of single-family residences.

#### ALGORITHMS

The energy savings calculation utilizes average performance data for available residential standard electric and fossil fuel-fired water heaters and typical water usage for residential homes. Because there is little electric energy associated with a fossil fuel-fired water heater, the energy savings are the full energy utilization of the electric water heater. The energy savings are obtained through the following formula:

$$\Delta kWh = \frac{\frac{1}{UEF_{base,elec}} \times HW \times 365 \frac{\text{days}}{\text{yr}} \times 8.3 \frac{\text{BTU}}{\text{gal} \cdot \text{F}} \times (T_{out} - T_{in})}{3412 \frac{\text{BTU}}{\text{kWh}}}$$

Although there is a significant electric savings, there is an associated increase in fossil fuel energy consumption. While this fossil fuel consumption does not count against PA Act 129 energy savings, it is expected to be used in the program TRC test. The increased fossil fuel usage is obtained through the following formula:

$$\Delta MMBTU = \frac{\frac{1}{UEF_{installed}} \times HW \times 365 \frac{\text{days}}{\text{yr}} \times 8.3 \frac{\text{BTU}}{\text{gal} \cdot \text{F}} \times (T_{out} - T_{in})}{1,000,000 \frac{\text{BTU}}{\text{MMBTU}}}$$

Demand savings result from the removal of the connected load of the electric water heater. The demand reduction is taken as the annual energy savings multiplied by the ratio of the average energy usage between 2 PM and 6 PM on summer weekdays to the total annual energy usage.

$$\Delta kW_{peak} = ETDF \times \Delta kWh$$

ETDF (Energy to Demand Factor) is defined below:

$$ETDF = \frac{\text{Average Demand}_{\text{Summer WD 2PM-6PM}}}{\text{Annual Energy Usage}}$$

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The ratio of the average energy usage between 2 PM and 6 PM on summer weekdays to the total annual energy usage is taken from an electric water heater metering study performed by BG&E. Source 7

**DEFINITION OF TERMS**

**Table 2-52: Terms, Values, and References for Fuel Switching: Electric Resistance to Fossil Fuel Water Heater**

Term	Unit	Values	Source
$UEF_{base,elec}$ , Uniform Energy Factor of baseline water heater	Proportion	EDC Data Gathering Default: Table 2-47 in the Heat Pump Water Heaters section	2
$UEF_{installed,NG}$ , Uniform Energy Factor of installed natural gas water heater	Proportion	EDC Data Gathering Default: ≤55 Gallons= 0.67 >55 Gallons= 0.77	3
$UEF_{installed,Propane}$ , Uniform Energy Factor of installed propane water heater	Proportion	EDC Data Gathering Default: ≤55 Gallons= 0.67 >55 Gallons= 0.77	3
$UEF_{installed,Tankless-Water-Heater}$ , Uniform Energy Factor of installed tankless water heater	Proportion	EDC Data Gathering Default: 0.90	3
$HW$ , Hot water used per day in gallons	$\frac{gallons}{day}$	45.5	4
$T_{out}$ , Temperature of hot water	°F	119	5
$T_{in}$ , Temperature of cold water supply	°F	52	6
$ETDF$ , Energy to Demand Factor (defined above)	$\frac{kW}{\frac{kWh}{yr}}$	0.00008047	7

**UNIFORM ENERGY FACTORS BASED ON RATED STORAGE VOLUME AND DRAW PATTERN**

The current Federal Standards for electric water heater Uniform Energy Factors (UEF) vary based on rated storage volume and draw pattern. This standard, which went into effect at the end of 2016, replaces the old federal standard equal to 0.96-(0.0003×Rated Storage in Gallons) for tanks equal to or smaller than 55-gallons and 2.057-(0.00113×Rated Storage) for tanks larger than 55-gallons. Table 2-47 in the Heat Pump Water Heaters section shows the UEF for various tanks sizes using both the new standard with draw patterns, and the pre-draw pattern standard, which will likely be more common in replacements through 2021.

**DEFAULT SAVINGS**

The electric savings for the installation of a fossil fuel water heater should be calculated using the partially deemed algorithm below.

$$\Delta kWh = \frac{1}{UEF_{base,elec}} \times HW \times 365 \frac{\text{days}}{\text{yr}} \times 8.3 \frac{\text{BTU}}{\text{gal}\cdot\text{F}} \times (T_{out} - T_{in})$$

$$\Delta kWh_{peak} = ETDF \times \Delta kWh$$

The default savings for the installation of a 50-gallon natural gas/propane water heater in place of a standard electric water heater are listed in Table 2-51, below.

**Table 2-53: Energy Savings & Demand Reductions for Fuel Switching, Domestic Hot Water Electric to Fossil Fuel**

Electric-unit-UEF	Energy Savings (kWh/yr)	Demand Reduction (kW)
0.92	2,938.9	0.2365

The default fossil-fuel consumption for the installation of a standard efficiency natural gas/propane water heater in place of a standard electric water heater is listed in Table 2-52 below.

**Table 2-54: Fuel Consumption for Fuel Switching, Domestic Hot Water Electric to Fossil Fuel**

Fuel-Type	UEF	Fossil Fuel Consumption (MMBTU/yr)
Gas	0.67	13.78
Propane	0.67	13.78

**Note:** 10.87 gallons of propane provide 1 MMBTU of heat.

### EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with assignment of stipulated energy savings.

### SOURCES

- 1) DEER Effective Useful Life values, accessed Oct. 2018. <http://www.deeresources.com/>
- 2) U.S. Federal Standards for Residential Water Heaters. Effective April 16, 2015. [http://www1.eere.energy.gov/buildings/appliance\\_standards/product.aspx/productid/27](http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/27)
- 3) Commission Order requires fuel switching to ENERGY STAR measures, not standard efficiency measures. The Energy Factor has therefore been updated to reflect the Energy Star 3.2 standard for Gas Storage Water Heaters From Residential Water Heaters Key Product Criteria. [https://www.energystar.gov/sites/default/files/Water%20Heaters%20Final%20Version%203.2\\_Program%20Requirements\\_1.pdf](https://www.energystar.gov/sites/default/files/Water%20Heaters%20Final%20Version%203.2_Program%20Requirements_1.pdf) Accessed Oct. 2018. For the Commission Order see p. 42 of the TRC Final Test Order.
- 4) "Residential End Uses of Water, Version 2." *Water Research Foundation*. (Apr 2016), p. 5. [https://www.circleofblue.org/wp-content/uploads/2016/04/WRF\\_REU2016.pdf](https://www.circleofblue.org/wp-content/uploads/2016/04/WRF_REU2016.pdf)
- 5) Pennsylvania Statewide Residential End-Use and Saturation Study, 2014. [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE\\_2014\\_PA\\_Statewide\\_Act129\\_Residential\\_Baseline\\_Study.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE_2014_PA_Statewide_Act129_Residential_Baseline_Study.pdf).
- 6) Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40-inch depth is 51.861. Calculated using Daily SCAN Standard – Period of Record data from April 1999 to



December 2018 from the Natural Resource Conservation Service Database.  
[https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\\_scan\\_por&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily_scan_por&state=PA). Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p. 78.  
<https://energy.mo.gov/sites/energy/files/MOTRM2017Volume2.pdf>

- 7) Straub, Mary and Switzer, Sheldon. "Using Available Information for Efficient Evaluation of Demand Side Management Programs". Study by BG&E. The Electricity Journal. Aug/Sept, 2011. p. 95. <http://www.sciencedirect.com/science/article/pii/S1040619011001941>

### 2.3.4 WATER HEATER TANK WRAP

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Tank
<b>Measure Life</b>	7 years <sup>Source 6</sup>
<b>Vintage</b>	Retrofit

This measure applies to the installation of an insulated tank wrap or “blanket” to existing residential electric hot water heaters.

The base case for this measure is a standard residential, tank-style, electric water heater with no external insulation wrap.

#### ELIGIBILITY

This measure documents the energy savings attributed to installing an insulating tank wrap on an existing electric resistance water heater. The target sector is residential.

The U.S. Department of Energy recommends adding a water heater wrap of at least R-8 to any water heater with an existing R-value less than R-24.<sup>Source 67</sup>

#### ALGORITHMS

The annual energy savings for this measure are assumed to be dependent upon decreases in the overall heat transfer coefficient that are achieved by increasing the total R-value of the tank insulation.

$$\Delta kWh = \frac{HOU}{3412 \frac{BTU}{kWh} \times \eta_{Elec}} \times \frac{HOU}{3412 \times \eta_{Elec}} \times \left( \frac{A_{base}}{R_{base}} - \frac{A_{insul}}{R_{insul}} \right) \times (T_{setpoint} - T_{ambient})$$

$$\Delta kW_{peak} = \frac{\Delta kWh}{HOU} \times CF$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDF_w$$

#### DEFINITION OF TERMS

Table 2-65: Terms, Values, and References for Water Heater Tank Wrap

Term	Unit	Value	Source
<i>HOU</i> , Annual hours of use for water heater tank	$\frac{hours}{year}$	8,760	-
<i>η<sub>Elec</sub></i> , Thermal efficiency of electric heater element	Proportion	0.98	3
<i>R<sub>base</sub></i> , R-value is a measure of resistance to heat flow prior to adding tank wrap	$\frac{Hr \cdot ^\circ F \cdot ft^2}{BTU}$	Default: 12 or EDC Data Gathering	1
<i>R<sub>insul</sub></i> , R-value is a measure of resistance to heat flow after addition of tank wrap	$\frac{Hr \cdot ^\circ F \cdot ft^2}{BTU}$	Default: 20 or EDC Data Gathering	2
<i>A<sub>base</sub></i> , Surface area of storage tank prior to adding tank wrap	$ft^2$	See Table 2-66	-

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Term	Unit	Value	Source
$A_{insul}$ , Surface area of storage tank after addition of tank wrap	ft <sup>2</sup>	See Table 2-66	-
$\eta_{Elec}$ , Thermal efficiency of electric heater element	Proportion	0.98	3
$T_{setpoint}$ , Temperature of hot water in tank	°F	119	4
$T_{ambient}$ , Temperature of ambient air	°F	70	45
$HOU$ , Annual hours of use for water heater tank $ETDF_s$ , Summer Energy to Demand Factor	Hours/yr $\frac{kW}{kWh}$	8,760.0001046	8
$CF$ , $ETDF_w$ , Winter Energy to Demand Coincidence Factor	Proportion $\frac{kW}{kWh}$	1-0.0001755	8

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Table 2-66: Deemed savings Default Savings by water heater capacity Water Heater Capacity

Capacity (gal)	R <sub>base</sub>	R <sub>insul</sub>	A <sub>base</sub> (ft <sup>2</sup> ) <sup>40</sup>	A <sub>insul</sub> (ft <sup>2</sup> ) <sup>41</sup>	ΔkWh	$\frac{\Delta kW_{summer}}{peak}$	$\frac{\Delta kW_{winter}}{peak}$
30	8	16	19.16	20.94	139.4	0.04590145	0.0244
30	10	18	19.16	20.94	96.6	0.04400101	0.0170
30	12	20	19.16	20.94	70.6	0.00840074	0.0124
30	8	18	19.16	20.94	158.1	0.04800165	0.0277
30	10	20	19.16	20.94	111.6	0.04270117	0.0196
30	12	22	19.16	20.94	82.8	0.00940087	0.0145
40	8	16	23.18	25.31	168.9	0.04930177	0.0296
40	10	18	23.18	25.31	117.1	0.04340122	0.0205
40	12	20	23.18	25.31	85.5	0.00980089	0.0150
40	8	18	23.18	25.31	191.5	0.02490200	0.0336
40	10	20	23.18	25.31	135.1	0.04540141	0.0237
40	12	22	23.18	25.31	100.3	0.04440105	0.0176
50	8	16	24.99	27.06	183.9	0.02400192	0.0323
50	10	18	24.99	27.06	127.8	0.04460134	0.0224
50	12	20	24.99	27.06	93.6	0.04070098	0.0164
50	8	18	24.99	27.06	208.0	0.02370218	0.0365
50	10	20	24.99	27.06	147.1	0.04680154	0.0258
50	12	22	24.99	27.06	109.4	0.04250114	0.0192
80	8	16	31.84	34.14	237.0	0.02740248	0.0416
80	10	18	31.84	34.14	165.3	0.04890173	0.0290
80	12	20	31.84	34.14	121.5	0.04390127	0.0213

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<sup>40</sup> Area values were calculated from average dimensions of several commercially available units, with radius values measured to the center of the insulation. Area includes tank sides and top to account for typical wrap coverage.

<sup>41</sup> A<sub>insul</sub> was calculated by assuming that the water heater wrap is a 2" thick fiberglass material.

Capacity (gal)	R <sub>base</sub>	R <sub>insul</sub>	A <sub>base</sub> (ft <sup>2</sup> ) <sup>40</sup>	A <sub>insul</sub> (ft <sup>2</sup> ) <sup>41</sup>	ΔkWh	$\frac{\Delta kW_{summer}}{peak}$	$\frac{\Delta kW_{winter}}{peak}$
80	8	18	31.84	34.14	267.4	0.03050280	0.0469
80	10	20	31.84	34.14	189.6	0.02160198	0.0333
80	12	22	31.84	34.14	141.4	0.01610148	0.0248

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Area values were calculated from average dimensions of several commercially available units, with radius values measured to the center of the insulation. Area includes tank sides and top to account for typical wrap coverage.  $A_{insul}$  was calculated by assuming that the water heater wrap is a 2" thick fiberglass material.

## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

- 1) Conservative estimate of R-12.
- 2) The water heater wrap is assumed to be a fiberglass blanket with R-8, increasing the total to R-20.
- 3) AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. <https://nextgen.ahridirectory.org/Search/QuickSearch?category=8&searchTypeId=3&productType=15> Weblink
- 4) [Pennsylvania Act 129 2014 Residential Baseline Study. Section 4.6.1, pg 60, Table 4-64. Weblink](#)
- 5) [Pennsylvania Act 129 2014 Residential Baseline Study. Section 5.4.4, pg 104. Weblink](#)
- 6) [California Electronic Technical Reference Manual. "Water Heater Tank Wrap". Accessed December 2023. Weblink.](#)
- 4) ~~U.S. Department of Energy. Pennsylvania Statewide Residential End-Use and Saturation Study, 2014, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014\\_PA\\_Statewide\\_Act129\\_Residential\\_Baseline\\_Study.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014_PA_Statewide_Act129_Residential_Baseline_Study.pdf).~~
- 5) ~~California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.~~
- 6) "Energy Savers", U.S. Department of Energy, accessed June, 2018 <https://www.energy.gov/energysaver/services/do-it-yourself-energy-savings-projects/savings-project-insulate-your-water>
- 7) (2018). Do-It-Yourself Savings Project: Insulate Water Heater Tank. Weblink
- 8) [Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink](#)

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### 2-3-52.3.4 WATER HEATER TEMPERATURE SETBACK

Target Sector	Residential Establishments
Measure Unit	Water Heater Temperature
Measure Life	2 years <sup>Source 169</sup>
Vintage	Retrofit

In homes where the water heater setpoint temperature is set high, savings can be achieved by lowering the setpoint temperature. The recommended lower setpoint is 120°F, but EDCs may substitute another if needed. Savings occur only when the lower temperature of the hot water does not require the use of more hot water. Savings do not occur in applications such as a shower or faucet where the user adjusts the hot water flow to make up for the lower temperature. Clothes washer hot water use and water heater tank losses are included in the savings calculation, but shower, faucet, and dishwasher use are not included due to expected behavioral and automatic (dishwasher) adjustments in response to lower water temperature. It is expected that the net energy use for the dish washer hot water will remain the same after a temperature reduction because dishwashers will adjust hot water temperature to necessary levels using internal heating elements.

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#### ELIGIBILITY

This protocol documents the energy savings attributed to reducing the electric or heat pump water heater temperature setpoint. The primary target sector is single-family residences.

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#### ALGORITHMS

The annual energy savings calculation utilizes average performance data for available residential water heaters and typical water usage for residential homes. The energy savings are obtained through the following formula, where the first term in the parentheses corresponds to tank loss savings and the second to clothes washer savings:

$$\Delta kWh = \frac{(T_{hot i} - T_{hot f})}{3412 \frac{BTU}{kWh}} \times \left( \frac{A_{tank} \times 8760 \frac{hrs}{yr}}{R_{tank} \times \eta_{elec}} + \frac{Cycles_{wash} \times V_{HW} \times 8.3 \frac{BTU}{gal \cdot ^\circ F}}{UEF_{WH}} \right) \frac{(T_{ho i} - T_{hot f})}{3412} \times \left( \frac{A_{tank} \times 8760}{R_{tank} \times \eta_{elec}} + \frac{Cycles_{wash} \times V_{HW} \times 8.3 \frac{BTU}{gal \cdot ^\circ F}}{UEF_{WH}} \right)$$

~~Demand savings result from reduced hours of operation of the heating element, rather than a reduced connected load. The demand reduction is taken as the annual energy savings multiplied by the ratio of the average demand between 2 PM and 6 PM on summer weekdays to the total annual energy usage.~~

$$kWh_{peak} = ETDF \times \Delta kWh$$

ETDF (Energy to Demand Factor) is defined below:

$$ETDF = \frac{\text{Average Demand}_{\text{Summer WD 2PM-6PM}}}{\text{Annual Energy Usage}}$$

The ratio of the average demand between 2 PM and 6 PM on summer weekdays to the total annual energy usage is taken from an electric water heater metering study performed by BG&E. <sup>Source-8</sup>

$$\Delta kW_{summer\ peak} = ETDf_s \times \Delta kWh$$

$$\Delta kW_{winter\ peak} = ETDf_w \times \Delta kWh$$

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**DEFINITION OF TERMS**

Table 2-67: Terms, Values, and References for Water Heater Temperature Setback

Term	Unit	Values	Source
$UEF_{WH,i}$ , Uniform Energy Factor $T_{hot,i}$ , Temperature setpoint of water heater initially	Proportion °F	EDC data collection Data Gathering Default: Electric Storage=0.90 HPWH= 2.00_130	45
$R_{tank}$ , R value $T_{hot,f}$ , Temperature setpoint of water heater tank after setback	$\frac{hr \cdot °F \cdot ft^2}{BTU}$	EDC Data Gathering data collection Default: 12_119	910
$A_{tank}$ , Surface Area of water heater tank	ft <sup>2</sup>	EDC Data Gathering Default: 24.99	50 gal. value in Table 2-54 Table 2-66
$R_{tank}$ , R value of water heater tank	$\frac{hr \cdot °F \cdot ft^2}{BTU}$	EDC Data Gathering Default: 12	8
$\eta_{elec}$ , Thermal efficiency of electric heater element (equiv. to COP for HPWH)	Proportion	Electric Storage: 0.98 HPWH: 2.103_11	1, 2, 3
$V_{HW}$ , Volume of hot water used per cycle by clothes washer	$\frac{gallons}{cycle}$	7	4
$Cycles_{wash}$ , Number of clothes washer cycles per year	$\frac{cycles}{yr}$	Clothes washer present: 251 178 No clothes washer: 0	54
$T_{hot,i}$ , Temperature setpoint $V_{HW}$ , Volume of hot water heater initially used per cycle by clothes washer	$\frac{gallons}{cycle}$	EDC Data Gathering Default: 130_25	63
$T_{hot,f}$ , Temperature setpoint $UEF_{WH,s}$ , Uniform Energy Factor of water heater after setback	Proportion °F	EDC data collection Default: 149 Electric Storage= 0.92 HPWH= 3.20	76
$ETDF_s$ , $ETDF_s$ , Summer Energy To Demand Factor (defined above)	$\frac{kW}{kWh/yr}$	0.000080470001057	87
$ETDF_w$ , Winter Energy To Demand Factor	$\frac{kW}{kWh}$	0.0001761	7

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**DEFAULT SAVINGS**

The energy savings and demand reductions are prescriptive according to the above formulae. However, some values for common configurations are provided in Table 2-68, below.

**Table 2-68: Default Energy Savings and Demand Reductions**

Type	Cycles <sub>was</sub> h	η <sub>elec</sub>	UEF <sub>WH</sub>	ΔkWh Energy Savings (ΔkWh)	Demand Reduction (ΔkW <sub>peak</sub> ) ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
Electric Storage	0	0.98	<del>0.90</del> 1.03	60.0	0.00480063	0.0106
Electric Storage w/Clothes Washer	254200	0.98	1.03	189.9	0.900199	0.0090033
HPWH	0	<del>2.43</del> 11	2.0080	18.9	28.00020	0.00230033
HPWH w/Clothes Washer	251	<del>2.43</del> 11	2.0080	54.567.0	0.00410070	0.0117

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**EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of water heater temperature setpoint coupled with assignment of stipulated energy savings.

**SOURCES**

- 1) Previous Federal Standards from 2004-2015 are 0.97 – 0.00132 x Rated Storage in Gallons. For a 60-gallon tank this is 0.90. “Energy Conservation Program: Energy Conservation Standards for Residential Water Heaters, Direct Heating Equipment, and Pool Heaters” US Dept of Energy Docket Number: EE-2006-BT-STD-0129, p. 30. The previous, long-standing requirements are used since this is a Retrofit measure applied to existing equipment, not new equipment.
- 2) AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. <https://www.ahridirectory.org/Search/QuickSearch?category=8&searchTypeId=3&producttype=15> Weblink



- 2) If HPWH UEF is known but COP of HPWH compressor is unknown, assume compressor efficiency is UEF/0.9. This yields a default COP of 3.11. Maryland EmPOWER Technical Reference Manual. (2023, version 11.0). "Water Heater Temperature Setback".
- 3) United States Department of Energy. Reduce Hot Water Use for Energy Savings. Weblink
- 3) U.S. Department of Energy. NEEA Heat Pump Water Heater Field Study Report. Prepared by Fluid Market Strategies. October 22, 2013. <http://neea.org/docs/default-source/reports/heat-pump-water-heater-field-study-report.pdf?sfvrsn=5>
- 4) Federal Energy Management Program Energy Cost Calculator, March 2010 (visited October 23, 2018) <https://www.energy.gov/node/789966>
- 5) 4) (2023). 2020 Residential Energy Consumption Survey. Weblink Calculated using "Frequency of clothes washer use" and "Frequency of dryer use" data for the Mid-Atlantic region from U.S. Department of Energy. 2015 Residential Energy Consumption Survey Pennsylvania. (2015). <https://www.eia.gov/consumption/residential/data/2015/index.php?view=microdata>
- 6) 5) Engineering assumption
- 7) Pennsylvania Statewide Residential End-Use and Saturation Study, 2014, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014\\_PA\\_Statewide\\_Act129\\_Residential\\_Baseline\\_Study.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014_PA_Statewide_Act129_Residential_Baseline_Study.pdf).
- 8) Straub, Mary and Switzer, Sheldon. "Using Available Information for Efficient Evaluation of Demand Side Management Programs". Study by BG&E. The Electricity Journal. Aug/Sept, 2011. p. 95. <http://www.sciencedirect.com/science/article/pii/S1040619011001941>
- 9) 1) Conservative estimate of R-12
- 6) Pennsylvania Act 129 2023 Residential Baseline Study. Section 8.3.5, pg 128, Table 110. Weblink
- 7) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink
- 8) Conservative estimate of R-12
- 9) Illinois Statewide Technical Reference Manual for Energy Efficiency Version 7. (2023, version 11.0. Effective January). "5.4.6 Water Heater Temperature Setback". Weblink
- 10) Pennsylvania Act 129 2014 Residential Baseline Study. Section 4.6.1, 2019.pg 60, Table 4-64. <http://www.ilsag.info/technical-reference-manual.html>Weblink

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### 2-3-62.3.5 WATER HEATER PIPE INSULATION

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Water Heater
<b>Measure Life</b>	43 years <sup>Source 3</sup>
<b>Measure Life</b>	11 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

This measure relates to the installation of foam insulation on exposed pipe in unconditioned space. The baseline for this measure is a standard efficiency 50 gallon electric water heater (UEF=0.920792) with an annual energy usage of 2,939 kWh. <sup>42</sup>See 2.3.1 Heat Pump Water Heaters section for baseline water heater consumption formula and assumptions.

#### ELIGIBILITY

This protocol documents the energy savings for an electric water heater attributable to insulating exposed pipe in unconditioned space to R-3 or above. ~~The target sector primarily consists of residential establishments.~~

#### ALGORITHMS

~~The annual energy savings are assumed to be 3% of the annual energy use of an electric water heater (2,939 kWh), or 88.2 kWh based on 10 feet of 3/4" thick insulation (equal to R-3 on a 1/2" pipe). This estimate is based on a recent report prepared by the ACEEE for the State of Pennsylvania (Source 1). On a per foot basis, this is equivalent to 8.82 kWh.~~

~~$$\Delta kWh = 8.82 \text{ kWh/yr per foot of installed insulation}$$~~

~~The summer coincident peak kW savings are calculated as follows:~~

~~$$\Delta kW_{peak} = \Delta kWh \times ETDf$$~~

~~The algorithms below calculate the total savings resulting from adding insulation to uninsulated pipes.~~

~~$$\Delta kWh = \left( \frac{1}{R_{exist}} - \frac{1}{R_{new}} \right) \times C_{inside} \times L_{effective} \times (T_{setpoint} - T_{ambient}) \times \frac{1}{\eta_{elec}} \times HOU \times \frac{1}{3412} \times ISR$$~~

~~$$L_{effective} = L_{horizontal} + (\alpha \times L_{vertical})$$~~

~~$$\Delta kW_{summer peak} = \Delta kWh \times ETDf_s$$~~

~~$$\Delta kW_{winter peak} = \Delta kWh \times ETDf_w$$~~

<sup>42</sup> See 2.3.1 Heat Pump Water Heaters section for baseline water heater consumption formula and assumptions.

**DEFINITION OF TERMS**

**Table 2-69: Terms, Values, and References for Water Heater Pipe Insulation**

Term	Unit	Value	Source
$R_{exist}$ , Pipe heat loss coefficient of existing uninsulated pipe	$\frac{hr \cdot ^\circ F \cdot ft^2}{BTU}$	See Table	2
$R_{new} = R_{exist} + R$ value of new insulation, Pipe heat loss coefficient of new insulated pipe	$\frac{hr \cdot ^\circ F \cdot ft^2}{BTU}$	EDC Data Gathering	-
$\Delta kWh$ , annual energy savings per foot of installed pipe insulation $C_{inside}$ , Inside circumference of pipe	$\frac{kWh}{yr} \cdot ft$	8-82EDC Data Gathering	47, 8
$L_{horizontal}$ , Length of pipe from water heating source which runs horizontally	ft	EDC Data Gathering	-
$L_{vertical}$ , Length of pipe from water heating source which runs vertically	ft	EDC Data Gathering	-
$\alpha$ , Horizontal to Vertical Adjustment Factor	None	See Table 2-70	6
$T_{setpoint}$ , Temperature of hot water in tank	$^\circ F$	119	10
$T_{ambient}$ , Temperature of ambient air	$^\circ F$	70	3
$\eta_{elec}$ , Thermal efficiency of electric heater element	Proportion	0.98	4
$HOU$ , Annual hours of use for water heater tank	$\frac{hours}{yr}$	8760	-
$ISR$ , In-service rate	%	EDC Data Gathering Direct Install Default: 100%	-
$ETDF, ETDF_s$ , Summer Energy to Demand Factor	$\frac{kW}{kWh/yr} \cdot \frac{kW}{kWh}$	0.000080470001046	25
$\Delta kW_{peak}$ , Summer peak kW savings per foot of installed pipe insulation $ETDF_w$ , Winter Energy To Demand Factor	$\frac{kW}{ft} \cdot \frac{kW}{kWh}$	0.000740001755	-5

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The demand reduction is taken as the annual energy savings multiplied by the ratio of the average energy usage during 2 PM to 6 PM on summer weekdays to the total annual energy usage. The Energy to Demand Factor is defined as:

$$ETDF = \frac{\text{Average Demand}_{\text{Summer WD 2PM-6PM}}}{\text{Annual Energy Usage}}$$

The ratio of the average energy usage between 2 PM to 6 PM on summer weekdays to the total annual energy usage is taken from an electric water heater metering study performed by BG&E.<sup>Source-2</sup>

**Table 2-70: Existing R-Values, Inside Circumference, and Horizontal to Vertical Adjustment Factor of Common Water Pipe Sizes and Materials**

Type and Size	R <sub>exist</sub>	C <sub>inside</sub>	α
½" Copper Pipe	0.444	0.1427	0.67
¾" Copper Pipe	0.521	0.2055	0.72
½" PEX	0.332	0.1270	0.73
¾" PEX	0.374	0.1783	0.77

### EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with assignment of stipulated energy savings.

### SOURCES

- 1) American Council for an Energy Efficient Economy, Summit Blue Consulting, Vermont Energy Investment Corporation, ICF International, and Synapse Energy Economics, Potential for Energy Efficiency, Demand Response, and Onsite Solar Energy in Pennsylvania, Report Number E093, April 2009, p. 117.
- 2) Straub, Mary and Switzer, Sheldon. "Using Available Information for Efficient Evaluation of Demand Side Management Programs". Study by BG&E. The Electricity Journal. Aug/Sept, 2011. p. 95. <http://www.sciencedirect.com/science/article/pii/S1040619011001941>
- 3) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, [http://www.deeresources.com/files/DEER2020/download/SupportTable\\_EUL2020.xlsx](http://www.deeresources.com/files/DEER2020/download/SupportTable_EUL2020.xlsx). Accessed November 13, 2018
- 1) California Electronic Technical Reference Manual. "Water Heater Pipe Wrap, Residential". Accessed December 2023. Weblink
- 2) Illinois Statewide Technical Reference Manual. (2023, version 11.0). "5.4.1 Domestic Hot Water Pipe Insulation". Weblink
- 3) Pennsylvania Act 129 2014 Residential Baseline Study. Section 5.4.4, pg 104. Weblink
- 4) AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. Weblink
- 5) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink
- 6) In cases with zero wind, heat loss (and therefore) savings is larger from horizontal pipe configurations than vertical pipe configurations due, perhaps to the way in which convective losses are handled. Given that most DHW pipe insulation installations begin with a vertical orientation from the water heater, an adjustment to the engineering calculation is needed. An analysis performed by the IL-TRM Technical Advisory Committee of the 3E PLUS tool by NAIMA yielded adjustment factors for horizontal to vertical loss and savings values. Weblink
- 7) Thomas, Varkie C. Pipe Sizing Charts Tables. Energy Models. Weblink
- 8) The Engineering Toolbox. (2018). ASTM F876 - PEX Tube – Dimensions. Weblink

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- 9) [Cadmus for PPL Electric Utilities. \(2022, September\). PPL Electric Utilities Annual Report to the Pennsylvania Public Utility Commission Phase IV of Act 129 PY13 Annual Report \(June 1, 2021 – May 31, 2022\). Appendix I. Evaluation Detail – Energy Efficient Homes Component, pg I-6, Table I-5. Weblink](#)
- 10) [Pennsylvania Act 129 2014 Residential Baseline Study. Section 4.6.1, pg 60, Table 4-64. Weblink](#)

### 2.3.72.3.6 LOW-FLOW FAUCET AERATORS

Target Sector	Residential Establishments
Measure Unit	Aerator
Measure Life	10 years <sup>Source 1</sup>
Vintage	Retrofit, New Construction

Installation of low-flow faucet aerators is an inexpensive and lasting approach for water conservation. These efficient aerators reduce water consumption and consequently reduce hot water usage and save energy associated with heating the water. This protocol presents the assumptions, analysis, and savings from replacing standard flow aerators with low-flow aerators in kitchens and bathrooms.

~~The low-flow kitchen and bathroom aerators will save on the electric energy usage due to the reduced demand of hot water.~~

#### ELIGIBILITY

This protocol documents the energy savings attributable to efficient low-flow aerators in residential applications. Laminar flow restrictors are also eligible. The maximum flow rate of qualifying equipment is 1.5 gallons per minute. Homes with non-electric water heaters do not qualify for this measure.

#### ALGORITHMS

The energy savings and demand reduction are obtained through the following calculations:

$$\Delta kWh = \frac{(GPM_{base} - GPM_{low}) \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in})}{3412 \frac{BTU}{kWh} \times RE} \times \frac{(GPM_{base} - GPM_{low}) \times 8.3 \times (T_{out} - T_{in})}{3412 \times RE}$$

$$\times \frac{DF \times T_{person-day} \times N_{persons} \times 365 \frac{days}{yr}}{N_{faucets-home}} \times ISR \times ELEC$$

$$\Delta kWh_{peak} kW_{summer\ peak} = \Delta kWh \times ETDF \times ETDf_s$$

Where:

$$ETDF = \frac{CF}{HOU} = \frac{\%_{faucet\ use,\ peak} \times 60 \frac{minutes}{hour}}{365 \frac{days}{yr} \times 240 \frac{minutes}{daily\ peak}}$$

Given:

$$CF = \frac{\%_{faucet\ use,\ peak} \times T_{person-day} \times N_{persons}}{N_{faucets-home} \times 240 \frac{minutes}{daily\ peak}}$$

$$HOU = \frac{T_{person-day} \times N_{persons} \times 365 \frac{days}{yr}}{N_{faucets-home} \times 60 \frac{minutes}{hour}}$$

~~The ratio of the average energy usage during 2 PM and 6 PM on summer weekdays to the total annual energy usage is taken from average daily load shape data collected for faucets from an~~

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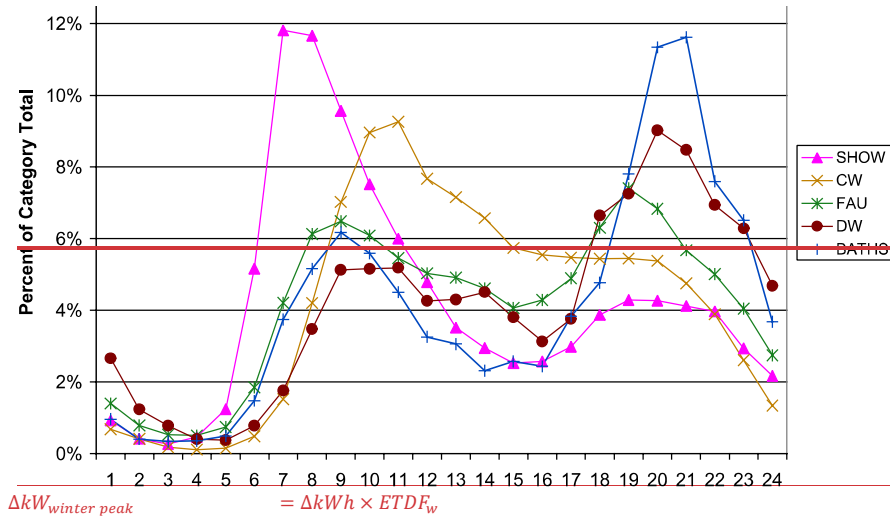
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Aquacraft, Inc study.<sup>Source 2</sup> The average daily load shapes (percentages of daily energy usage that occur within each hour) are plotted in Figure 2-1 below (symbol FAU represents faucets).<sup>43</sup>

Figure 2-1: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup>



**DEFINITION OF TERMS**

Table 2-71: Low-Flow Faucet Aerator Calculation Assumptions

Term	Unit	Value	Source
$GPM_{base}$ , Average baseline aerator flow rate of aerator (GPM)	$\frac{gallons}{minute}$	EDC Data Gathering or Default = 2.2	32
$GPM_{low}$ , Average post-measure efficient aerator flow rate of aerator (GPM)	$\frac{gallons}{minute}$	EDC Data Gathering or Default = 1.5	32
$T_{person-day T_{out}}$ , Average time of hot mixed water usage per person per day (minutes/temperature flowing from the faucet (°F))	$\frac{minutes}{person-day} \cdot F$	Kitchen=4.593.0 Bathroom=1.686.0 Unknown=6.487.8	45
$N_{persons T_{in}}$ , Average number/temperature of persons per household water entering the house (°F)	$\frac{persons}{house} \cdot F$	Default SF=2.5 53 Default MF=1.7 Default Unknown=2.5 Or EDC Data Gathering	116
$T_{out}$ , Average mixed water temperature flowing from the faucet (°F) RE, Recovery efficiency of electric water heater	$Proportion \cdot F$	Kitchen=Default: Standard: 0.98 HPWH: 3.93 Bathroom=86	67

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<sup>43</sup> SHOW = showers, CW = clothes washers, FAU = Faucets, DW = dishwashers, BATHS = baths. FAU is the relevant curve for this measure.

Term	Unit	Value	Source
		Unknown=87.8; 1.22	
$T_{in}$ , Average temperature of water entering the house ( $^{\circ}$ F) flowing down drain	$^{\circ}$ F	Kitchen=75% Bathroom=90% Unknown=79.5%	78
$RE$ , Recovery efficiency of electric hot water heater usage per person per day (minutes)	$\frac{minutes}{person \cdot day}$	Default: Standard: 0.98 HPWH: Kitchen=4.5 Bathroom=1.6 Unknown=2.47	8, 103
ETDF, Energy To Demand Factor Average number of persons per household	$\frac{kWh}{person \cdot year}$	Default SF=2.6 Default MF=1.7 Default Unknown=2.4 Or EDC Data Gathering 0.000434	29
$N_{faucets-home}$ , Average number of faucets in the home	$\frac{faucets}{house}$	EDC Data Gathering, Default see Table 2-59 Table 2-72	54
$DF$ , Percentage of water flowing down drain In-Service Rate	%	Kitchen=75% Bathroom=90% Unknown=79.5% EDC Data Gathering, Kit Delivery Default: 26% Direct Install Default: 100%	910
$ELEC$ , Percentage of homes with electric water heat In-Service Rate	%	Default: Unknown=47% Or EDC Data Gathering: Kit Delivery Default: 28% Direct Install Default: Electric = 100% Fossil Fuel = 0%	EDC Data Gathering, 424
$ETDF$ , Summer Energy to Demand Factor Percentage of homes with electric water heat	$\frac{\% kWh}{kWh}$	Default: SF: 0.0001057 MF: 0.0001006 Unknown=35%: 0.0001046 Or EDC Data Gathering: Electric = 100% Fossil Fuel = 0.0%	511
$\%_{faucet-use:peak}$ , percentage of daily faucet use during PJM peak period $ETDF_w$ , Winter Energy to Demand Factor	$\frac{\% kWh}{kWh}$	49.5% SF: 0.0001761 MF: 0.0001733 Unknown: 0.0001755	211

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Table 2-72: Average Number of Faucets per Home

Faucet Type	Single Family	Multifamily	Unknown
Kitchen	1.42	1.01	1.02



Bathroom	2.26	1.24	2.0
Unknown	3-31.9	21.2	3-01.7

### DEFAULT SAVINGS

Default savings assume an electric resistance storage water heater with RE = 0.98.

Table 2-62: Default Savings for Low-Flow Faucet Aerators

Housing Type	Faucet Location	Water Heater Fuel (%-electric)	Kit Delivery: Unit Energy Savings (kWh)	Kit Delivery: Unit Demand Savings (kW)	Direct Install: Unit Energy Savings (kWh)	Direct Install: Unit Demand Savings (kW)
Single Family	Kitchen	Unknown (35%)	19.5	0.0026	69.8	0.0094
	Bathroom	Unknown (35%)	3.5	0.0005	12.3	0.0017
	Unknown	Unknown (35%)	8.2	0.0011	29.2	0.0039
Multifamily	Kitchen	Unknown (35%)	14.6	0.0020	52.2	0.0070
	Bathroom	Unknown (35%)	4.3	0.0006	15.4	0.0021
	Unknown	Unknown (35%)	8.3	0.0011	29.8	0.0040
Statewide (Unknown Housing Type)	Kitchen	Unknown (35%)	21.5	0.0029	76.8	0.0103
	Bathroom	Unknown (35%)	3.8	0.0005	13.6	0.0018
	Unknown	Unknown (35%)	9.0	0.0012	32.1	0.0043
Single Family	Kitchen	Electric (100%)	55.8	0.0075	199.5	0.0267
	Bathroom	Electric (100%)	9.9	0.0013	35.3	0.0047
	Unknown	Electric (100%)	23.4	0.0031	83.4	0.0112
Multifamily	Kitchen	Electric (100%)	41.8	0.0056	149.2	0.0200
	Bathroom	Electric (100%)	12.3	0.0017	44.0	0.0059
	Unknown	Electric (100%)	23.8	0.0032	85.1	0.0114
Statewide (Unknown Housing Type)	Kitchen	Electric (100%)	61.4	0.0082	219.4	0.0294
	Bathroom	Electric (100%)	10.9	0.0015	38.8	0.0052
	Unknown	Electric (100%)	25.7	0.0034	91.8	0.0123

### EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with EDC Data Gathering.

### SOURCES

- 1) California's Database of Energy Efficiency Resources (DEER), updated 2/5/2014. <http://www.deeresources.com/files/DEER2013codeUpdate/download/DEER2014-EUL-table-update-2014-02-05.xlsx>
- 2) Aquacraft, Inc., Water Engineering and Management. The end use of hot water in single family homes from flow trace analysis. 2001. <http://s3.amazonaws.com/zanran-storage/www.aquacraft.com/ContentPages/47768067.pdf>. The statewide values were used for inputs in the ETRDF algorithm components. The CF for faucets is found to be 0.00413:  $\{ \% \text{ faucet use during peak} \times (T_{\text{Person-Day}} \times N_{\text{Person}}) / (N_{\text{faucets-home}}) \} / 240 \text{ (minutes in peak period)} = [19.5\% \times (6.1 \times 2.5 / 3.0)] / 240 = 0.00413$ . The Hours for

faucets is found to be 30.9:  $(T_{\text{Person-Day}} \times N_{\text{Persons}} \times 365) / (N_{\text{faucets-home}}) / 60 = (6.1 \times 2.5 \times 365) / 3.0 / 60 = 30.9$ . The resulting  $F_{HD}$  is calculated to be 0.000134:  $CF / \text{Hours} = 0.00413 / 30.9 = 0.000134$ .

- 1) [California Electronic Technical Reference Manual. "Faucet Aerator, Residential". Accessed November 2023. Weblink](#)
- 2) [10 CFR 430.32\(o\). Weblink](#)
- 3) ~~Cadmus and Opinion Dynamics Evaluation Team. for Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. (2013, June 2013. Baseline GPM of replaced aerators is set to the federal minimum GPM of 2.2. The GPM of new aerators is set to the typical rated GPM value of 1.5 GPM. Discounted GPM flow rates were not applied because the "throttle factor" adjustment was found to have been already accounted for in the mixed water temperature variable. Additionally, the GPM<sub>Base</sub> was set to a default value of 2.2 due to the inability to verify what the GPM flow rate was of the replaced faucet.~~
- 4) ~~3) Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. If 2.7 min/person/day for unknown aerator location is known, use the corresponding kitchen/bathroom value. If unknown, use 6.1 min/person/day calculated as the weighted average length of use value, which is the total for the household: kitchen (4.5 and bathroom min/person/day) + bathroom (1.6 min/person/day) = 6.1 min/person/day. by average kitchens and bathrooms per home from the 2023 PA residential baseline study.~~
- 5) ~~Pennsylvania Act 129 2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf).~~
- 4) ~~Table 7. NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Pg 122, table 105 (ELEC). Pg 130, table 112 (N<sub>faucets-home</sub>). Weblink Single-family average faucets calculated as weighted average of single-family attached and single-family detached using 2023 Pennsylvania residential baseline study data.~~
- 6) ~~5) Cadmus and Opinion Dynamics Evaluation Team. for Michigan Evaluation Working Group. (2013, June). Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. Table 7. The study finds that the average mixed water temperature flowing from the kitchen and bathroom faucets is 93°F and 86°F, respectively. If the faucet location is unknown, 87.8°F is the corresponding value to be used, which was calculated by taking a weighted average of faucet type (using the statewide values):  $(1 \times 93 + 3 \times 86) / (1 + 3) = 87.8$ .~~
- 7) ~~6) Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40-inch depth is 51.86452.502. Calculated using Daily SCAN Standard - Period of Record data from April 1999 December 2003 to December 2018 2023 from the Natural Resource Conservation Service Database. [https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\\_scan\\_per&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily_scan_per&state=PA) Weblink. Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p.(2017, March). "2.6.1 Water Heater". Pg 78. <https://energy.mo.gov/sites/energy/files/MOTRM2017Volume2.pdf> Weblink~~
- 8) ~~7) AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. <https://www.ahridirectory.org/Search/SearchForm?programId=24&searchTypeId=2> Average recovery efficiency for heat pump water heaters is 3.93. Accessed December 2023. Weblink 1.22 for unknown type calculated as the weighted average of electric resistance and HPWH recover efficiencies by the relative proportions of electric resistance and HPWHs from the 2023 PA residential baseline study.~~

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- 9)8) Illinois TRM Effective June 1, Statewide Technical Reference Manual. (2013, version 11.0). "5.4.4 Low Flow Faucet Aerators". Weblink. Faucet usages are at times dictated by volume, and only "directly down the drain" usage will provide savings. Due to the lack of a metering study that has determined this specific factor, the Illinois Technical Advisory Group has deemed these values to be 75% for the kitchen and 90% for the bathroom. If the aerator location is unknown, an average of 79.5% should be used, which is based on the assumption that 70% of household water runs through the kitchen faucet and 30% through the bathroom  $(0.7 \times 0.75 + 0.3 \times 0.9) = 0.795$ .
- 10) NEEA Heat Pump Water Heater Field Study Report. Prepared by Fluid Market Strategies. October 22, 2013. <https://neea.org/img/uploads/heat-pump-water-heater-field-study-report.pdf>.
- 11)9) U.S. Census Bureau, 2017-2021 American Community Survey 5-Year (2013-2017) Estimates for 2017. <http://data.census.gov>. Weblink
- 12) Average of PY9 values for kit delivery for FirstEnergy EDCs. [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/electric\\_distribution\\_company\\_act\\_129\\_reporting\\_requirements.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/electric_distribution_company_act_129_reporting_requirements.aspx)

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- 10) Weighted average of ISRs from surveys of FirstEnergy customers that received aerators in kits in PY13 and PY14.
- 11) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

### 2-3.82.3.7 LOW-FLOW SHOWERHEADS

Target Sector	Residential Establishments
Measure Unit	Water Heater Showerhead
Measure Life	910 years <sup>Source 1</sup>
Vintage	Retrofit, New Construction

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This measure relates to the installation of a low-flow (generally 1.5 GPM) showerhead in bathrooms in homes with an electric water heater. The baseline is a standard showerhead using 2.5 GPM.

#### ELIGIBILITY

This protocol documents the energy savings attributable to replacing a standard showerhead with an energy-efficient low-flow showerhead for electric water heaters. The target sector primarily consists of residential establishments.

#### ALGORITHMS

The annual energy savings are obtained through the following formula:

$$\Delta kWh = \frac{(GPM_{base} - GPM_{low}) \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in})}{3412 \frac{BTU}{kWh} \times RE} \times \frac{(GPM_{base} - GPM_{low}) \times 8.3 \times (T_{out} - T_{in})}{3412 \times RE} \times \frac{T_{person-day} \times N_{persons} \times N_{showers-day} \times 365 \frac{days}{yr}}{N_{showerheads-home}} \times \frac{ISR \times ELEC}{N_{showerheads-h}}$$

$$\Delta kWh_{peak} kW_{summer\ peak} = \Delta kWh \times ETDF \times ETDf_s$$

Where:

$$ETDF = \frac{CF}{HOU} = \frac{\%_{showers-use,peak} \times 60 \frac{minutes}{hour}}{365 \frac{days}{yr} \times 240 \frac{minutes}{daily\ peak}}$$

Given:

$$CF = \frac{\%_{showers-use,peak} \times T_{person-day} \times N_{persons} \times N_{showers-day}}{N_{showerheads-home} \times 240 \frac{minutes}{daily\ peak}}$$

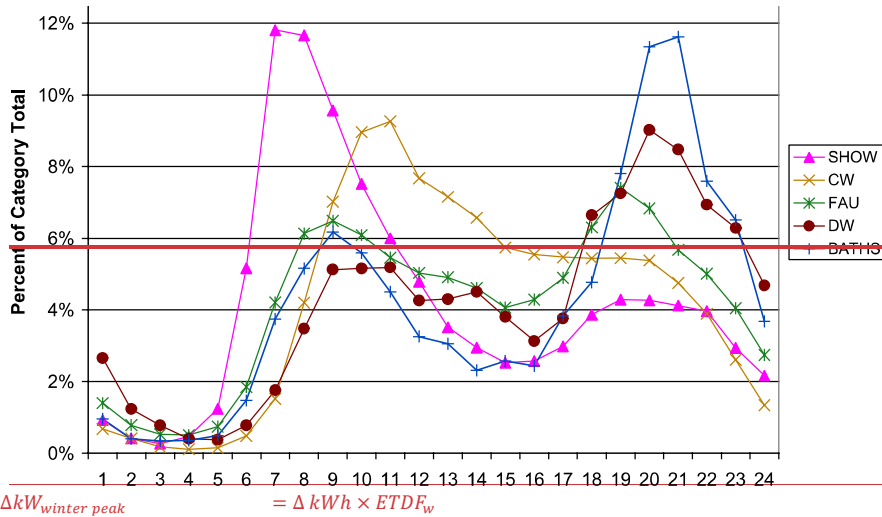
$$HOU = \frac{T_{person-day} \times N_{persons} \times N_{showers-day} \times 365 \frac{days}{yr}}{N_{showerheads-home} \times 60 \frac{minutes}{hour}}$$

The ratio of the average energy usage during 2-PM and 6-PM on summer weekdays to the total annual energy usage is taken from average daily load shape data collected for showerheads from an Aquacraft, Inc study.<sup>Source 2</sup> The average daily load shapes (percentages of daily energy usage that occur within each hour) during are plotted in Figure 2-2 below (symbol SHOW represents showerheads).<sup>44</sup>

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<sup>44</sup> SHOW = showers, CW = clothes washers, FAU = Faucets, DW = dishwashers, BATHS = baths. SHOW is the relevant curve for this measure.

Figure 2-2: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup>



**DEFINITION OF TERMS**

Table 2-73: Terms, Values, and References for Low-Flow Showerhead

Term	Unit	Value	Source
$GPM_{base}$ , Gallons per minute of baseline showerhead	$\frac{gallons}{minute}$	EDC Data Gathering or Default = 2.5	32
$GPM_{low}$ , Gallons per minute of low-flow showerhead	$\frac{gallons}{minute}$	EDC Data Gathering	EDC Data Gathering
$T_{out}$ , Assumed temperature of water used by showerhead $T_{person-day}$ , Average time of shower usage per person (minutes)	$\frac{minutes \cdot F}{day}$	7.8101	57
$T_{in}$ , Assumed temperature of water entering house $N_{persons}$ , Average number of persons per household	$\frac{persons \cdot F}{hou}$	EDC Data Gathering or Default SF=2.5 Default MF=1.7 Default unknown=2.553	68
$N_{showers=day}$ , Average number of showers per person per day $RE$ , Recovery efficiency of electric water heater	$\frac{showers}{person \cdot day}$ <i>Prop ortion</i>	0.6 Default: Electric resistance: 0.98 HPWH: 3.93 Unknown: 1.22	79
$N_{showerheads=home}$ , Average number of showers in the home $T_{person-day}$ , Average shower usage per person (minutes)	$\frac{showers \cdot minutes}{house \cdot day}$	EDC Data Gathering or Default SF=1.6 Default MF=1.1 Default unknown=1.57.8	83

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Term	Unit	Value	Source
$N_{persons}$ , Average number of persons per household $T_{out}$ , Assumed temperature of water used by showerhead	$\frac{\circ F \cdot persons}{household}$	EDC Data Gathering or Default SF=2.6 Default MF=1.7 Default unknown=2.4044	94
$N_{showers-day}$ , Average number of showers per person per day $T_{in}$ , Assumed temperature of water entering house	$\frac{showers}{person \cdot day}$	520.6	405
$RE$ , Recovery efficiency of electric water heater $N_{showerheads-home}$ , Average number of showers in the home	$\frac{showers}{home}$ Proportion	EDC Data Gathering or Default: SF=1.9 Standard: 0.98 HPWH: 2.1 Default MF=1.2 Default unknown = 1.7	11, 136
$ETDF$ , Energy To Demand Factor $ISR$ , In-Service Rate	$\frac{kWh}{kWh_{peak}}$ %	0.0008014 EDC Data Gathering, Kit Default = 21% Direct Install Default = 100%	12 EDC Data Gathering, 10
$ELEC$ , Percentage of homes with electric water heat $ISR$ , In-Service Rate	%	EDC Data Gathering, or Kit Default = 35% Unknown=47% Direct Install Default Electric = 100% Fossil Fuel = 0%	EDC Data Gathering, 146
$ETDF$ , Summer Energy to Demand Factor $ELEC$ , Percentage of homes with electric water heat	$\frac{\% kWh}{kWh_{peak}}$	EDC Data Gathering or Default: SF: 0.0001057 MF: 0.0001006 Unknown=35% Electric = 100% Fossil Fuel = 0.0% 0.0001046	811
$\%_{shower-use,peak}$ , percentage of daily shower use during PJM peak period $ETDF_w$ , Winter Energy to Demand Factor	$\frac{\% kWh}{kWh_{peak}}$	11.7% SF: 0.0001761 MF: 0.0001733 Unknown: 0.0001755	42 11

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**DEFAULT SAVINGS**

Default savings assume an electric resistance storage water heater with RE = 0.98.

**Table 2-64: Default Savings for Low-Flow Showerheads**

Housing Type	Low-Flow Rate (gpm)	Water-Heater Fuel (%-electric)	Energy Savings per Unit (kWh)		Demand Savings per Unit (kW)	
			Kit Delivery	Direct Install	Kit Delivery	Direct Install
Single-Family	2.0	Unknown (35%)	19.9	56.8	0.0016	0.0046
	1.75	Unknown (35%)	29.8	85.2	0.0024	0.0068
	1.5	Unknown (35%)	39.8	113.6	0.0032	0.0094
Multifamily	2.0	Unknown (35%)	19.7	56.2	0.0016	0.0045
	1.75	Unknown (35%)	29.5	84.3	0.0024	0.0068
	1.5	Unknown (35%)	39.3	112.4	0.0032	0.0090
Statewide (Unknown Housing Type)	2.0	Unknown (35%)	21.2	60.6	0.0017	0.0049
	1.75	Unknown (35%)	31.8	90.9	0.0025	0.0073
	1.5	Unknown (35%)	42.4	121.2	0.0034	0.0097
Single-Family	2.0	Electric (100%)	56.8	162.3	0.0046	0.0130
	1.75	Electric (100%)	85.2	243.5	0.0068	0.0195
	1.5	Electric (100%)	113.6	324.6	0.0094	0.0260
Multifamily	2.0	Electric (100%)	56.2	160.5	0.0045	0.0129
	1.75	Electric (100%)	84.3	240.8	0.0068	0.0193
	1.5	Electric (100%)	112.4	321.1	0.0090	0.0257
Statewide (Unknown Housing Type)	2.0	Electric (100%)	60.6	173.1	0.0049	0.0139
	1.75	Electric (100%)	90.9	259.7	0.0073	0.0208
	1.5	Electric (100%)	121.2	346.3	0.0097	0.0278

**EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of installation coupled with EDC Data Gathering.

**SOURCES**

- 1) ~~Efficiency Vermont, Technical Reference User Manual: Measure Savings California Electronic Technical Reference Manual. "Low-Flow Showerheads". Accessed December 2023. Weblink~~
- 2) ~~10 CFR 430.32(p). Weblink~~
- 1) ~~Algorithms and Cost Assumptions, TRM User Manual No. 2008-53, 07/18/08, <http://www.veic.org/docs/ResourceLibrary/TRM-User-Manual-Excerpts.pdf>~~
- 2) ~~Aquacraft, Inc., Water Engineering and Management. The end-use of hot water in single family homes from flow trace analysis. 2001. <http://s3.amazonaws.com/zanran-storage/www.aquacraft.com/ContentPages/47768067.pdf>~~
- 3) ~~Cadmus and Opinion Dynamics Evaluation Team. for Michigan Evaluation Working Group. (2013, June). Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. Uses the federal minimum GPM allowed as the baseline for the replaced showerheads, corresponding to 2.5 GPM.~~



- 4) ~~Illinois TRM Effective June 1, 2013. Allows for varying flow rate of the low-flow showerhead, most notably values of 2.0 GPM, Table 6 1.75 GPM and 1.5 GPM. Custom or actual values are also allowed for.~~
- 5) ~~3) Table 6. Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. The study compared shower length by single-family and multifamily populations, finding no statistical difference in showering times. For the energy-saving analysis, the study used the combined single-family and multifamily average shower length of 7.8 minutes.~~
- 4) ~~U.S. Census Bureau, 2017-2021 American Community Survey 5-Year (2013-2017) Estimates. Weblink~~
- 5) ~~Cadmus and Opinion Dynamics Evaluation Team for Michigan Evaluation Working Group. (2013, June). Showerhead and Faucet Aerator Meter Study. Table 8. For each shower fixture metered, the evaluation team knew the total number of showers taken, duration of time meters remained in each home, and total occupants reported to live in the home. From these values, the average showers taken per day, per person was calculated. The study compared showers per day, per person by single-family and multifamily populations, finding no statistical difference in the values. For the energy-saving analysis, the study used the combined single-family and multifamily average showers per day, per person of 0.6.~~
- 6) ~~1) 2017. <http://factfinder.census.gov>.~~
- 7) ~~1) Table 8. Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. For each shower fixture metered, the evaluation team knew the total number of showers taken, duration of time meters remained in each home, and total occupants reported to live in the home. From these values average showers taken per day, per person was calculated. The study compared showers per day, per person by single-family and multifamily populations, finding no statistical difference in the values. For the energy-saving analysis, the study used the combined single-family and multifamily average showers per day, per person of 0.6.~~
- 8) ~~6) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 2018 Residential Baseline Study, Pg 122, table 105 (ELEC). Pg 130 table, 112 (N<sub>faucets-home</sub>). [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Weblink~~
- 7) ~~Cadmus and Opinion Dynamics Evaluation Team. for Michigan Evaluation Working Group. (2013, June). Showerhead and Faucet Aerator Meter Study. Temperature sensors provided the mixed water temperature readings resulting in an average of 101°F.~~
- 9) ~~1) Using Rock Spring, PA (Site 2036) as a proxy, the mean. For Michigan Evaluation Working Group. June 2013. Temperature sensors provided the mixed water temperature readings resulting in an average of 101°F.~~
- 10) ~~8) Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40-inch depth is 54.86452.502. Calculated using Daily SCAN Standard - Period of Record data from April 1999 December 2003 to December 2018 2023 from the Natural Resource Conservation Service Database. [https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\\_scan\\_por&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily_scan_por&state=PA) Weblink. Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p.(2017, March). "2.6.1 Water Heater". Pg 78. <https://energy.mo.gov/sites/energy/files/MO-TRM2017Volume2.pdf> Weblink~~
- 11) ~~AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. Average recovery efficiency for heat pump water heaters is 3.93. Accessed December 2023. <https://www.ahridirectory.org/NewSearch?programId=24&searchTypeId=Weblink3>~~
- 12) ~~9) Aquacraft, Inc., Water Engineering 1.22 for unknown type calculated as the weighted average of electric resistance and Management. The end-use HPWH recover efficiencies by~~

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the relative proportions of hot water in single-family-homes electric resistance and HPWHs from flow trace analysis, 2001.  
[http://s3.amazonaws.com/zanran\\_storage/www.aquacraft.com/ContentPages/47768067.pdf](http://s3.amazonaws.com/zanran_storage/www.aquacraft.com/ContentPages/47768067.pdf).  
The statewide values were used for inputs in the ETDF algorithm components. The CF for showerheads is found to be 0.00380:  $\{ \% \text{ showerhead use during peak} \times (T_{\text{person-day}} \times N_{\text{person}} \times N_{\text{showers-day}}) / (N_{\text{showerheads-home}}) \} / 240$  (minutes in peak period) =  $\{ 11.7\% \times (7.8 \times 2.5 \times 0.6 / 1.5) \} / 240 = 0.00371$ . The Hours for showerheads is found to be 47.5:  $(T_{\text{person-day}} \times N_{\text{persons}} \times 365) / (N_{\text{showerheads-home}}) / 60 = (7.8 \times 2.5 \times 0.6 \times 365) / 1.5 / 60 = 47.5$ . The resulting ETDF is calculated to be 0.00008014:  $CF / \text{Hours} = 0.00380 / 47.5 = 0.00008014$ the 2023 PA residential baseline study.

13) NEEA Heat Pump Water Heater Field Study Report. Prepared by Fluid Market Strategies. October 22, 2013. <https://neea.org/img/uploads/heat-pump-water-heater-field-study-report.pdf>

14) Average of PY9 values for kit delivery for FirstEnergy EDCs. [http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/electric\\_distribution\\_company\\_act\\_129\\_reporting\\_requirements.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/electric_distribution_company_act_129_reporting_requirements.aspx)

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- 10) Weighted average of ISRs from surveys of FirstEnergy customers that received showerheads in kits in PY13 and PY14.
- 11) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

**2-3.92.3.8 THERMOSTATIC SHOWER RESTRICTION VALVES**

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Water Heater
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

This measure relates to the installation of a device that reduces hot water usage during shower warm-up by way of a thermostatic shower restriction valve, reducing hot water waste during shower warm-up.

**ELIGIBILITY**

This protocol documents the energy savings attributable to installing a thermostatic restriction valve, device, or equivalent product on an existing showerhead. Only homes with electric water heaters are eligible. Savings associated with this measure may be combined with a low-flow showerhead as the sum of the savings of the two measures. ~~The target sector primarily consists of residences.~~

**ALGORITHMS**

**ALGORITHMS**

The annual energy savings are obtained through the following formula:

$$\Delta kWh = \frac{GPM_{base} \times 8.3 \times (T_{out} - T_{in})}{3412 \times RE} \times \frac{BehavioralWasteSeconds \times (N_{persons} \times N_{showers-day}) \times 365}{60 \times N_{showerheads-h}} \times ISR \times ELEC$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDF_w$$

**DEFINITION OF TERMS**

$$\Delta kWh = ISR \times ELEC \times \frac{GPM_{base} \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times (T_{out} - T_{in})}{3412 \frac{BTU}{kW} \times RE} \times \frac{BehavioralWasteSeconds \times (N_{persons} \times N_{showers-day}) \times 365 \frac{days}{yr}}{60 \frac{sec}{min} \times N_{showerheads-home}}$$

$$\Delta kW_{peak} = \Delta kWh \times ETDF$$

The ratio of the average energy usage during 2-PM and 6-PM on summer weekdays to the total annual energy usage is taken from average daily load shape data collected for showerheads from an Aquacraft, Inc study.<sup>Source 2</sup> The average daily load shapes (percentages of daily energy usage

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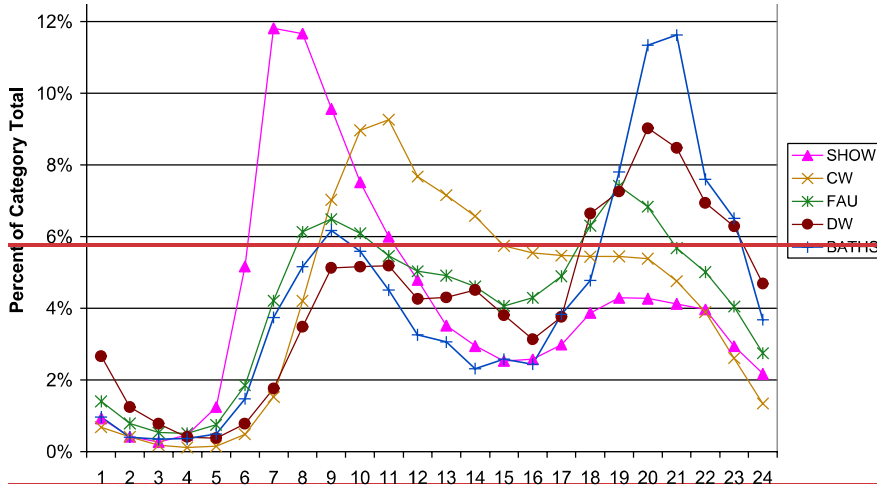
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that occur within each hour) during are plotted in Figure 2-3: Daily Load Shapes for Hot Water Measures below (symbol SHOW represents showerheads).<sup>45</sup>

A default in-service rate (ISR) of 100% is permissible for direct-install programs, but EDC data-gathering is required for kit delivery.

Figure 2-3: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup>



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### DEFINITION OF TERMS

Default savings assume an electric resistance storage water heater with RE = 0.98.

Table 2-74: Terms, Values, and References for Thermostatic Shower Restriction Valve

Parameter	Unit	Value	Source
$GPM_{Base}$ , Gallons per minute of baseline showerhead	$\frac{\text{gallons}}{\text{min}}$	EDC Data Gathering or Default: Standard shower head= 2.5 Low-Flow Shower Head=1.50	35
$T_{out}$ , Assumed temperature of water used by showerhead	$^{\circ}F$	EDC Data Gathering or Default: 104	6
$T_{in}$ , Assumed temperature of water entering house	$^{\circ}F$	53	7
RE, Recovery efficiency of electric water heater	Proportion	Default: Electric resistance: 0.98 HPWH: 3.93 Unknown: 1.22	8
BehavioralWasteSeconds.Time	sec	EDC Data Gathering or Default = 59	6

<sup>45</sup> SHOW = showers, CW = clothes washers, FAU = Faucets, DW = dishwashers, BATHS = baths. SHOW is the relevant curve for this measure.

Parameter	Unit	Value	Source
$N_{persons}$ , Average number of persons per household	$\frac{persons}{household}$	EDC Data Gathering or Default: SF=2.56 MF=1.7 Unknown=2.54	43
$N_{showers-Day}$ , Average number of showers per person per day	$\frac{showers}{person \cdot day}$	0.6	54
$N_{showerheads-home}$ , Average number of showerhead fixtures in the home	<del>None</del> units	EDC Data Gathering or Default: SF=1.69 MF=1.12 Unknown = 1.57	65
<del><math>T_{out}</math>, Assumed temperature of water used by showerhead</del>	<del><math>^{\circ}F</math></del>	<del>EDC Data Gathering or Default: 104</del>	<del>7</del>
<del><math>T_{in}</math>, Assumed temperature of water entering house</del>	<del><math>^{\circ}F</math></del>	<del>52</del>	<del>8</del>
<del><math>RE</math>, Recovery efficiency of electric water heater</del>	<del>Proportion</del>	<del>Default: 0.98 HPWH: 2.1</del>	<del>9, 11</del>
<del><math>ETDF</math>, Energy To Demand Factor</del>	<del><math>\frac{kW}{kWh/yr}</math></del>	<del>0.00008014</del>	<del>10</del>
<del><math>ISR</math>, In-Service Rate</del>	<del>%</del>	<del>EDC Data Gathering Default, direct install: 100%</del>	<del>EDC Data Gathering</del>
<del><math>ELEC</math>, Percentage of homes with electric water heat</del>	<del>%</del>	<del>EDC Data Gathering or Default: Electric = 100% Fossil Fuel = 0.0% Unknown=3547%</del>	<del>65</del>
<del><math>BehavioralWasteSeconds</math>, Time <math>ETDF_s</math>, Summer Energy to Demand Factor</del>	<del><math>\frac{sec \cdot kW}{kWh}</math></del>	<del>EDC Data Gathering or Default = 59SF: 0.0001057 MF: 0.0001006 Unknown: 0.0001046</del>	<del>79</del>
<del><math>ETDF_w</math>, Winter Energy to Demand Factor</del>	<del><math>\frac{kW}{kWh}</math></del>	<del>SF: 0.0001761 MF: 0.0001733 Unknown: 0.0001755</del>	<del>9</del>

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### DEFAULT SAVINGS

Default savings values should only be used for direct install delivery. For other delivery methods, EDCs must estimate and apply an ISR appropriate to the delivery method.

Table 2-75: Default Savings for Thermostatic Restriction Valve

Application/Housing Type	Baseline Flowrate (GPM)	Water Heater Fuel (% electric)	Energy Savings (kWh/yr) Water Heater Type	Peak Demand Reduction (kW) ΔkWh	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
Single Family	2-5	100%	Unknown (35%) Electric Resistance	74.6	38.0	0.0079
	2		Unknown (35%)	30.4	0.0024	
	4.5		Unknown (35%)	22.8	0.0048	

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Multifamily	2.5100%	Unknown (35%)HPWH	3718.6	0.00300020	0.8033	
	2100%	Unknown (35%)	30.159.9	0.00240063	0.0106	
	1.5	Unknown (35%)	22.6	0.0018		
Unknown / Default Housing Type	2.547%	Unknown (35%)	40.528.2	0.00320030	0.0050	
	2	Unknown (35%)	32.4	0.0026		
	1.5	Unknown (35%)	24.3	0.0019		
Single-Family	2.5	Electric (100%)	108.6	0.0087		
	2	Electric (100%)	86.9	0.0070		
	1.5	Electric (100%)	65.1	0.0052		
Multifamily	2.5100%	Electric (100%)Resistance	407.477.2	0.00860078	0.8134	
	2	Electric (100%)	85.9HPWH	19.3	0.00690019	0.0033
	1.5	Electric (100%)	64.4Unknown	62.0	0.00520062	0.0108
	47%	Unknown	29.2	0.0029	0.0051	
Unknown / Default Housing Type	2.547%	Electric (100%)Unknown	115.829.1	0.00930030	0.0051	
	2	Electric (100%)	92.7	0.0074		
	1.5	Electric (100%)	69.5	0.0056		

### EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with EDC Data Gathering.

### SOURCES

- 1) Uniform Plumbing Code (UPC) certification under the International Association of Plumbing and Mechanical Officials standard IGC 244-2007a stipulates device must meet 10,000 cycles without failure. Measure life:  $[10,000 \text{ cycles} / (N_{\text{persons}} \times N_{\text{showers-day}} \times 365)] = [10,000 / (2.5 \times 0.6 \times 365)] = 18 \text{ years}$ . Note that measure life is calculated to be 18 years; however, PA Act 129 savings can be claimed for no more than 15 years.
- 2) ~~Aquacraft, Inc., Water Engineering and Management. The end use of hot water in single family homes from flow trace analysis. 2001. <http://s3.amazonaws.com/zanran-storage/www.aquacraft.com/ContentPages/47768067.pdf>.~~
- 3) ~~Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. Uses the federal minimum GPM allowed as the baseline for the replaced showerheads, corresponding to 2.5 GPM.~~
- 3) U.S. Census Bureau, 2017-2021 American Community Survey 5-Year (2013-2017) Estimates. [Weblink](#)

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- 4) Table 8. Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. For each shower fixture metered, the evaluation team knew the total number of showers taken, duration of time meters remained in each home, and total occupants reported to live in the home. From these values average showers taken per day, per person was calculated. The study compared showers per day, per person by single-family and multifamily populations, finding no statistical difference in the values. For the energy-saving analysis, the study used the combined single-family and multifamily average showers per day, per person of 0.6.
- 4) – for 2017. <http://factfinder.census.gov>.
- 5) ~~1) Table 8. Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. For each shower fixture metered, the evaluation team knew the total number of showers taken, duration of time meters remained in each home, and total occupants reported to live in the home. From these values average showers taken per day, per person was calculated. The study compared showers per day, per person by single-family and multifamily populations, finding no statistical difference in the values. For the energy-saving analysis, the study used the combined single-family and multifamily average showers per day, per person of 0.6.~~
- 6) 5) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Pg 122, table 105 (ELEC). Pg 130 table, 115 (GPM<sub>base</sub>, N<sub>showerheads-home</sub>). Weblink
- 7) 6) PPL Electric 2014 ShowerStart Pilot Study. Cadmus memo to PPL Electric in November 2014. The previous T<sub>out</sub> value was based on the average water temperature of the entire shower, whereas this pilot study T<sub>out</sub> value is based on the average water temperature of the period after the user resumed the water flow by pulling the ShowerStart cord. This pilot study T<sub>out</sub> value is more accurate than the previous value because it excludes the warmup phase of the shower and thus reflects the temperature of the water saved by the ShowerStart device during the behavioral waste period more accurately. The BehavioralWasteSeconds value represents the average time the ShowerStart device is engaged during a shower. The BehavioralWasteSeconds value includes instances when the user did not engage the ShowerStart device (instances when BehavioralWasteSeconds = 0s).
- 8) 7) Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40-inch depth is ~~51.86~~ 52.502. Calculated using Daily SCAN Standard - Period of Record data from ~~April 1999~~ December 2003 to December ~~2018~~ 2023 from the Natural Resource Conservation Service Database. [https://wcc.sc.egov.usda.gov/nwcc/rgprt?report=daily\\_scan\\_por&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgprt?report=daily_scan_por&state=PA) Weblink. Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures. p.(2017, March). "2.6.1 Water Heater". Pg 78. <https://energy.mo.gov/sites/energy/files/MOTRM2017Volume2.pdf> Weblink
- 9) – AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. <https://www.ahridirectory.org/Search/SearchForm?programId=24&searchTypeId=2>
- 10) – Aquacraft, Inc., Water Engineering and Management. The end use of hotAverage recovery efficiency for heat pump water in single-family homes from flow trace analysis. 2001. [http://s3.amazonaws.com/zanran\\_storage/www.aquacraft.com/ContentPages/47768067.pdf](http://s3.amazonaws.com/zanran_storage/www.aquacraft.com/ContentPages/47768067.pdf). The statewide values were used for inputs in the ETDF algorithm components. The CF for showerheads/heaters is found to be 0.00380: [% showerhead use during peak × (T<sub>Person-Day</sub> × N<sub>Persons</sub> × N<sub>showers-day</sub>) / (N<sub>showerheads-home</sub>) / 240 (minutes in peak period) = [11.7% × (7.8 × 2.5 × 0.6 / 3.93. Accessed December 2023. Weblink 1.5)] / 240 = 0.00380. The Hours for showerheads is found to be 47.5: (T<sub>Person-Day</sub> × N<sub>Persons</sub> × 365) / (N<sub>showerheads-home</sub>) / 60 = (7.8 × 2.5 × 0.6 × 365) / 1.5 / 60 = 47.5. The resulting ETDF is 22 for unknown type calculated to be 0.00008014: CF / Hours = 0.00380 / 47.5 = 0.00008014.

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- 8) NEEA Heat Pump Water Heater Field Study Report. Prepared as the weighted average of electric resistance and HPWH recover efficiencies by Fluid Market Strategies. October 22, 2013. <https://neea.org/img/uploads/heat-pump-water-heater-field-study-report.pdf> the relative proportions of electric resistance and HPWHs from the 2023 PA residential baseline study.
- 9) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

**2-3.102.3.9 DRAIN WATER HEAT RECOVERY UNITS**

Target Sector	Residential <del>Establishments</del>
Measure Unit	Drain Water Heat Recovery Unit
Measure Life	15 years <sup>Source 121</sup>
Vintage	Retrofit, New Construction

This measure relates to the installation of a vertical drain water heat recovery unit in homes with electric water heaters. Drain water heat recovery units capture waste heat from ~~shower grey~~ drain water and use it to preheat cold water that is delivered to the ~~shower fixture's~~ mixing valve, the water heater, or both. Savings are calculated per drain water heat recovery unit. ~~A term is included to accommodate multifamily buildings with multiple units' drains connected to a single drain water heat recovery unit.~~

**ELIGIBILITY**

**ELIGIBILITY**

This protocol documents the energy savings attributable to installing a vertical drain water heat recovery unit to a ~~shower~~ drain pipe. The target sector primarily consists of residences.

**ALGORITHMS**

**ALGORITHMS**

The ~~algorithms for annual energy savings and peak demand savings are obtained through the following formulas shown below:~~

$$\Delta kWh = \frac{(T_{out} - T_{in}) \times 8.3 \frac{BTU}{gal \cdot ^\circ F} \times GPM \times T_{person \cdot day} \times N_{persons} \times N_{showers \cdot day} \times N_{units} \times 365 \frac{days}{yr} \times SF}{3412 \frac{BTU}{kW} \times RE}$$

$$\Delta kWh = \frac{(T_{out} - T_{in}) \times 8.3 \times GPHD \times 365 \times SF}{3412 \times RE}$$

$$\Delta kW_{peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter \ peak} = \Delta kWh \times ETDF_w$$

**DEFINITION OF TERMS**

Where:

$$ETDF = \frac{CF}{HOU}$$

Given:

$$CF = \frac{\%_{shower \ use \ peak} \times T_{person \cdot day} \times N_{persons} \times N_{showers \cdot day}}{240 \frac{minutes}{daily \ peak}}$$

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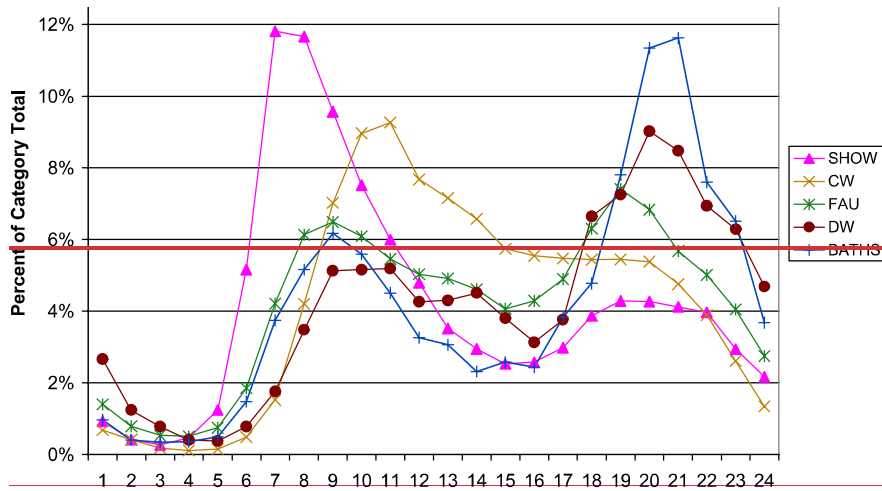
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$$HOU = \frac{T_{person-day} \times N_{persons} \times N_{showers-day} \times 365 \frac{days}{yr}}{60 \frac{minutes}{hour}}$$

The ratio of the average energy usage during 2 PM and 6 PM on summer weekdays to the total annual energy usage is taken from average daily load shape data collected for showerheads from an Aquacraft, Inc study.<sup>Source 8</sup> The average daily load shapes (percentages of daily energy usage that occur within each hour) during are plotted in Figure 2-2 below (symbol SHOW represents showerheads).<sup>46</sup>

Figure 2-4: Daily Load Shapes for Hot Water Measures<sup>Source 2</sup>



**DEFINITION OF TERMS**

Table 2-76: Terms, Values, and References for Drain Water Heat Recovery Units

Term	Unit	Value	Source
$T_{out}$ , Assumed temperature of water used by showerhead	° F	101	52
$T_{in}$ , Assumed temperature of water entering house	° F	52.53	63
GPM, Gallons per minute of showerhead	$\frac{gallons}{minute}$	Default standard = 2.5 Low flow = EDC Data Gathering <sup>47</sup>	4
$T_{person-day}$ , Average time of shower usage per person (minutes)	$\frac{minutes}{day}$	7.8	2

<sup>46</sup> SHOW = showers, CW = clothes washers, FAU = Faucets, DW = dishwashers, BATHS = baths. SHOW is the relevant curve for this measure.

<sup>47</sup> The low-flow showerhead GPM should be used where both a low-flow showerhead and a drain water heat recovery unit are installed in the same home.

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Term	Unit	Value	Source
$N_{persons}$ , Average number of persons per household	$\frac{persons}{house}$	EDC Data-Gathering or Default SF=2.5 Default MF=1.7 Default unknown=2.5	3
$N_{showers=day}$ , Average number GPHD. Gallons of showershot water use per personhousehold per day	$\frac{showers}{person \rightarrow day} \frac{gallon}{day}$	0.6 Shower only: 17.8 Whole house: 45.5	4
$N_{units}$ , Number of units in a multifamily building with drains connected to the drain water heat recovery unit.	Units	SF: 1 MF: 1 or EDC Data Gathering	-
$SF$ , Water heating energy savings factor	%	30%	40, 115
$RE$ , Recovery efficiency of electric water heater	Proportion	Default: Resistance: 0.98 HPWH: 2.3.93 Unknown: 1.22	7, 96
$ETDF$ – $ETDF_s$ , Summer Energy to Demand Factor	$\frac{kWh}{kW} / \frac{kWh}{kW}$	SF: 0.000080+30001057 MF: 0.0001006 Unknown: 0.0001046	87
$\%_{shower-use=peak}$ , percentage of daily shower use during PJM-peak period $ETDF_w$ , Winter Energy to Demand Factor	$\% \frac{kW}{kWh}$	11.7% SF: 0.0001761 MF: 0.0001733 Unknown: 0.0001755	87

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**DEFAULT SAVINGS**

**DEFAULT SAVINGS**

Table 2-77: Default Savings for Drain Water Heat Recovery Unit

Housing Type	Flow Rate (gpm)	Energy Savings per Unit (kWh)		Demand Savings per Unit (kW)	
		Electric Resistance	HPWH	Electric Resistance	HPWH
Single Family/ Unknown	2.5	365.7	170.7	0.0293	0.0137
	2.0	292.6	136.5	0.0234	0.0109
	1.75	256.0	119.5	0.0205	0.0096
	1.5	219.4	102.4	0.0176	0.0082
Multifamily	2.5	248.7	116.1	0.0199	0.0093
	2.0	198.9	92.8	0.0159	0.0074
	1.75	174.1	81.2	0.0139	0.0065
	1.5	149.2	69.6	0.0120	0.0056

Housing Type	Water Heater Type	Shower Only			Whole House		
		Energy Savings (kWh)	Peak Demand Savings (kW)		Energy Savings (kWh)	Peak Demand Savings (kW)	
			Summer	Winter		Summer	Winter
Single Family	Resistance	232.2	0.0245	0.0409	593.6	0.0627	0.1045
	HPWH	57.9	0.0061	0.0102	148.0	0.0156	0.0261
	Unknown Electric	186.5	0.0197	0.0329	476.8	0.0504	0.0840
Multifamily	Resistance	232.2	0.0234	0.0402	593.6	0.0597	0.1029
	HPWH	57.9	0.0058	0.0100	148.0	0.0149	0.0257
	Unknown Electric	186.5	0.0188	0.0323	476.8	0.0480	0.0826
Unknown	Resistance	232.2	0.0243	0.0408	593.6	0.0621	0.1042
	HPWH	57.9	0.0061	0.0102	148.0	0.0155	0.0260
	Unknown Electric	186.5	0.0195	0.0327	476.8	0.0499	0.0837

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### EVALUATION PROTOCOLS

The most appropriate evaluation protocol for this measure is verification of installation coupled with EDC Data Gathering.

### SOURCES

- 1) Sachs, H., Talbot J., Kaufman N. (2012, February) "Emerging Hot Water Technologies and Practices for Energy Efficiency as of 2011". Pg 69. ACEEE. Weblink. Note that measure life is defined as 30 years; however, PA Act 129 Legislation caps measure life at 15 years.
- 1) Cadmus and Opinion Dynamics for Michigan Evaluation Team Working Group. (2013, June). Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. Uses the federal minimum GPM allowed as the baseline for the replaced showerheads, corresponding to 2.5 GPM.
- 2) Table 6. Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. The study compared shower length by single-family and multifamily populations, finding no statistical difference in showering times. For the energy-saving analysis, the study used the combined single-family and multifamily average shower length of 7.8 minutes.
- 3) American Community Survey 5-Year (2013-2017) Estimates for 2017. <http://factfinder.census.gov>.
- 4) Table 8. Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. For each shower fixture metered, the evaluation team knew the total number of showers taken, duration of time meters remained in each home, and total occupants reported to live in the home. From these values average showers taken per day, per person was calculated. The study compared

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showers per day, per person by single-family and multifamily populations, finding no statistical difference in the values. For the energy-saving analysis, the study used the combined single-family and multifamily average showers per day, per person of 0.6.

- 5) 2) Cadmus and Opinion Dynamics Evaluation Team. Showerhead and Faucet Aerator Meter Study. For Michigan Evaluation Working Group. June 2013. Memorandum. Temperature sensors provided the mixed water temperature readings resulting in an average of 101°F.
- 6) 3) Using Rock Spring, PA (Site 2036) as a proxy, the mean of soil temperature at 40-inch depth is 54.86452.502. Calculated using Daily SCAN Standard - Period of Record data from April 1999 to December 20182003 to December 2023 from the Natural Resource Conservation Service Database.  
[https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily\\_scan\\_por&state=PA](https://wcc.sc.egov.usda.gov/nwcc/rgrpt?report=daily_scan_por&state=PA) Weblink.  
Methodology follows Missouri TRM 2017 Volume 2: Commercial and Industrial Measures, p. 78. <https://energy.mo.gov/sites/energy/files/MOTRM2017Volume2.pdf>.
- 4) DeOreo, W., Mayer, P., Dziegielewski, B., Kiever, J. for Water Research Foundation. (2016, April). "Residential End Uses of Water, Version 2 Executive Report." Page 5, Table 1. Weblink
- 7) AHRI Directory. All electric storage water heaters have a recovery efficiency of .98. <https://www.ahridirectory.org/Search/SearchForm?programId=24&searchTypeId=2>
- 8) Aquacraft, Inc., Water Engineering and Management. The end use of hot water in single family homes from flow trace analysis. 2001.  
[http://s3.amazonaws.com/zanran\\_storage/www.aquacraft.com/ContentPages/47768067.pdf](http://s3.amazonaws.com/zanran_storage/www.aquacraft.com/ContentPages/47768067.pdf).  
The statewide values were used for inputs in the ETDF algorithm components. The CF for showerheads is found to be 0.00380:  $[\% \text{ showerhead use during peak} \times (T_{\text{Person-Day}} \times N_{\text{Person}} \times N_{\text{showers-day}}) / (N_{\text{showerheads-home}})] / 240$  (minutes in peak period) =  $[11.7\% \times (7.8 \times 2.5 \times 0.6 / 1.5)] / 240 = 0.00380$ . The Hours for showerheads is found to be 47.5:  $(T_{\text{Person-Day}} \times N_{\text{Persons}} \times 365) / (N_{\text{showerheads-home}}) / 60 = (7.8 \times 2.5 \times 0.6 \times 365) / 1.5 / 60 = 47.5$ . The resulting ETDF is calculated to be 0.00008014:  $CF / \text{Hours} = 0.00380 / 47.5 = 0.00008014$ .
- 9) NEEA Heat Pump Water Heater Field Study Report. Prepared by Fluid Market Strategies. October 22, 2013. <https://neea.org/img/uploads/heat-pump-water-heater-field-study-report.pdf>
- 4) 5) Heat Recovery from Wastewater Using a Gravity-Film Heat Exchanger, Department of Energy Federal Energy Management Program. U.S. DOE Federal Energy Management Program report DOE/EE-0247 Revised. July, 2005. Lower end of 30 – 50% range estimated for different devices and installation configurations (equal, unequal to water heater, and unequal to shower).  
[https://www.fpl.fs.fed.us/documnts/informationalkits/infokit\\_0003\\_DrainwaterFact%20Sheet.pdf](https://www.fpl.fs.fed.us/documnts/informationalkits/infokit_0003_DrainwaterFact%20Sheet.pdf) Weblink
- 6) AHRI Directory. All electric storage water heaters have a recovery efficiency of 0.98. Average recovery efficiency for heat pump water heaters is 3.93. Accessed December 2023. Weblink 1.22 for unknown type calculated as the weighted average of electric resistance and HPWH recover efficiencies by the relative proportions of electric resistance and HPWHs from the 2023 PA residential baseline study.
- 7) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

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### 2.3.10 SMART WATER HEATER CONTROLS

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Water Heater Controller
<b>Measure Life</b>	11 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout, New Construction

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Smart water heater controls prevent the unnecessary heating of water. They use analytics to learn household water use patterns and heat water only at times of anticipated need. Smart controllers also have a user interface to allow manual control settings (i.e., scheduling) and help customers understand and act on water heating energy usage. The controllers reduce unnecessary reheat during periods of low demand while the water heater idles and the temperature drifts within an acceptable range.

Smart Water Heater Controls add a web-enabled control box that functions as a junction box to an electric tank's power source, so it turns on/off the power to the tank per the control algorithm or customer commands. Smart Water Heater Controls will have functions that are located in the home and on the Internet (the cloud). Homes with Wi-Fi can enable full operating capabilities or utilize a cellular option. While compatible with the device, gas water heaters are not eligible for savings for this measure.

#### ELIGIBILITY

This measure documents the energy savings resulting from Smart Water Heater Control with professional installation with electric resistance or heat pump storage water heaters. The primary target sector is single-family residences.

#### ALGORITHMS

The annual energy savings calculation utilizes average performance data for available residential water heaters and typical water usage for residential homes. The energy savings are obtained through the following formula, where the term in the parentheses corresponds to tank loss savings.

$$\Delta kWh = \frac{\Delta T}{3412} \times \left( \frac{A_{tank} \times 8760}{R_{tank} \times \eta_{elec}} + \frac{Cycles_{wash} \times V_{HW} \times 8.3}{UEF_{WH}} \right)$$

Clothes washers will draw the same amount of water for a load regardless of temperature, where, for example, with a shower, the user will just adjust the valve to get their desired temperature if the incoming hot water is cooler. Therefore, there are extra savings for clothes washers, but not other uses.

Demand savings result from reduced hours of operation of the heating element, rather than a reduced connected load.

$$\Delta kW_{summer\ peak} = E_{TDFs} \times \Delta kWh$$

$$\Delta kW_{winter\ peak} = E_{TDFw} \times \Delta kWh$$

Alternatively, if an EDC configures the smart water heater to reduce demand savings by avoiding reheat during the peak demand period, peak demand savings will be calculated using the telemetry data from the devices via a SWE-approved estimation method.

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**DEFINITION OF TERMS**

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**Table 2-78: Terms, Values, and References for Smart Water Heater Controls**

Term	Unit	Values	Source
$\Delta T$ , change in the average hot water weekly temperature draw using the smart water heater control compared to the baseline water heater	$^{\circ}F$	5.4	8
$R_{tank}$ , R value of water heater tank	$\frac{hr \cdot ^{\circ}F \cdot ft^2}{BTU}$	EDC Data Gathering Default: 12	3
$A_{tank}$ , Surface Area of water heater tank	$ft^2$	EDC Data Gathering Default: 24.99	50 gal. value in Table 2-66
$\eta_{elec}$ , Thermal efficiency of electric heater element	Proportion	Electric Storage: 0.98 HPWH: 3.11	4; 5
$V_{HW}$ , Volume of hot water used per cycle by clothes washer	$\frac{gallons}{cycle}$	20	6
$Cycles_{wash}$ , Number of clothes washer cycles per year	$\frac{cycles}{yr}$	Clothes washer present: 178 No clothes washer: 0	7
$UEF_{WH}$ , Uniform Energy Factor of water heater	Proportion	EDC data collection Default: Electric Storage= 0.92 HPWH= 3.20	2
$ETDFs$ , Energy To Demand Factor (summer, defined above)	$\frac{kW}{kWh}$	0.0001046	9
$ETDFw$ , Energy To Demand Factor (winter, defined above)	$\frac{kW}{kWh}$	0.0001755	9

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**DEFAULT SAVINGS**

The energy savings and demand reductions are prescriptive according to the above formula.

**Table 2-79: Default Energy Savings and Demand Reductions**

Type	$\Delta kWh$	$\Delta kW_{summer\ peak}$	$\Delta kW_{winter\ peak}$
Electric Storage	29.46	0.00308	0.00517
Electric Storage w/ Clothes Washer	47.65	0.00498	0.00836
HPWH	9.28	0.00097	0.00163
HPWH w/ Clothes Washer	23.90	0.00250	0.00419

**SOURCES**

- California Electronic Technical Reference Manual. "Storage Water Heater, Residential". Accessed March 2024. Weblink



- 2) [NMR Group for the Pennsylvania Public Utility Commission. \(2024, March\). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 8.3.5, Table 110, pg 128. Weblink](#)
  - 3) [Conservative estimate of R-12](#)
  - 11) ~~Zaloum et al., Drain Water Heat Recovery Characterization and Modeling, Sustainable Buildings and Communities, Natural Resources Canada, Ottawa, June 29, 2007. [http://gfxtechnology.com/NRCAN-6\\_29\\_07.pdf](http://gfxtechnology.com/NRCAN-6_29_07.pdf)~~
  - 12) ~~1) Sachs, Talbot, Kaufman, "Emerging Hot Water Technologies and Practices for Energy Efficiency as of 2011," ACEEE, February 2012. Note that measure life is defined as 30 years; however, PA Act 129 Legislation caps measure life at 15 years.~~
- [AHRI Directory. All electric storage water heaters have a recovery efficiency of .98.](#)
- 4) [Weblink](#)
  - 5) [If HPWH UEF is known but COP of HPWH compressor is unknown, assume compressor efficiency is UEF/0.9. This yields a default COP of 3.11. Maryland EmPOWER Technical Reference Manual. \(2023, version 11.0\). "Water Heater Temperature Setback". Weblink](#)
  - 6) [ENERGY STAR. Clothes Washers. Accessed March 2024. Weblink](#)
  - 7) [U.S. Energy Information Administration. \(2023\). 2020 Residential Energy Consumption Survey. Weblink. Calculated using "Frequency of clothes washer use" and "Frequency of dryer use" data for Pennsylvania.](#)
  - 8) [Gunn, K., Kalensky, D., Schoenbauer, B., Haynor, A. \(2018, April\). "Field Study of an Intelligent, Networked, Retrofittable Water Heater Controller". Pg. 44. Gas Technology Institute for Minnesota Department of Commerce, Division of Energy Resources. Weblink](#)
  - 9) [Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink](#)

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## 2.4 APPLIANCES

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If a customer submits a rebate for a product that has applied for ENERGY STAR certification but has not yet been certified, the savings will be counted for that product contingent upon its eventual certification as an ENERGY STAR measure. If at any point the product is rejected by ENERGY STAR, the product is then ineligible for the program and savings will not be counted.<sup>48</sup>

### 2.4.1 ENERGY STAR REFRIGERATORS

Target Sector	Residential Establishments
Target Sector	Residential
Measure Unit	Refrigerator
Measure Life	14 years <sup>Source 1</sup>
Vintage	Replace on Burnout

#### ELIGIBILITY

This measure is for the purchase and installation of a new refrigerator meeting ENERGY STAR or ENERGY STAR Most Efficient criteria. An ENERGY STAR refrigerator is about 10-percent% more efficient than the minimum federal government standard. The ENERGY STAR Most Efficient is a new certification that identifies the most efficient products among those that qualify for ENERGY STAR. ENERGY STAR Most Efficient refrigerators must be at least 15-percent% more efficient than the minimum federal standard.

#### ALGORITHMS

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of refrigerators. ~~The number of refrigerators will be determined using market assessments and market tracking.~~

If the volume and configuration of the refrigerator is known, the baseline model's annual energy consumption ( $kWh_{base}$ ) may be determined using [Table 2-68](#).

~~Table 2-81. The efficient model's annual energy consumption ( $kWh_{ee}$  or  $kWh_{me}$ ) may be determined using manufacturers' test data for the given model. Where test data is not available the algorithms in Table 2-68 and Table 2-70 for "ENERGY STAR and ENERGY STAR Most Efficient maximum energy usage in kWh/year" may be used to determine the efficient model's annual energy consumption for a conservative savings estimate may be determined using Table 2-81.~~

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#### ENERGY STAR Refrigerator

$$\Delta kWh = kWh_{base} - kWh_{ee}$$

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~~$$\Delta kWh_{peak} \Delta kWh_{summer peak} = (kWh_{base} - kWh_{ee}) \times ETD F ETD F_s$$~~

~~$$\Delta kWh_{winter peak} = (kWh_{base} - kWh_{ee}) \times ETD F_w$$~~

#### ENERGY STAR Most Efficient Refrigerator

<sup>48</sup> The Pennsylvania SWE and PUC TUS staff added this condition relating to certification that has been applied for but not yet received at the request of several of the Pennsylvania EDCs. EDCs will be responsible for tracking whether certification is granted.

$$\Delta kWh = kWh_{base} - kWh_{me}$$

$$\Delta kW_{peak} \Delta kW_{summer\ peak} = (kWh_{base} - kWh_{me}) \times ETDF - ETDF_s$$

$$\Delta kW_{winter\ peak} = (kWh_{base} - kWh_{me}) \times ETDF_w$$

**DEFINITION OF TERMS**

**Table 2-69: Terms, Values, and References for ENERGY STAR Refrigerators**

Term	Unit	Value	Source
<i>kWh<sub>base</sub></i> , Annual energy consumption of baseline unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-68	2
<i>kWh<sub>ee</sub></i> , Annual energy consumption of ENERGY STAR qualified unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-68	3
<i>kWh<sub>me</sub></i> , Annual energy consumption of ENERGY STAR Most Efficient qualified unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-69	4
<i>ETDF</i> , Energy to Demand Factor	$\frac{kW}{kWh/yr}$	0.0001614	5

**80: Terms, Values, and References for ENERGY STAR Refrigerators**

Term	Unit	Value	Source
<i>kWh<sub>base</sub></i> , Annual energy consumption of baseline unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-81	EDC Data Gathering, 2, 7
<i>kWh<sub>ee</sub></i> , Annual energy consumption of ENERGY STAR qualified unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-83	EDC Data Gathering, 3
<i>kWh<sub>me</sub></i> , Annual energy consumption of ENERGY STAR Most Efficient qualified unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-83	EDC Data Gathering, 4
<i>ETDF<sub>s</sub></i> , Summer peak Energy to Demand Factor	$\frac{kW}{kWh}$	0.0001354	5
<i>ETDF<sub>w</sub></i> , Winter peak Energy to Demand Factor	$\frac{kW}{kWh}$	0.0001014	5

Refrigerator energy use is characterized by configuration (top freezer, bottom freezer, etc.), volume, whether defrost is manual or automatic, and whether there is an automatic icemaker, and whether there is through-the-door ice. If this information is known, annual energy consumption (*kWh<sub>base</sub>*) of the federal standard model may be determined using Table 2-68. The efficient model's annual energy consumption (*kWh<sub>ee</sub>* or *kWh<sub>me</sub>*) may be determined using manufacturer's test data for the given model. Where test data is not available, the algorithms in Table 2-68 and Table 2-69 Table 2-82 for "ENERGY STAR and ENERGY STAR Most Efficient maximum energy usage in kWh/year" may be used to determine efficient energy consumption for a conservative savings estimate.

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The term “AV” in the equations refers to “Adjusted Volume” in ft<sup>3</sup>. For Category 1 and 1A “All-refrigerators”:

$$AV = \text{Fresh Volume} + \text{Freezer Volume}$$

For all other categories:

$$AV = \text{Fresh Volume} + 1.76 \times \text{Freezer Volume}$$

I = 1 for a product with an automatic icemaker and 0 for a product without an automatic icemaker. See Table 2-82 for door coefficients.

**Table 2-81: Federal Standard and ENERGY STAR Refrigerators Maximum Annual Energy Consumption if Configuration and Volume Known<sup>49</sup>**

Refrigerator Category	Federal Standard Maximum Usage in kWh/yr <sup>9/15/14 - 1/30/29</sup>	ENERGY STAR Maximum Energy Usage in kWh/yr <sup>1/31/29 - 1/30/30</sup>	As of 1/31/30
<b>Standard Size Models: 7.75 cubic feet or greater</b>			
1. Refrigerator-freezers and refrigerators other than all-refrigerators with manual defrost.	7.99 × AV + 225.0		7.19 × 6.79 × AV + 202.5191.3
1A. All-refrigerators— manual defrost.	6.79 × AV + 193.6		6.11 × AV + 174.25.77AV + 164.6
2. Refrigerator-freezers— partial automatic defrost	7.99 × AV + 225.0		7.19 × (6.79 × AV + 202.5191.3) × K2
3. Refrigerator-freezers— automatic defrost with top-mounted freezer without an automatic icemaker.	8.07 × AV + 233.7		7.26 × 6.86 × AV + 240.3198.6 + 281
3-BI. Built-in refrigerator-freezer— automatic defrost with top-mounted freezer without an	9.15 × AV + 264.9		8.24 × AV + 238.4 + 281

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<sup>49</sup> Lettering convention (1, 1A, etc.) of Federal standard and ENERGY STAR specifications included for clear reference to the standards as well as for correspondence to entries in the default savings table.

Refrigerator Category	Federal Standard Maximum Usage in kWh/yr 5/14 - 1/30/29	ENERGY STAR Maximum Energy Usage in kWh/yr 1/31/29 - 1/30/30	As of 1/31/30
automatic icemaker.			
3I. Refrigerator-freezers— automatic defrost with top-mounted freezer with an automatic icemaker without through-the-door ice service.	$8.07 \times AV + 317.7$	$7.26 \times AV + 294.3$	
3I-BI. Built-in refrigerator-freezers— automatic defrost with top-mounted freezer with an automatic icemaker without through-the-door ice service.	$9.15 \times AV + 348.9$	$8.24 \times AV + 322.4$	
3A. All-refrigerators— automatic defrost.	$7.07 \times AV + 201.6$		$(6.36 \times 01 \times AV + 184.171,4) \times K3A$
3A-BI. Built-in All-refrigerators— automatic defrost.	$8.02 \times AV + 228.5$		$(7.22 \times AV + 205.7) \times K3ABI$
4. Refrigerator-freezers— automatic defrost with side-mounted freezer without an automatic icemaker.	$8.51 \times AV + 297.8$		$(7.66 \times 28 \times AV + 268.0254.9) \times K4 + 28I$
4-BI. Built-In Refrigerator-freezers— automatic defrost with side-mounted freezer without	$10.22 \times AV + 357.4$		$9.20 \times (8.79 \times AV + 321.7307.4) \times K4BI + 28I$

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Refrigerator Category	Federal Standard Maximum Usage in kWh/yr 5/14 - 1/30/29	ENERGY STAR Maximum Energy Usage in kWh/yr 1/31/29 - 1/30/30	As of 1/31/30
an automatic icemaker.			
4I. Refrigerator-freezers— automatic defrost with side-mounted freezer with an automatic icemaker without through-the-door ice service.	$8.51 \times AV + 381.8$	<del><math>7.66 \times AV + 352.0</math></del>	
4I-BI. Built-In Refrigerator-freezers— automatic defrost with side-mounted freezer with an automatic icemaker without through-the-door ice service.	$10.22 \times AV + 441.4$	<del><math>9.20 \times AV + 405.7</math></del>	
5. Refrigerator-freezers— automatic defrost with bottom-mounted freezer without an automatic icemaker.	$8.85 \times AV + 317.0$		<del><math>(7.97 \times 61 \times AV + 285.3272.6) \times K5 + 281</math></del>
5-BI. Built-In Refrigerator-freezers— automatic defrost with bottom-mounted freezer without an automatic icemaker.	$9.40 \times AV + 336.9$		<del><math>(8.46 \times 65 \times AV + 303.2309.9) \times K5BI + 281</math></del>
5I. Refrigerator-freezers— automatic defrost with bottom-mounted freezer	$8.85 \times AV + 401.0$	<del><math>7.97 \times AV + 369.3</math></del>	

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Refrigerator Category	Federal Standard Maximum Usage in kWh/yr 5/14 - 1/30/29	ENERGY STAR Maximum Energy Usage in kWh/yr 1/31/29 - 1/30/30	As of 1/31/30
with an automatic icemaker without through-the-door ice service.			
5I-BI. Built-In Refrigerator-freezers— automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.	$9.40 \times AV + 420.9$	<del><math>8.46 \times AV + 387.2</math></del>	
5A. Refrigerator-freezer— automatic defrost with bottom-mounted freezer with through-the-door ice service.	$9.25 \times AV + 475.4$	<del><math>8.33 \times (7.76 \times AV + 436.3351.9) \times K5A</math></del>	
5A-BI. Built-in refrigerator-freezer— automatic defrost with bottom-mounted freezer with through-the-door ice service.	$9.83 \times AV + 499.9$	<del><math>(8.85 \times 21 \times AV + 458.3370.7) \times K5ABI</math></del>	
6. Refrigerator-freezers— automatic defrost with top-mounted freezer with through-the-door ice service.	$8.40 \times AV + 385.4$	<del><math>7.56 \times 14 \times AV + 355.3280.0</math></del>	
7. Refrigerator-freezers— automatic	$8.54 \times AV + 432.8$	<del><math>(7.69 \times 31 \times AV + 397.9322.5) \times K7</math></del>	

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Refrigerator Category	Federal Standard Maximum Usage in kWh/yr 5/14 - 1/30/29	ENERGY STAR Maximum Energy Usage in kWh/yr 1/31/29 - 1/30/30	As of 1/31/30
defrost with side-mounted freezer with through-the-door ice service.			
7-BI. Built-In Refrigerator-freezers— automatic defrost with side-mounted freezer with through-the-door ice service.	10.25 × AV + 502.6	9.23 × (8.82 × AV + 460.7384.1) × K7BI	
<b>Compact Size Models: Less than 7.75 cubic feet and 36 inches or less in height</b>			
11. Compact refrigerator-freezers and refrigerators other than all-refrigerators with manual defrost.	9.03 × AV + 252.3	8.437.68 × AV + 227.4214.5	
11A. Compact all-refrigerators— manual defrost.	7.84 × AV + 219.1	7.066.66 × AV + 197.186.2	
12. Compact refrigerator-freezers— partial automatic defrost	5.91 × AV + 335.8	(5.32 × AV + 302.2) × K12	
13. Compact refrigerator-freezers— automatic defrost with top-mounted freezer.	11.80 × AV + 339.2	10.62 × AV + 305.3 + 28I	
13I. Compact refrigerator-freezers— automatic defrost with top-mounted freezer with an	11.80 × AV + 423.2	10.62 × AV + 389.3	

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Refrigerator Category	Federal Standard Maximum Usage in kWh/yr 5/14 - 1/30/29	ENERGY STAR Maximum Energy Usage in kWh/yr 1/31/29 - 1/30/30	As of 1/31/30
automatic icemaker.			
13A. Compact all-refrigerators— automatic defrost.	$9.17 \times AV + 259.3$	$(8.25 \times AV + 233.4) \times K13A$	
14. Compact refrigerator-freezers— automatic defrost with side-mounted freezer.	$6.82 \times AV + 456.9$	$6.14 \times AV + 411.2 + 28I$	
14I. Compact refrigerator-freezers— automatic defrost with side-mounted freezer with an automatic icemaker.	$6.82 \times AV + 540.9$	$6.14 \times AV + 495.2$	
15. Compact refrigerator-freezers— automatic defrost with bottom-mounted freezer.	$11.80 \times AV + 339.2$	$10.62 \times AV + 305.3 + 28I$	
15I. Compact refrigerator-freezers— automatic defrost with bottom-mounted freezer with an automatic icemaker.	$11.80 \times AV + 423.2$	$10.62 \times AV + 389.3$	

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**Table 2-82: Default Savings Values: Door Coefficients for ENERGY STAR Refrigerators<sup>50</sup>Federal Standard Energy Consumption Algorithms**

Refrigerator Category Door Coefficient <sub>d</sub>	Assumed Adjusted Volume of Unit (cubic feet) <sup>50</sup> Products with a Transparent Door <sub>d</sub>	Conventional Unit Energy Usage in kWh/yr Products without a Transparent Door with a Door-in-Door <sub>d</sub>			ENERGY STAR Energy Usage in kWh/yr Products without a Transparent Door or Door-in-Door with Added External Doors <sub>d</sub>	$\Delta kWh/yr^{51}$	$\Delta kW_{peak}$
1A. All refrigerators— manual defrost. K <sub>2</sub>	151.0	2961.0	267	30	$0.00481 + 0.02 \times (N_d^{52} - 1)$		
2. Refrigerator-freezers— partial automatic defrost. K <sub>3A</sub>	151.1	3461.0	311	35	1.0-0056		
3A. All refrigerators— automatic defrost. K <sub>3AB</sub>	151.1	3081.0	278	31	1.0-0050		
3I. Refrigerator-freezers— automatic defrost with top-mounted freezer with an automatic icemaker without through-the-door ice service. K <sub>4</sub>	22.21.1	4971.06	455	41	$1 + 0.006702 \times (N_d - 2)$		
4I. Refrigerator-freezers— automatic defrost with side-mounted freezer with an automatic icemaker without through-the-door ice service. K <sub>4B</sub>	281.1	6241.06	567	54	$1 + 0.008702 \times (N_d - 2)$		
5A. Refrigerator-freezer— automatic defrost with bottom-mounted freezer with	31.51.1	7661.06	698	68	$1 + 0.014002 \times (N_d - 2)$		

<sup>50</sup> Lettering convention (1A, 2, etc.) of Federal standard and ENERGY STAR specifications included for clear reference to the standards as well as for correspondence to entries in the default savings table.

<sup>51</sup> kWh/yr savings may differ from Conventional Usage—ENERGY STAR Usage by 1 kWh/yr due to rounding error.

<sup>52</sup> N<sub>d</sub> is the number of external doors. The maximum N<sub>d</sub> values are 2 for K12 and K2, 3 for K9BI, and 5 for all other K values.

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through-the-door ice service.K5					
51. Refrigerator-freezers— automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.K5B	24.81.1	6201.06	567	54	$1 + 0.008602 \times (N_d - 2)$
7. Refrigerator-freezers— automatic defrost with side-mounted freezer with through-the-door ice service.K5A	30.51.1	6931.06	632	61	$1 + 0.009802 \times (N_d - 3)$
<b>Compact Size Models: Less than 7.75 cubic feet and 36 inches or less in height.K5AB</b>	1.1	1.06			$1 + 0.02 \times (N_d - 3)$
11A. Compact all-refrigerators— manual defrost.K7	41.1	2541.06	226	25	$1 + 0.004902 \times (N_d - 2)$
12. Compact refrigerator-freezers— partial automatic defrost.K7B	41.1	3601.06	324	36	$1 + 0.005802 \times (N_d - 2)$
13. Compact refrigerator-freezers— automatic defrost with top-mounted freezer.K12	5.61.0	4051.0	365	40	$1 + 0.006502 \times (N_d - 1)$
15. Compact refrigerator-freezers— automatic defrost with bottom-mounted freezer.K13A	6.31.1	4141.0	372	41	1.0067

ENERGY STAR Most Efficient annual energy consumption (kWh<sub>me</sub>) may be determined using manufacturer's test data for the given model. Where test data is not available, the algorithms in Table 2-70 for "ENERGY STAR Most Efficient maximum energy usage in kWh/year" may be used

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to determine efficient energy consumption for a conservative savings estimate. Baseline annual energy usage consumption (kWh<sub>base</sub>) of the federal standard model may be determined using Table 2-68. E<sub>ann</sub> stands for Maximum Annual Energy Usage.

Table 2-72: ENERGY STAR Most Efficient Annual Energy Usage if Configuration and Volume Known<sup>Source 4</sup>

Table 2-83: ENERGY STAR and ENERGY STAR Most Efficient Maximum Annual Energy Consumption

Refrigerator Category	ENERGY STAR Maximum Energy Usage in kWh/yr	ENERGY STAR Most Efficient Maximum Annual Energy Usage in kWh/yr
1. Refrigerator-freezers and refrigerators other than all-refrigerators with manual defrost.	$7.19 \times AV + 202.5$	$AV \leq 71.81.1, AEC_{MAX}^{53} \leq 5, E_{ann} \leq 6.39.83 \times AV + 180.0164.3$ $AV > 71.5, E_{ann} 81.1, AEC_{MAX} \leq 637$
1A. All-refrigerators—manual defrost	$6.11 \times AV + 174.2$	-
2. Refrigerator-freezers—partial automatic defrost.	$7.19 \times AV + 202.5$	$AV \leq 71.81.1, AEC_{MAX} \leq 5, E_{ann} \leq 6.39.83 \times AV + 180.0164.3$ $AV > 71.5, E_{ann} 81.1, AEC_{MAX} \leq 637$
3. Refrigerator-freezers—automatic defrost with top-mounted freezer without an automatic icemaker.	$E_{ann} \leq 637 \text{ kWh/yr}$ $7.26 \times AV + 210.3$	-
3—BI. Built-in refrigerator-freezer—automatic defrost with top-mounted freezer without an automatic icemaker.	$E_{ann} \leq 637 \text{ kWh/yr}$ $8.24 \times AV + 238.4$	-
3I. Refrigerator-freezers—automatic defrost with top-mounted freezer with an automatic icemaker without through-the-door ice service.	$7.26 \times AV + 294.3$ $E_{ann} \leq 637 \text{ kWh/yr}$	-
3I—BI. Built-in refrigerator-freezers—automatic defrost with top-mounted freezer with an automatic icemaker.	$E_{ann} \leq 637 \text{ kWh/yr}$ $8.24 \times AV + 322.4$	-

<sup>53</sup> Maximum annual energy consumption.

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Refrigerator Category	ENERGY STAR Maximum Energy Usage in kWh/yr	ENERGY STAR Most Efficient Maximum Annual Energy Usage in kWh/yr	Inserted Cells
without through-the-door ice service			Formatted: Font: Font color: Auto
3A. All-refrigerators—automatic defrost	$6.36 \times AV + 181.4$	-	Formatted: Font: Font color: Auto
3A-BI. Built-in All-refrigerators—automatic defrost	$7.22 \times AV + 205.7$	-	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt
4. Refrigerator-freezers—automatic defrost with side-mounted freezer without an automatic icemaker	$7.66 \times AV + 268.0$	$AV \leq 5867.6, E_{ann}AEC_{MAX} \leq 6.8421 \times AV + 322.2$ $AV > 5867.6, E_{ann}AEC_{MAX} \leq 637$	Formatted: Font color: Auto
4-BI. Built-In Refrigerator-freezers—automatic defrost with side-mounted freezer without an automatic icemaker	$9.20 \times AV + 321.7$	$AV \leq 5867.6, E_{ann}AEC_{MAX} \leq 6.8421 \times AV + 322.2$ $AV > 5867.6, E_{ann}AEC_{MAX} \leq 637$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt
4I. Refrigerator-freezers—automatic defrost with side-mounted freezer with an automatic icemaker without through-the-door ice service	$7.66 \times AV + 352.0$	$AV \leq 46.2, E_{ann}54.0, AEC_{MAX} \leq 6.8421 \times AV + 322.2$ $AV > 46.2, E_{ann}54.0, AEC_{MAX} \leq 637$	Formatted: Font color: Auto
4I-BI. Built-In Refrigerator-freezers—automatic defrost with side-mounted freezer with an automatic icemaker without through-the-door ice service	$9.20 \times AV + 405.7$	$AV \leq 46.2, E_{ann}54.0, AEC_{MAX} \leq 6.8421 \times AV + 322.2$ $AV > 46.2, E_{ann}54.0, AEC_{MAX} \leq 637$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt
5. Refrigerator-freezers—automatic defrost with bottom-mounted freezer without an automatic icemaker	$7.97 \times AV + 285.3$	$AV \leq 54.2, E_{ann} \leq 7.08628, AEC_{MAX} \leq 6.46 \times AV + 253.6$ $AV > 54.2, E_{ann}62.8, AEC_{MAX} \leq 637$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt

Refrigerator Category	ENERGY STAR Maximum Energy Usage in kWh/yr	ENERGY STAR Most Efficient Maximum Annual Energy Usage in kWh/yr	Inserted Cells
5—BI. Built-In Refrigerator-freezers—automatic defrost with bottom-mounted freezer without an automatic icemaker.	$8.46 \times AV + 303.2$	$AV \leq 54.2, E_{ann} \leq 7.0862.8, AEC_{MAX} \leq 6.46 \times AV + 253.6$ $AV > 54.2, E_{ann} \leq 62.8, AEC_{MAX} \leq 637$	Formatted: Font: Font color: Auto Formatted: Font: Font color: Auto Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt Formatted: Font: Font color: Auto Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt Formatted: Font color: Auto
5I. Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.	$7.97 \times AV + 369.3$	$AV \leq 42.3, E_{ann} \leq 7.0849.8, AEC_{MAX} \leq 6.46 \times AV + 337.6$ $AV > 42.3, E_{ann} \leq 49.8, AEC_{MAX} \leq 637$	Formatted: Font color: Auto Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt Formatted: Font color: Auto Formatted: Font color: Auto Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt Formatted: Font color: Auto
5I—BI. Built-In Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.	$8.46 \times AV + 387.2$	$AV \leq 42.3, E_{ann} \leq 7.0849.8, AEC_{MAX} \leq 6.46 \times AV + 337.6$ $AV > 42.3, E_{ann} \leq 49.8, AEC_{MAX} \leq 637$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt Formatted: Font color: Auto Formatted: Font color: Auto Formatted: ... [212] Formatted: Font color: Auto Formatted: ... [213]
5A. Refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service.	$8.33 \times AV + 436.3$	$AV \leq 32.4, E_{ann} \leq 7.4039.6, AEC_{MAX} \leq 6.75 \times AV + 397.1$ $AV > 28.0, E_{ann} \leq 39.6, AEC_{MAX} \leq 637$	Formatted: Font color: Auto Formatted: Font color: Auto Formatted: ... [214] Formatted: Font color: Auto Formatted: ... [215]
5A—BI. Built-in refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service.	$8.85 \times AV + 458.3$	$AV \leq 32.4, E_{ann} \leq 7.4039.6, AEC_{MAX} \leq 6.75 \times AV + 397.1$ $AV > 28.0, E_{ann} \leq 39.6, AEC_{MAX} \leq 637$	Formatted: Font color: Auto Formatted: Font color: Auto Formatted: ... [216] Formatted: Font color: Auto Formatted: ... [217]
6. Refrigerator-freezers—automatic defrost with top-mounted freezer with through-the-door ice service.	$E_{ann} \leq 637 \text{ kWh/yr}$ $7.56 \times AV + 355.3$		Formatted: Font color: Auto Formatted: ... [218] Inserted Cells Formatted: Font color: Auto Formatted: Font color: Auto Formatted: ... [219]
7. Refrigerator-freezers—automatic defrost with side-mounted	$7.69 \times AV + 397.9$	$AV \leq 40.1, E_{ann} \leq 47.9, AEC_{MAX} \leq 6.8323 \times AV + 363.0$	Formatted Table Inserted Cells Formatted: Font color: Auto

Refrigerator Category	ENERGY STAR Maximum Energy Usage in kWh/yr	ENERGY STAR Most Efficient Maximum Annual Energy Usage in kWh/yr	Inserted Cells
freezer with through-the-door ice service		$AV > 35.3, E_{ann} \leq 338.6, AEC_{MAX} \leq 637$	Formatted: Font: Font color: Auto
7-BI. Built-In Refrigerator-freezers—automatic defrost with side-mounted freezer with through-the-door ice service	$9.23 \times AV + 460.7$	$AV \leq 40.1, E_{ann} \leq 338.6, AEC_{MAX} \leq 637$ $AV > 35.3, E_{ann} \leq 338.6, AEC_{MAX} \leq 637$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt
11. Compact refrigerator-freezers and refrigerators other than all-refrigerators with manual defrost	$8.13 \times AV + 227.1$	$AEC_{MAX} \leq 6.32 \times AV + 176.6$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt
11A. Compact all-refrigerators—manual defrost	$7.06 \times AV + 197.2$	$AEC_{MAX} \leq 5.49 \times AV + 153.4$	Formatted: Font color: Auto
12. Compact refrigerator-freezers—partial automatic defrost	$5.32 \times AV + 302.2$	$AEC_{MAX} \leq 4.14 \times AV + 235.1$	Formatted: Font color: Auto
13. Compact refrigerator-freezers—automatic defrost with top-mounted freezer	$10.62 \times AV + 305.3$	$AEC_{MAX} \leq 8.26 \times AV + 237.4$	Formatted: No Spacing,paragraph 6pt space, Space Before: 0 pt, After: 0 pt
13I. Compact refrigerator-freezers—automatic defrost with top-mounted freezer with an automatic icemaker	$10.62 \times AV + 389.3$	$AEC_{MAX} \leq 8.26 \times AV + 321.4$	Formatted: Font color: Auto
13A. Compact all-refrigerators—automatic defrost	$8.25 \times AV + 233.4$	$AEC_{MAX} \leq 6.42 \times AV + 181.5$	Formatted: Font color: Auto
14. Compact refrigerator-freezers—automatic defrost with side-mounted freezer	$6.14 \times AV + 411.2$	$AEC_{MAX} \leq 4.77 \times AV + 319.8$	Formatted: Font color: Auto
14I. Compact refrigerator-freezers—automatic defrost with side-mounted	$6.14 \times AV + 495.2$	$AEC_{MAX} \leq 4.77 \times AV + 403.8$	Formatted: Font color: Auto

Refrigerator Category	ENERGY STAR Maximum Energy Usage in kWh/yr	ENERGY STAR Most Efficient Maximum Annual Energy Usage in kWh/yr
freezer with an automatic icemaker		
15. Compact refrigerator-freezers—automatic defrost with bottom-mounted freezer	$10.62 \times AV + 305.3$	$AEC_{MAX} \leq 8.26 \times AV + 237.4$
15l. Compact refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker	$10.62 \times AV + 389.3$	$AEC_{MAX} \leq 8.26 \times AV + 321.4$

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**DEFAULT SAVINGS**

**DEFAULT SAVINGS**

Table 2-84 displays the default savings for prevalent configurations of ENERGY STAR refrigerators. Default savings assume no special doors (i.e. door coefficient=1). Note that there are zero default savings for ENERGY STAR refrigerator categories 3l, 5l, 5A after 1/30/29, and there are zero default savings for ENERGY STAR refrigerator categories 3, 5, and 7 after 1/30/30. Table 2-85 displays the default savings for prevalent configurations of ENERGY STAR Most Efficient refrigerators.

Table 2-84: Default Savings Values for ENERGY STAR Most Efficient Refrigerators<sup>Source 4</sup> Refrigerators

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Refrigerator Category	Assumed Adjusted Volume of Unit (ft <sup>3</sup> ) <sup>Source 7</sup>	Conventional Unit Energy Usage in kWh/yr <sup>54</sup>	ENERGY STAR Most Efficient Consumption in kWh/yr <sup>Source 4</sup>	ΔkWh	ΔkW <sub>peak</sub>
1. Refrigerator-freezers and refrigerators other than all-refrigerators with manual defrost.	15.1	296	277	20	0.0032
2. Refrigerator-freezers—partial automatic defrost	15.1	346	277	69	0.0112
3l. Refrigerator-freezers—automatic defrost with top-mounted freezer with an automatic icemaker without through-the-door ice service.	22.2	497	397	99	0.0160
4l. Refrigerator-freezers—automatic defrost with side-mounted freezer	28.1	621	514	107	0.0173

<sup>54</sup> Baseline consumption of unit based on category and assumed volume.



Refrigerator Category	Assumed Adjusted Volume of Unit (ft <sup>3</sup> ) <sup>Source 7</sup>	Conventional Unit Energy Usage in kWh/yr <sup>54</sup>	ENERGY STAR-Most Efficient Consumption in kWh/yr <sup>Source 4</sup>	ΔkWh	ΔkW <sub>peak</sub>
with an automatic icemaker without through-the-door ice service.					
5A. Refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service.	34.5	766	630	137	0.0220
5I. Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.	24.8	593	513	80	0.0129
7. Refrigerator-freezers—automatic defrost with side-mounted freezer with through-the-door ice service.	30.5	693	574	122	0.0197

Refrigerator Category	Assumed Adjusted Volume of Unit (cubic feet) <sup>Source 6</sup>	Time Period	ΔkWh/yr	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
3. Refrigerator-freezers—automatic defrost with top-mounted freezer without an automatic icemaker.	18.6	9/15/14 - 1/30/30	38	0.0052065	0.0038991
3I. Refrigerator-freezers—automatic defrost with top-mounted freezer with an automatic icemaker without through-the-door ice service.	21.9	9/15/14 - 1/30/29	41	0.0055680	0.0041698
5. Refrigerator-freezers—automatic defrost with bottom-mounted freezer without an automatic ice maker	29.8	9/15/14 - 1/30/30	49	0.0066335	0.0049677
5I. Refrigerator-freezers—automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.	18.6	9/15/14 - 1/30/29	59	0.0079979	0.0059896
5A. Refrigerator-freezer—automatic defrost with bottom-mounted freezer with through-the-door ice service.	21.9	9/15/14 - 1/30/29	64	0.0086118	0.0064493
7. Refrigerator-freezers—automatic defrost with side-mounted freezer with through-the-door ice service.	29.8	9/15/14 - 1/30/30	60	0.0081494	0.0061030

**Table 2-85: Default Savings Values for ENERGY STAR Most Efficient Refrigerators**

Refrigerator Category	Assumed Adjusted Volume of Unit (cubic feet) <sup>Source 6</sup>	Time Period	$\Delta$ kWh/yr	$\Delta$ kW <sub>summer peak</sub>	$\Delta$ kW <sub>winter peak</sub>
5. Refrigerator-freezers— automatic defrost with bottom-mounted freezer without an automatic ice maker	29.8	9/15/14 - 1/30/30	133	0.0179489	0.0134418
		As of 1/31/30	64	0.0086381	0.0064690
5I. Refrigerator-freezers— automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.	18.6	9/15/14 - 1/30/29	160	0.0216548	0.0162171
		As of 1/31/29	21	0.0028388	0.0021260
5A. Refrigerator-freezer— automatic defrost with bottom-mounted freezer with through-the-door ice service.	21.9	9/15/14 - 1/30/29	172	0.0233271	0.0174695
		As of 1/31/29	9	0.0012321	0.0009227
7. Refrigerator-freezers— automatic defrost with side-mounted freezer with through-the-door ice service.	29.8	9/15/14 - 1/30/30	163	0.0220597	0.0165203
		As of 1/31/30	16	0.0021705	0.0016254

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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- 4) ~~ENERGY STAR Most Efficient 2019 Recognition Criteria for Refrigerator-Freezers. Table 2. <https://www.energystar.gov/sites/default/files/Refrigerator-Freezers%20ENERGY%20STAR%20Most%20Efficient%202019%20Final%20Criteria.pdf>~~
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- 5) ~~Average adjusted volume of ENERGY STAR-certified refrigerators by configuration. Accessed December 2023. 8760 hours. The temperature adjustment factor is 1.23 and is based on Blasnik, Michael, "Measurement and Verification of Residential Refrigerator Energy Use, Final Report, 2003-2004 Metering Study", July 29, 2004 (p. 47) and assuming 78% of refrigerators are in cooled space (based on BGE Energy Use Survey, Report of Findings, December 2005; Mathew Greenwald & Associates) and 22% in un-cooled space. The load shape adjustment factor is 1.15, based on the same report.~~
- 6) ~~ENERGY STAR Appliances Calculator. Accessed July 2018. [https://www.energystar.gov/sites/default/files/asset/document/appliance\\_calculator.xlsx](https://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx)~~
- 7) ~~ENERGY STAR Most Efficient volumes taken from average sizes of qualified units. Energy Star Qualified Models. Accessed July 25, 2018. <https://www.energystar.gov/productfinder/product/certified-residential-refrigerators/results> Weblink~~
- 7) ~~U.S. DOE. (2024, January). Direct final rule. Federal Register, 89 (11), pages 3,026-3,116. Weblink~~

## 2.4.2 ENERGY STAR FREEZERS

Target Sector	Residential <del>Establishments</del>
Measure Unit	Freezer
Measure Life	11 years <sup>Source 43</sup>
<del>Vintage</del>	<del>Replace on Burnout</del>
<u>Vintage</u>	<u>Replace on Burnout</u>

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### ELIGIBILITY

This measure is for the purchase and installation of a new freezer meeting ENERGY STAR criteria. An ENERGY STAR freezer must be at least 10 ~~percent~~% more efficient than the minimum federal government standard.

### ALGORITHMS

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of freezers. ~~The number of freezers will be determined using market assessments and market tracking.~~

If the volume and configuration of the freezer is known, the baseline model's annual energy consumption ( $kWh_{base}$ ) may be ~~are determined using~~ Table 2-86Table 2-86. ~~The efficient model's annual energy consumption ( $kWh_{ee}$ ) may be determined using Table 2-72.~~ ~~The efficient model's annual energy consumption ( $kWh_{ee}$ ) may be determined using manufacturer's test data for the given model.~~ manufacturer's test data for the given model. Where test data is not available the algorithms in ~~Table 2-73~~Table 2-87Table 2-87 for "ENERGY STAR Maximum Energy Usage in  $kWh/year$ " may be used to determine the efficient energy consumption for a conservative savings estimate.

### ENERGY STAR Freezer

$$\Delta kWh = kWh_{base} - kWh_{ee}$$

$$\Delta kW_{peak} \Delta kW_{summer\_peak} = (kWh_{base} - kWh_{ee}) \times \del{ETDF}ETDF_s$$

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### DEFINITION OF TERMS

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$$\del{\Delta kW_{winter\_peak}} = (kWh_{base} - kWh_{ee}) \times ETDF_w$$

**DEFINITION OF TERMS**

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**Table 2-86: Terms, Values, and References for ENERGY STAR Freezers**

Term	Unit	Value	Source
$kWh_{base}$ , Annual energy consumption of baseline unit	$kWh/yr$	EDC Data Gathering Default = Table 2-87	<a href="#">EDC Data Gathering</a> , 1
$kWh_{ee}$ , Annual energy consumption of ENERGY STAR qualified unit	$kWh/yr$	EDC Data Gathering Default = <a href="#">Table 2-73</a> Table 2-89	<a href="#">EDC Data Gathering</a> , 2
<del><math>ETDF</math></del> , <del><math>ETDF_s</math></del> , Summer Energy to Demand Factor	<del><math>\frac{kW}{kWh/yr}</math></del> $\frac{kW}{kWh}$	0.00016140001387	36
<del><math>ETDF_w</math></del> , Winter Energy to Demand Factor	<del><math>\frac{kW}{kWh}</math></del> $\frac{kW}{kWh}$	0.0000998	6

Freezer energy use is characterized by configuration (upright, chest-of-compact), volume, and whether defrost is manual or automatic. If this information is known, annual energy consumption of the federal minimum efficiency standard model may be determined using [Table 2-72](#) Table 2-86. The efficient model's annual energy consumption ( $kWh_{ee}$ ) may be determined using manufacturers' test data for the given model. Where test data is not available, the algorithms in [Table 2-73](#) Table 2-87 for "ENERGY STAR maximum energy usage in kWh/year" may be used to determine efficient energy consumption for a conservative savings estimate. The term "AV" in the equations refers to "Adjusted Volume," which is  $AV = 1.76 \times$  Freezer Volume.

**Table 2-87: Federal Standard and ENERGY STAR Freezers – Maximum Annual Energy Consumption – if Configuration and Volume Known<sup>55</sup>**

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Freezer Category	Federal Standard Maximum Usage (kWh/yr) 9/15/14 - 1/30/29	ENERGY STAR Maximum Energy Usage (kWh/yr) 1/31/2 9 - 1/30/30	As of 1/31/30
8. Upright freezers with manual defrost		$5.57 \times AV + 193.7$	<del><math>5.01 \times AV + 174.3</math></del>
9. Upright freezers with automatic defrost without automatic icemaker	$8.62 \times AV + 228.3$	<del><math>(7.7633 \times AV + 205.5194.1) \times K9 + 281</math></del>	

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<sup>55</sup> Lettering convention (8, 9, 9i, etc) of Federal standard and ENERGY STAR specifications included for clear reference to the standards as well as for correspondence to entries in the default savings table.

Freezer Category	Federal-Standard Maximum Usage (kWh/yr) <del>9/15/14 - 1/30/29</del>	ENERGY STAR Maximum Energy Usage (kWh/yr) <del>1/31/2 9 - 1/30/30</del>	As of 1/31/30
9I. Upright freezers with automatic defrost with an automatic icemaker.	$8.62 \times AV + 312.3$		$7.76 \times AV + 289.5$
<del>9</del> BI. Built-In Upright freezers with automatic defrost without an automatic icemaker.	$9.86 \times AV + 260.9$		$8.87(9.37 \times AV + 234.8247.9) \times K9BI + 281$
9I–BI. Built-in upright freezers with automatic defrost with an automatic icemaker.	$9.86 \times AV + 344.9$		$8.87 \times AV + 318.8$
<u>9A-BI. NEW PRODUCT CLASS: Upright built-in freezer with auto defrost and through-door-ice</u>			$9.86 \times AV + 288.9$
10. Chest freezers and all other freezers except compact freezers.		$7.29 \times AV + 107.8$	<del>8.56</del> $\times AV + 97.0$
10A. Chest freezers with automatic defrost.		$10.24 \times AV + 148.1$	<del>9.22</del> $\times AV + 133.3$
16. Compact upright freezers with manual defrost.	$8.65 \times AV + 225.7$		$7.7935 \times AV + 203.1191.8$
17. Compact upright freezers with automatic defrost.	$10.17 \times AV + 351.9$		$9.15 \times AV + 316.7$
18. Compact chest freezers.	$9.25 \times AV + 136.8$		$8.337.86 \times AV + 123.1107.8$

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The default values for each configuration are given in Table 2-74. Note that a compact freezer is defined as a freezer that has a volume less than 7.75 cubic feet and is 36 inches or less in height.

**DEFAULT SAVINGS**

**Table 2-88: Default Savings Values for ENERGY STAR Freezers: Door Coefficients for Federal Standard Energy Consumption Algorithms**

Freezer Category	Average Unit Adj. Volume (ft <sup>3</sup> )	Conventional Usage <sup>Source 5</sup> (kWh/yr)	ENERGY STAR Usage <sup>Source 5</sup> (kWh/yr)	ΔkWh	ΔkW <sub>peak</sub>		
8. Upright freezers with manual defrost.	42.6	264	237	27	0.0043		
<b>Door Coefficient</b>	<b>Products with a Transparent Door</b>	<b>9. Upright freezers with automatic defrost without an automatic icemaker. Products without a Transparent Door with a Door-in-Door</b>	<b>24.7 Products without a Transparent Door or Door-in-Door with Added External Doors</b>	441	397	44	0.0074
10. Chest freezers and all other freezers except compact freezers. K9	48.51 <sub>0</sub>	2431 <sub>0</sub>	218 <sub>25</sub>	$1 + 0.003902 \times (N_d - 1)$			
16. Compact upright freezers with manual defrost. K9B	3.71 <sub>0</sub>	2571 <sub>0</sub>	234 <sub>26</sub>	$1 + 0.004202 \times (N_d - 1)$			
17. Compact upright freezers with automatic defrost.	7.7	430	387	43	0.0070		
18. Compact chest freezers.	8.9	219	197	22	0.0035		

**Table 2-89: ENERGY STAR and ENERGY STAR Most Efficient Maximum Annual Energy Consumption**

Freezer Category	ENERGY STAR Maximum Energy Usage in kWh/yr	ENERGY STAR Most Efficient Maximum Energy Usage in kWh/yr
8. Upright freezers with manual defrost	$5.01 \times AV + 174.3$	$AV \leq 99.9, AEC_{MAX} \leq 4.73 \times AV + 164.6$ $AV > 99.9, AEC_{MAX} \leq 637$
9. Upright freezers with automatic defrost without an automatic icemaker	$7.76 \times AV + 205.5$	$AV \leq 65.9, AEC_{MAX} \leq 6.90 \times AV + 182.6$ $AV > 65.9, AEC_{MAX} \leq 637$

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<u>Freezer Category</u>	<u>ENERGY STAR Maximum Energy Usage in kWh/yr</u>	<u>ENERGY STAR Most Efficient Maximum Energy Usage in kWh/yr</u>
<u>9I. Upright freezers with automatic defrost with an automatic icemaker</u>	<u><math>7.76 \times AV + 289.5</math></u>	<u><math>AV \leq 53.7, AEC_{MAX} \leq 6.90 * AV + 266.6</math></u> <u><math>AV &gt; 53.7, AEC_{MAX} \leq 637</math></u>
<u>9-BI. Built-In Upright freezers with automatic defrost without an automatic icemaker</u>	<u><math>8.87 \times AV + 234.8</math></u>	<u><math>AV \leq 65.9, AEC_{MAX} \leq 6.90 * AV + 182.6</math></u> <u><math>AV &gt; 65.9, AEC_{MAX} \leq 637</math></u>
<u>9I-BI. Built-in upright freezers with automatic defrost with an automatic icemaker</u>	<u><math>8.87 \times AV + 318.8</math></u>	<u><math>AV \leq 53.7, AEC_{MAX} \leq 6.90 * AV + 266.6</math></u> <u><math>AV &gt; 53.7, AEC_{MAX} \leq 637</math></u>
<u>10. Chest freezers and all other freezers except compact freezers</u>	<u><math>6.56 \times AV + 97.0</math></u>	<u><math>AV \leq 88.0, AEC_{MAX} \leq 6.20 * AV + 91.6</math></u> <u><math>AV &gt; 88.0, AEC_{MAX} \leq 637</math></u>
<u>10A. Chest freezers with automatic defrost</u>	<u><math>9.22 \times AV + 133.3</math></u>	<u><math>AV \leq 58.7, AEC_{MAX} \leq 8.70 * AV + 125.9</math></u> <u><math>AV &gt; 58.7, AEC_{MAX} \leq 637</math></u>
<u>16. Compact upright freezers with manual defrost</u>	<u><math>7.79 \times AV + 203.1</math></u>	<u><math>AEC_{MAX} \leq 6.92 * AV + 180.6</math></u>
<u>17. Compact upright freezers with automatic defrost</u>	<u><math>9.15 \times AV + 316.7</math></u>	<u><math>AEC_{MAX} \leq 8.14 * AV + 281.5</math></u>
<u>18. Compact chest freezers</u>	<u><math>8.33 \times AV + 123.1</math></u>	<u><math>AEC_{MAX} \leq 7.4 * AV + 109.4</math></u>

**DEFAULT SAVINGS**

Table 2-90 displays the default savings for prevalent configurations of ENERGY STAR freezers. Default savings assume no special doors (i.e. door coefficient=1). Note that there are zero default savings for ENERGY STAR freezer category 16 after 1/30/29, and zero default savings for ENERGY STAR freezer category 9 after 1/30/30. Table 2-90 displays the default savings for prevalent configurations of ENERGY STAR Most Efficient refrigerators.



**Table 2-90: Default Savings Values for ENERGY STAR Freezers**

Freezer Category	Assumed Adjusted Volume of Unit (cubic feet) <sup>Source 5</sup>	Time Period	ΔkWh/yr	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
9. Upright freezers with automatic defrost without an automatic icemaker	28.6	9/15/14 - 1/30/30	47	0.0065764	0.0047320
16. Compact upright freezers with manual defrost	5.5	9/15/14 - 1/30/29	27	0.0037872	0.0027251

**Table 2-91: Default Savings Values for ENERGY STAR Most Efficient Freezers**

Freezer Category	Assumed Adjusted Volume of Unit (cubic feet)	Time Period	ΔkWh	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
9. Upright freezers with automatic defrost without an automatic icemaker	28.6	9/15/14 - 1/30/30	95	0.0131667	0.0094740
		As of 1/31/30	24	0.0033021	0.0023760
16. Compact upright freezers with manual defrost	5.5	9/15/14 - 1/30/29	55	0.0075682	0.0054456
		As of 1/31/29	14	0.0018797	0.0013526

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

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- 3)2) Consistent with the conversion factors in the Mid-Atlantic, Illinois, and Wisconsin TRMs. Derived from: (Temperature Adjustment Factor x Load Shape Adjustment Factor)/8760 hours. The temperature adjustment factor is 1.23 and is based on Blasnik, Michael, "Measurement and Verification of Residential Refrigerator Energy Use, Final Report, 2003-2004 Metering Study", July 29, 2004 (p. 47) and assuming 78% of refrigerators are in-cooled space (based on BGE Energy Use Survey, Report of Findings, December 2005; Mathew Greenwald & Associates) and 22% in un-cooled space. The load shape adjustment factor is 1.15, based on the same report. [Weblink](#)
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### 2.4.3 REFRIGERATOR / FREEZER RECYCLING WITH AND WITHOUT REPLACEMENT

<b>Target Sector</b>	Residential <del>Establishments</del>
<b>Measure Life</b>	<p><b>Without Replacement:</b> <sup>Source 1</sup>                      Refrigerator: 5 years                      Freezer: 4 years</p> <p><b>With Replacement (see Measure Life below):</b>                      Refrigerator: 6 years                      Freezer: 5 years</p>
<b>Vintage</b>	Early Retirement, Early Replacement

#### ELIGIBILITY

Refrigerator recycling programs are designed to save energy through the removal of old-but--operable refrigerators from service. By offering free pickup, providing incentives, and disseminating information about the operating cost of old refrigerators, these programs are designed to encourage consumers to:

- Discontinue the use of secondary refrigerators
- Relinquish refrigerators previously used as primary units when they are replaced (rather than keeping the old refrigerator as a secondary unit)
- Prevent the continued use of old refrigerators in another household through a direct transfer (giving it away or selling it) or indirect transfer (resale on the used appliance market).

Commonly implemented by third-party contractors (who collect and decommission participating appliances), these programs generate energy savings through the retirement of inefficient appliances. The decommissioning process captures environmentally harmful refrigerants and foam and enables the recycling of the plastic, metal, and wiring components.

This protocol applies to both residential and non-residential sectors, as refrigerator and freezer usage and energy usage are assumed to be independent of customer rate class.<sup>56</sup> The savings algorithms are based on regression analysis of metered data on kWh consumption from other Statesstates. The savings algorithms for this measure can be applied to refrigerator and freezer retirements or early replacements meeting the following criteria:

- 1) Existing, working refrigerator or freezer 10-30 cubic feet in size (savings do not apply if unit is not working)
- 2) Unit is a primary or secondary unit

~~EDCs can use data gathering to calculate program savings using the savings algorithms, the Existing Unit Energy Consumption (UEC) regression equation coefficients, and actual program year recycled refrigerator/freezer data.~~

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<sup>56</sup> For example, non-residential rate class usage cases include residential dwellings that are master-metered, usage in offices or any other applications that involve typical refrigerator usage.

## ALGORITHMS

The total annual energy savings (kWh/yr) achieved from recycling old-but-operable refrigerators are calculated using the following general algorithm:

### Energy Savings

$$\Delta kWh = N \times (UEC - kWh_{ee}) \times PART_{USE}$$

Note that lifetime savings will be calculated with this same general algorithm but with an adjusted measure life.

### Unit Energy Consumption<sup>Source 2</sup>

To calculate the Annual energy consumption (UEC) of the existing refrigerator or freezer an EDC can calculate program savings calculated using the savings algorithms, the Existing UEC regression equation coefficients, and actual below. Actual program year recycled refrigerator/freezer data. An EDC's use of actual program year data can provide provides a more accurate annual ex ante savings estimate than default values would due to the changing mix of recycled appliance models from year-to-year.

The kWh<sub>ee</sub> of the efficient refrigerator/freezer may be determined using manufacturers' test data for the given model. If test data are not available, the algorithms in Table 2-68 or Table 2-70 may be used to determine the efficient energy consumption for ENERGY STAR and ENERGY STAR Most Efficient models, respectively.

The kWh<sub>ee</sub> of the efficient freezers may be determined using manufacturers' test data for the given model. If test data are not available, the algorithms in Table 2-73 Table 2-83 and Table 2-89 may be used to determine the efficient unit's refrigerator's or freezer's annual energy consumption.

Note that if the unit is being recycled without replacement, the kWh<sub>ee</sub> variable takes on the value of zero. The kWh<sub>ee</sub> variable only applies to direct install replacement of the recycled refrigerator or freezer unit.

$$\begin{aligned}
 UEC_{Refrigerator} &= 365.25 \text{ days} \\
 &\times \left( 0.582 + 0.027 \times AGE + 1.055 \times PRE1990 \right. \\
 &\quad + 0.067 \times AV - 1.977 \times CONFIG_{single-door} + 1.071 \times CONFIG_{side-by-side} \\
 &\quad \left. + 0.605 \times PRIMARY + 0.02 \times \left( UNCONDITIONED \times CDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right. \\
 &\quad \left. - 0.045 \times \left( UNCONDITIONED \times HDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right) \left( 0.582 + 0.027 \times AGE \right. \\
 &\quad + 1.055 \times PRE1990 + 0.067 \times V - 1.977 \times CONFIG_{single-door} \\
 &\quad + 1.071 \times CONFIG_{side-by-side} + 0.605 \times PRIMARY \\
 &\quad \left. + 0.02 \times \left( UNCONDITIONED \times CDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right. \\
 &\quad \left. - 0.045 \times \left( UNCONDITIONED \times HDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right)
 \end{aligned}$$

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$$UEC_{Freezer} = 365.25 \text{ days}$$

$$\begin{aligned} & \times \left( -0.955 + 0.0454 \times AGE + 0.543 \times PRE1990 + 0.120 \times AV \right. \\ & \left. + 0.298 \times CONFIG_{chest} + 0.082 \times \left( UNCONDITIONED \times CDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right. \\ & \left. - 0.031 \times \left( UNCONDITIONED \times HDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right) \left( -0.955 + 0.0454 \times AGE \right. \\ & \left. + 0.543 \times PRE1990 + 0.120 \times V + 0.298 \times CONFIG_{chest} \right. \\ & \left. + 0.082 \times \left( UNCONDITIONED \times CDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right. \\ & \left. - 0.031 \times \left( UNCONDITIONED \times HDD \div 365.25 \frac{\text{days}}{\text{year}} \right) \right) \end{aligned}$$

### Adjusted Volume (AV)

The adjusted volume equations below account for the greater load of freezer compartments compared to compartments for fresh food. For Category 1 and 1A "All-refrigerators":

$$AV = \text{Fresh Volume} + \text{Freezer Volume}$$

For all other categories:

$$AV = \text{Fresh Volume} + 1.76 \times \text{Freezer Volume}$$

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### Part-Use Factor

When calculating default per unit kWh savings for a removed refrigerator or freezer, it is necessary to calculate and apply a "Part-Use" factor. "Part-use" is an appliance recycling-specific adjustment factor used to convert the UEC (determined through the methods detailed above) into an average per-unit deemed savings value. The UEC itself is not equal to the default savings value, because: (1) the UEC model yields an estimate of annual consumption, and (2) not all recycled refrigerators and freezers would have operated year-round had they not been decommissioned through the program.

In Program Year 38, the Commission determined that the average removed refrigerator was plugged in and used 72.8% of the year and the average freezer was plugged in and used 84.5% of the year.<sup>Source 43</sup> These are the default values for the part-use factor. EDCs may elect to calculate an EDC-specific part-use factor for a specific program year. In the event an EDC desires to calculate an EDC-specific part-use factor, EDCs should use the methodology described in section 4.34 of the DOE, Uniform Methods Project protocol.<sup>Source 32</sup>

### Peak Demand Savings

Use the below algorithm to calculate the peak demand savings. Multiply the annual kWh savings by an Energy to Demand Factor (ETDF), which is supplied below.

$$\Delta kW_{peak}$$

#### Peak Demand Savings

Use the below algorithms to calculate peak demand savings.

$$\Delta kW_{summer\_peak} = \Delta kWh \times ETDF_{ETDF_s}$$

$$\Delta kW_{winter\_peak} = \Delta kWh \times ETDF_w$$

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## DEFINITION OF TERMS

Table 2-92: Terms, Values, and References for Refrigerator and Freezer Recycling

Term	Unit	Values	Source
<i>N</i> , The number of refrigerators or freezers recycled through the program	None	EDC Data Gathering	EDC Data Gathering
<i>PART_USE</i> , The portion of the year the average refrigerator or freezer would likely have operated if not recycled through the program	%	EDC Data Gathering According to Section 4.4 of UMP Protocol Default: Refrigerator = 72.8% Freezer = 84.5%	4EDC Data Gathering, 3
<i>ETDF<sub>s</sub></i> , Summer Energy to Demand Factor	$\frac{kW}{kWh/yr}$	0.0001614Refrigerator = 0.0001354 Freezer = 0.0001387	54
<i>ETDF<sub>w</sub></i> , Winter Energy to Demand Factor	$\frac{kW}{kWh/yr}$	Refrigerator = 0.0001014 Freezer = 0.0000998	4
<i>AGE</i> , age of appliance	years	EDC Data Gathering	EDC Data Gathering
<i>PRE1990</i> , Fraction of appliances manufactured before 1990	%	EDC Data Gathering	EDC Data Gathering
<i>AV</i> , Adjusted Volume/calculated as described above of recycled unit	ft <sup>3</sup>	EDC Data Gathering	EDC Data Gathering
<i>CONFIG<sub>single-door</sub></i> , Fraction of refrigerators with single-door configuration	%	EDC Data Gathering	EDC Data Gathering
<i>CONFIG<sub>side-by-side</sub></i> , Fraction of refrigerators with side-by-side configuration	%	EDC Data Gathering	EDC Data Gathering
<i>CONFIG<sub>chest</sub></i> , Fraction of freezers with chest configuration	%	EDC Data Gathering	EDC Data Gathering
<i>PRIMARY</i> , Fraction of appliances in primary use (in absence of program)	%	EDC Data Gathering	EDC Data Gathering
<i>UNCONDITIONED</i> , Fraction of appliances located in Unconditioned space	%	EDC Data Gathering Default: Refrigerator=812% Freezer=4552%	9EDC Data Gathering, 7
<i>CDD</i> , Cooling degree days	°F-day/year	See <b>CDD65</b> in Vol. 1, App. A	408
<i>HDD</i> , Heating degree days	°F-day/year	See <b>HDD65</b> in Vol. 1, App. A	408
<i>kWh<sub>ee</sub></i> , Annual energy consumption of ENERGY STAR qualified unit	kWh/yr	EDC Data Gathering  Refrigerator Default: See Table 2-68 or Table 2-70 in Table 2-84 in Sec. 2.4.12.4.1 ENERGY STAR Refrigerators  Freezer Default: See Table 2-73 Table 2-90 in Sec. 2.4.22.4.2 ENERGY STAR Freezers	7,8EDC Data Gathering, 6

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Refrigerator energy use is characterized by configuration (top freezer, bottom freezer, etc.), volume, whether defrost is manual or automatic and whether there is through the door ice. The efficient model's annual energy consumption may be determined using manufacturer's test data for the given model. If test data are not available, the algorithms Table 2-68 or Table 2-70 in Sec. 2.4.1 ENERGY STAR Refrigerators may be used to determine the efficient energy consumption for ENERGY STAR and ENERGY STAR Most Efficient models, respectively. The default values for each configuration are reported in Table 2-69 (ENERGY STAR) or Table 2-71 (ENERGY STAR Most Efficient) in Sec. 2.4.1, ENERGY STAR Refrigerators.

~~Freezer energy use is characterized by configuration (upright, chest or compact), volume and whether defrost is manual or automatic. The efficient model's annual energy consumption may be determined using manufacturers' test data for the given model. If test data are not available, the algorithms in Table 2-73 in Sec. 2.4.2, ENERGY STAR Freezers may be used to determine the efficient unit's energy consumption. The default values for each configuration are reported in Table 2-74 in the ENERGY STAR Freezers section. Note that a compact freezer is defined as a freezer that has a volume less than 7.75 cubic feet and is 36 inches or less in height.~~

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## MEASURE LIFE

The measure lives for refrigerators and freezers recycled without replacement are 5 years and 4 years, respectively, from the California ~~DEER EUA table~~. ~~Electronic Technical Reference Manual~~. These values represent 1/3 of the EUL of a new refrigerator or freezer.

For refrigerators and freezers recycled with replacement, the adjusted measure life is 6 years for refrigerators and 5 years for freezers.

### Adjusted Measure Life Rationale:

Refrigerator/freezer recycling with replacement programs commonly calculate savings over two periods, the RUL of the existing unit, and the remainder of the EUL of the efficient unit beyond the RUL of the existing unit. For the first period of savings (the RUL of the existing unit), the energy savings are equal to the savings difference between the existing baseline unit and the ENERGY STAR unit; the RUL can be assumed to be 1/3 of the measure EUL of the ENERGY STAR unit. For the second period of savings (the remaining EUL of the efficient unit), the energy savings are equal to the difference between a Federal Standard unit and the ENERGY STAR unit.

The EUL of a new ENERGY STAR refrigerator is ~~12~~14 years (see the ~~ENERGY STAR Refrigerators~~ENERGY STAR Refrigerators section). However, a study of a low-income refrigerator replacement program for SDG&E (2006) found that among the program's target population, refrigerators are likely to be replaced less frequently than among average customers. As a result, the report updating the California DEER database recommended an EUL of 18 years for such programs. <sup>Source 65</sup>

To simplify the calculation of savings and remove the need to calculate two different savings, an adjusted value for measure life of 6 years for both low-income specific and non-low-income specific programs can be used with the savings difference between the existing baseline unit and the ENERGY STAR unit over the adjusted measure life. The 6-year adjusted measure life is derived by averaging the lifetime savings of a non-low-income replacement with a ~~12~~14-year measure life and a low-income replacement with an 18-year measure life.

The derivation of the 6-year adjusted measure life can be demonstrated with an example of a typical refrigerator replacement with an ENERGY STAR unit. Assuming a refrigerator of type 5l in the ~~ENERGY STAR Refrigerators~~ENERGY STAR Refrigerators section with an adjusted volume of 20 ft<sup>3</sup>, annual savings would be 578 kWh for the RUL of the existing baseline unit and ~~annual savings of~~ 49 kWh for the remaining EUL.<sup>57</sup>

In the case of a non-low-income program there is an RUL of ~~45~~ years for the existing unit ( $1/3 * 12 = 4$ ) and a remaining EUL of the efficient unit of ~~89~~ years ( $2/3 * 12 = 8$ ). The lifetime savings are equal to ~~2,7063,331~~ kWh ( $578 \text{ kWh/yr} * 4 \text{ yrs} + 49 \text{ kWh} / \text{yr} * 8 \text{ yrs}$ ), resulting in an adjusted measure life of ~~56~~ years:  $2,7063,331 \text{ kWh} / 578 \text{ kWh/yr} = 56$  years.

In the case of a low-income program there is an RUL of 6 years for the existing unit ( $1/3 * 18 = 6$ ) and a remaining EUL of the efficient unit of 12 years ( $2/3 * 18 = 12$ ). The lifetime savings are equal to

<sup>57</sup> A refrigerator with automatic defrost with bottom-mounted freezer with an automatic icemaker without through-the-door ice service.

4,059056 kWh (578 kWh/yr \* 6 yrs + 49 kWh / yr \* 12 yrs), resulting in an adjusted measure life of 7 years: 4,059056 kWh / 578 kWh/yr = 7 years.

Averaging the two lifetime savings values results in an adjusted measure life of 6 years (3,383694 kWh / 578 kWh/yr = 6 years) that can be used for both low-income specific and non-low-income specific programs.

## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

1) California Public Utilities Commission Database for Energy Efficient Resources (DEER)-EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx> Accessed December 2018.

1) US DOE Uniform Method Project, Savings Protocol for Refrigerator Retirement, April California Electronic Technical Reference Manual. "Refrigerator or Freezer, Residential". Accessed December 2023. Weblink

2) Keeling, J., Bruchs, D. (2017). <https://www.nrel.gov/docs/fy17osti/68563.pdf>

3) U.S. Department of Energy, Uniform Methods Project protocol titled "Chapter 7: Refrigerator Recycling Evaluation Protocol", prepared by Doug Bruchs and Josh Keeling of the Cadmus Group, September 2013. The Uniform Methods Project: Methods for Determining Energy-Efficiency Savings for Specific Measures". Section 4.4. National Renewable Energy Laboratory. <https://www.nrel.gov/docs/fy17osti/68563.pdf> Weblink

4) Based on a Cadmus survey of 510 PPL participants in PY8.

5) Consistent with the conversion factors in the Mid-Atlantic, Illinois, and Wisconsin TRMs. Derived from: (Temperature Adjustment Factor x Load Shape Adjustment Factor)/8760 hours. The temperature adjustment factor is 1.23 and is based on Blasnik, Michael, "Measurement and Verification of Residential Refrigerator Energy Use, Final Report, 2003-2004 Metering Study", July 29, 2004 (p. 47) and assuming 78% of refrigerators are in-cooled space (based on BGE Energy Use Survey, Report of Findings, December 2005; Mathew Greenwald & Associates) and 22% in un-cooled space. The load shape adjustment factor is 1.15, based on the same report.

4) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

6) Seiden, K., Bruchs, D., Peters, J., Moran, D., Burdick, M. (2006, July). "2004-2005 Final Report: A Measurement and Evaluation Study of the 2004-2005 Limited Income Refrigerator Replacement & Lighting Program, Prepared for: San Diego Gas & Electric, July 31, 2006". Weblink

Federal Standards for Residential Refrigerators and Freezers, Effective 9/14/

7) U.S. EPA. (2014). [http://www1.eere.energy.gov/buildings/appliance\\_standards/product.aspx/productid/43](http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/43)

8) ENERGY STAR Program Requirements Product Specifications for Residential Refrigerators and Freezers Consumer Refrigeration Products, Version 5.0, Effective 9/15/2014.1.

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[https://www.energystar.gov/ia/partners/product\\_specs/program\\_reqs/Refrigerators\\_and\\_Freezers\\_Program\\_Requirements\\_V5.0.pdf](https://www.energystar.gov/ia/partners/product_specs/program_reqs/Refrigerators_and_Freezers_Program_Requirements_V5.0.pdf). Weblink

- 9) Statewide average Proportion of refrigerators and freezers calculated using data gathered for all housing types from 2023 Pennsylvania Act 129-2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf).

- 10) PA SWE Team Calculations with data from the National Solar Radiation Database, 1991-2005 Update: Typical Meteorological Year 3. NREL. [http://rredc.nrel.gov/solar/old\\_data/nsrdb/1991-2005/tmy3/by\\_state\\_and\\_city.html](http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html).

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#### **~~2.4.4 ENERGY STAR CLOTHES WASHERS~~**

- 8) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)

### 2.4.4 LOW-CAPACITY REFRIGERATOR / FREEZER RECYCLING WITHOUT REPLACEMENT

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Clothes Washer
<b>Measure Life</b>	14 years <sup>Source 1</sup> Without Replacement: <sup>Source 1</sup> Refrigerator: 5 years Freezer: 4 years
<b>Vintage</b>	Replace on Burnout/Early Retirement

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#### ELIGIBILITY

Refrigerator and freezer recycling programs are designed to save energy through the removal of old-but-operable compact refrigerators and freezers from service. This measure focuses on “mini-fridges” and small freezers, including those regulated as compact refrigerators and freezers (which are defined as having a total volume of 7.5 ft<sup>3</sup> or less), specifically those units with an interior size (total volume) less than 10 cubic feet which are excluded from the Uniform Methods Project-based 2.4.3 Refrigerator / Freezer Recycling of the 2026 TRM.

By offering free pickup, providing incentives, and disseminating information about the operating cost of old compact refrigerators, these programs are designed to encourage consumers to:

- Discontinue the use of secondary compact refrigerators
- Relinquish compact refrigerators previously used as primary units when they are replaced (rather than keeping the old compact refrigerator as a secondary unit or on site of a large facility)
- Prevent the continued use of old compact refrigerators in another location through a direct transfer (giving it away or selling it) or indirect transfer (resale on the used appliance market).

This protocol applies to both residential and non-residential sectors, as refrigerator and freezer usage and energy usage are assumed to be independent of customer rate class. The savings algorithms are based on current and historic federal efficiency standards for refrigerators and freezers. The savings algorithms for this measure can be applied to refrigerator and freezer retirements meeting the following criteria:

- 1) Existing, working compact refrigerator or freezer less than 10 cubic feet in size (savings does not apply if unit is not working)
- 2) Unit is a primary, secondary, or abandoned

EDCs can use data gathering to calculate program savings using the federal efficiency standards, and actual program year recycled refrigerator/freezer data.

#### ALGORITHMS

The total annual energy savings (kWh/yr) achieved from recycling old-but-operable refrigerators are calculated using the following general algorithms:

##### Energy Savings

$$\Delta kWh = UEC \times PART_{USE}$$

Note that lifetime savings will be calculated with this same general algorithm but with an adjusted measure life.

### **Unit Energy Consumption (UEC)**

Recognizing that determination of appliance characteristics via measurement or make/model lookup may be impractical in some cases, several options for determining the UEC of the existing refrigerator or freezer are permitted, listed below. Option 1 uses the product class average UECs provided in Table 2. The remaining options are more precise than Option 1 and are listed in descending order of precision (Options 2 through 5). EDCs may choose to forego the extra documentation required for the more precise calculation options but note that these options should allow for the capture of more savings.

- 1) The default class-dependent UEC from Table 2.
- 2) The official label energy rating for the model such as from an EnergyGuide or historic ENERGY STAR records. Documentation should include the model number and information source.
- 3) Calculated from class-dependent formula in Table 3 with age verified by nameplate, compressor age, or model and serial number, and adjusted or total volume verified from (1) the nameplate, (2) similar sources as option 2, or (3) measured in the field.
- 4) Calculated from class-dependent formula in Table 3 with age verified by nameplate, compressor age, or model and serial number, using the age-appropriate default volume from Table 4.
- 5) Calculated from the “2015 to date” class-dependent formula in Table 3 with total volume verified from nameplate or measured Adjusted volume.

If both fresh and freezer compartment volumes are available, adjusted volume should be calculated as follows:

$$\underline{\text{All Refrigerator}^{58} \text{ AV}} = \text{Total Volume} = \text{Fresh Volume} + \text{Freezer Volume}$$

$$\underline{\text{Refrigerator AV}} = \text{Fresh Volume} + 1.63 \times \text{Freezer Volume}$$

$$\underline{\text{Freezer AV}} = 1.76 \times \text{Freezer Volume}$$

Otherwise, the class-dependent average adjusted volume to total volume ratio may be used from Table 4.

### **Part-Use Factor**

When calculating per unit kWh savings for a removed refrigerator or freezer, it is necessary to calculate and apply a “Part-Use” factor. “Part-use” is an appliance recycling-specific adjustment factor used to convert the UEC (determined through the methods described above) into an average per-unit deemed savings value. The UEC itself is not equal to the default savings value, because: (1) the UEC model yields an estimate of annual consumption, and (2) not all recycled refrigerators and freezers would have operated year-round had they not been decommissioned through the program.

In Program Year 8, the Commission determined that the average removed standard size refrigerator was plugged in and used 72.8% of the year and the average freezer was plugged in and used 84.5% of the year. <sup>Source 2</sup> These are the default values for the part-use factor. EDCs may elect to calculate an EDC-specific part-use factor for a specific program year. In the event an EDC desires to calculate an EDC-specific part-use factor, EDCs should use the methodology described in section 4.4 of the DOE, Uniform Methods Project protocol. <sup>Source 3</sup>

<sup>58</sup> An all-refrigerator is an appliance in which the freezer compartment—generally the cooling coil as a U shape within the fresh volume—has a volume of 0.5 ft<sup>3</sup> or less.

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### Peak Demand Savings

Use the below algorithm to calculate the peak demand savings. Multiply the annual kWh savings by an Energy to Demand Factor (ETDF), which is supplied below.

This measure is for the purchase and installation of a clothes washer meeting ENERGY STAR eligibility criteria. ENERGY STAR clothes washers use less energy and hot water than non-qualified models.

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### ELIGIBILITY

This protocol documents the energy savings attributed to purchasing an ENERGY STAR clothes washer instead of a standard one. If a customer submits a rebate for a product that has applied for ENERGY STAR Certification but has not yet been certified, the savings will be counted for that product contingent upon its eventual certification as an ENERGY STAR measure. If at any point the product is rejected by ENERGY STAR, the product is then ineligible for the program and savings will not be counted. The target sector is residential.

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### ALGORITHMS

The general form of the equation for the ENERGY STAR Clothes Washer measure savings algorithm is:

$$\text{Total Savings} = \text{Number of Clothes Washers} \times \text{Savings per Clothes Washer}$$

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of clothes washers.

Per unit energy and demand savings are given by the following algorithms:

$$\Delta kWh = \text{Cycles} \times$$

$$\left( \frac{CAPY_{base}}{IMEF_{base}} \times \left( CW_{base} + DHW_{base} \times \%_{elecDHW} + Dryer_{base} \times \%_{elecDryer} \times \%_{dry wash} \right) \right) - \left( \frac{CAPY_{ee}}{IMEF_{ee}} \times \left( CW_{ee} + DHW_{ee} \times \%_{elecDHW} + Dryer_{ee} \times \%_{elecDryer} \times \%_{dry wash} \right) \right)$$

$$\Delta kW_{peak} = \frac{\Delta kWh}{\text{Cycles} \times \text{Time}_{cycle}} \times CF$$

Where IMEF is the Integrated Modified Energy Factor, which is the energy performance metric for clothes washers. IMEF is defined as:

IMEF is the quotient of the cubic foot capacity of the clothes container, C, divided by the total clothes washer energy consumption per cycle, with such energy consumption expressed as the sum of the machine electrical energy consumption (M), the hot water energy consumption (E), the energy required for removal of the remaining moisture in the wash load (D), and the combined low-power mode energy consumption (L). The higher the value, the more efficient the clothes washer is. <sup>Source 2</sup>

$$IMEF = \frac{C}{(M + E + D + L)}$$

### DEFINITION OF TERMS

$$\Delta kW_{summer peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter peak} = \Delta kWh \times ETDF_w$$

**DEFINITION OF TERMS**

**Table 2-93: Terms, Values, and References for ENERGY STAR Clothes Washers/Mini-Frig Recycling**

Term	Unit	Value	Source
$CAP_{base}$ – Capacity of baseline clothes washer	$ft^3$	EDC Data Gathering Default: 3.5	EDC Data Gathering 4
$CAP_{EE}$ – Capacity of ENERGY STAR clothes washer	$ft^3$	EDC Data Gathering Default: 3.5	EDC Data Gathering 4
$IMEF_{base}$ – Integrated Modified Energy Factor of baseline clothes washer	$\frac{ft^3}{(kWh/cycle)}$	Table 2-77	8
$IMEF_{EE}$ – Integrated Modified Energy Factor of ENERGY STAR clothes washer	$\frac{ft^3}{(kWh/cycle)}$	EDC Data Gathering Default: Table 2-77	EDC Data Gathering 2
Cycles – Number of clothes washer cycles per year	$\frac{cycles}{yr}$	254	5
$CW_{base}$ – % of total energy consumption for baseline clothes washer mechanical operation	%	8.1%	4
$CW_{EE}$ – % of total energy consumption for ENERGY STAR clothes washer mechanical operation	%	5.8%	4
$DHW_{base}$ – % of total energy consumption attributed to baseline clothes washer water heating	%	26.5%	4
$DHW_{EE}$ – % of total energy consumption attributed to ENERGY STAR clothes washer water heating	%	34.2%	4
$\%_{ElecDWH}$ – % of water heaters that are electric	%	EDC Data Gathering Default: 35%	EDC Data Gathering 3
$Dryer_{base}$ – % of total energy consumption for baseline clothes washer/dryer operation	%	65.4%	4

Term	Unit	Value	Source
$Dryer_{EE}$ – % of total energy consumption for ENERGY STAR clothes washer dryer operation	%	63.0%	4
$\%_{elec\ dryer}$ – Percentage of dryers that are electric	%	EDC Data Gathering Default: 74%	EDC Data Gathering 3
$\%_{dry}$ – Percentage of homes with a dryer that use the dryer every time clothes are washed	%	Default= 96% Or EDC data gathering	5
$Time_{cycle}$ – average duration of a clothes washer cycle	hours	1.04	6
$CF$ – Demand Coincidence Factor. The coincidence of average clothes washer demand to summer system peak	Proportion	0.029	7

The current federal standard for clothes washers went into effect on January 1, 2018, and is not scheduled to change until 2024. The efficiency standards are detailed in Table 2-77.

Note that the current standards are based on the Integrated Modified Energy Factor (IMEF) and Integrated Water Factor (IWF). The IMEF incorporates energy use in standby and off modes and includes updates to the provisions of per-cycle measurements. The IWF more accurately represents consumer usage patterns as compared to the current metric. Previous standards were based on MEF and WF.

Term	Unit	Values	Source
<u>UEC, Unit Energy Consumption</u>	<u>kWh/yr</u>	<u>EDC Data Gathering</u> <u>Default in Table 2</u>	<u>Varies</u>
<u>Total Volume, Fresh plus Frozen Volume</u>	<u>ft<sup>3</sup></u>	<u>EDC Data Gathering</u>	
<u>Fresh Volume, volume of refrigerator</u>	<u>ft<sup>3</sup></u>	<u>EDC Data Gathering</u>	
<u>Frozen Volume, volume capable of maintaining 0°F</u>	<u>ft<sup>3</sup></u>	<u>EDC Data Gathering</u>	
<u>AV, Adjusted Volume/calculated as described above</u>	<u>ft<sup>3</sup></u>	<u>EDC Data Gathering,</u> <u>defaults in Table 4</u>	<u>6–8</u>
<u>PART USE, the portion of the year the average refrigerator or freezer would likely have operated if not recycled through the program</u>	<u>%</u>	<u>EDC Data Gathering</u> <u>According to Section 4.4 of</u> <u>UMP Protocol</u> <u>Default:</u> <u>Refrigerator= 72.8%</u> <u>Freezer= 84.5%</u>	<u>2</u>
<u>ETDF<sub>s</sub>, Summer peak Energy to Demand Factor</u>	<u>kW</u> <u>kWh</u>	<u>Refrigerator = 0.0001354</u> <u>Freezer = 0.0001387</u>	<u>4</u>
<u>ETDF<sub>w</sub>, Winter peak Energy to Demand Factor</u>	<u>kW</u> <u>kWh</u>	<u>Refrigerator = 0.0001014</u> <u>Freezer = 0.0000998</u>	<u>4</u>

**Table 2-94: Federal Standards and ENERGY STAR Specifications for Clothes Washers<sup>Source 2-8</sup>: Product Class Descriptions and Default UEC**

Configuration	Minimum IMEF	ENERGY STAR Minimum IMEF
Top-loading, Standard	1.57	2.06
Front-loading, Standard	1.84	2.76

**DEFAULT SAVINGS**

Product Class <sup>59</sup>	Average UEC (kWh/yr)
11 - Compact refrigerator and Refrigerator-Freezer other than All-Refrigerator - manual defrost	288.3
11A - Compact all-refrigerator - manual defrost <sup>60</sup>	242.7
12 - Compact refrigerator-freezer - partial automatic defrost	361.7
13 - Compact refrigerator-freezers - automatic defrost with top-mounted freezer	405.2
13I - Compact refrigerator-freezers - automatic defrost with top-mounted freezer and automatic icemaker	298.2
13A - Compact all-refrigerators - automatic defrost	538.8
14 - Compact refrigerator-freezer - automatic defrost with side-mounted freezer	492.1
14I - Compact refrigerator-freezer - automatic defrost with side-mounted freezer and automatic icemaker	571.5
15 - Compact refrigerator-freezer - automatic defrost with bottom-mounted freezer	413.4
15I - Compact refrigerator-freezer - automatic defrost with bottom-mounted freezer and automatic icemaker	486.3
16 - Compact upright freezers with manual defrost	253.6
17 - Compact upright freezers with automatic defrost	394.5
18 - Compact chest freezers	180.1

<sup>59</sup> This measure uses the federal efficiency standards for compact refrigerators and freezers, which are defined as having a total volume of 7.5 ft<sup>3</sup> or less. However, this measure is also meant to cover equipment with a total volume of 10 ft<sup>3</sup>, which are excluded from section 2.4.3 Refrigerator/Freezer Recycling of the 2026 TRM.

<sup>60</sup> An all-refrigerator is an appliance in which the freezer compartment—(generally the exposed cooling coil as a U shape within the fresh volume)—has a volume of 0.5 ft<sup>3</sup> or less.



**Table 2-95: Default Clothes Washer Savings: Federal Standard-Based UEC by Product Class**

<u>Class</u>	<u>1992 or earlier (1/1/1990)</u>	<u>1993 to 2000 (1/1/1993)</u>	<u>2001 to 2014 (1/1/2001)</u>	<u>2015 to date (9/14/2014)</u>
<u>11</u>	<u><math>16.3 \times AV + 316</math></u>	<u><math>13.5 \times AV + 299</math></u>	<u><math>10.70 \times AV + 299.0</math></u>	<u><math>9.03 \times AV + 252.3</math></u>
<u>11A</u>				<u><math>7.84 \times AV + 219.1</math></u>
<u>12</u>	<u><math>21.8 \times AV + 429</math></u>	<u><math>10.4 \times AV + 398</math></u>	<u><math>7.00 \times AV + 398.0</math></u>	<u><math>5.91 \times AV + 335.8</math></u>
<u>13</u>	<u><math>23.5 \times AV + 471</math></u>	<u><math>16.0 \times AV + 355</math></u>	<u><math>12.70 \times AV + 355.0</math></u>	<u><math>11.80 \times AV + 339.2</math></u>
<u>13I</u>				<u><math>11.80 \times AV + 423.2</math></u>
<u>13A</u>				<u><math>9.17 \times AV + 259.3</math></u>
<u>14</u>	<u><math>27.7 \times AV + 488</math></u>	<u><math>11.8 \times AV + 501</math></u>	<u><math>7.60 \times AV + 501.0</math></u>	<u><math>6.82 \times AV + 456.9</math></u>
<u>14I</u>				<u><math>6.82 \times AV + 540.9</math></u>
<u>15</u>	<u><math>27.7 \times AV + 488</math></u>	<u><math>16.5 \times AV + 367</math></u>	<u><math>13.10 \times AV + 367.0</math></u>	<u><math>11.80 \times AV + 339.2</math></u>
<u>15I</u>				<u><math>11.80 \times AV + 423.2</math></u>
<u>16</u>	<u><math>10.9 \times AV + 422</math></u>	<u><math>10.3 \times AV + 264</math></u>	<u><math>9.78 \times AV + 250.8</math></u>	<u><math>8.65 \times AV + 225.7</math></u>
<u>17</u>	<u><math>16.0 \times AV + 623</math></u>	<u><math>14.9 \times AV + 391</math></u>	<u><math>11.40 \times AV + 391.0</math></u>	<u><math>10.17 \times AV + 351.9</math></u>
<u>18</u>	<u><math>14.8 \times AV + 223</math></u>	<u><math>11.0 \times AV + 160</math></u>	<u><math>10.45 \times AV + 152.0</math></u>	<u><math>9.25 \times AV + 136.8</math></u>

The average adjusted volumes below were calculated by the SWE using a combined database of refrigerators and freezers from Sources 5–8. These were combined into a single data set, and readily identifiable duplicate entries were removed. In addition, low-voltage devices intended for use in cars and RVs were excluded. The number of models in each class is given, as are some historic class prevalence data based on AHAM sales information from 2008.

**Table 2-96: Average Adjusted Volume (AV) and AV to Total Volume ratio by Product Class**

Class	Compact Products Historic Share <small>Source 5</small>	Adjusted Volume <small>Sources 6 - 8</small>			
		Sample Size	2014 or earlier	2015 to date	AV ÷ Total Vol.
<u>11</u>	<u>69%</u>	<u>51</u>	<u>3.13</u>	<u>4.3</u>	<u>109%</u>
<u>11A</u>		<u>626</u>		<u>3.0</u>	<u>101%</u>
<u>12</u>	<u>4.9%</u>	<u>369</u>	<u>5.2</u>	<u>5.2</u>	<u>118%</u>
<u>13</u>	<u>0.7%</u>	<u>58</u>	<u>4.4</u>	<u>6.7</u>	<u>121%</u>
<u>13I</u>		<u>1</u>		<u>11.7</u>	<u>119%</u>
<u>13A</u>		<u>1,029</u>		<u>4.2</u>	<u>100%</u>
<u>14</u>	<u>0.3%</u>	<u>27</u>	<u>5.5</u>	<u>6.0</u>	<u>116%</u>
<u>14I</u>		<u>24</u>		<u>4.9</u>	<u>110%</u>
<u>15</u>	<u>0.3%</u>	<u>20</u>	<u>7.4</u>	<u>7.9</u>	<u>125%</u>
<u>15I</u>		<u>21</u>		<u>7.0</u>	<u>130%</u>
<u>16</u>	<u>9.1%</u>	<u>84</u>	<u>5.5</u>	<u>5.5</u>	=
<u>17</u>	<u>5.5%</u>	<u>44</u>	<u>6.9</u>	<u>6.9</u>	=
<u>18</u>	<u>3.6%</u>	<u>223</u>	<u>8.2</u>	<u>8.2</u>	=

**Measure Life**

Fuel Mix	Washer Type	DkWh	$\Delta kW_{peak}$
Electric-DHW/Electric-Dryer	Top-Loading	129.2	0.0144
	Front-Loading	154.7	0.0172
Electric-DHW/Gas-Dryer	Top-Loading	35.8	0.0040
	Front-Loading	47.4	0.0053
Gas-DHW/Electric-Dryer	Top-Loading	144.0	0.0127
	Front-Loading	127.5	0.0142
Gas-DHW/Gas-Dryer	Top-Loading	20.6	0.0023
	Front-Loading	20.2	0.0022
Default (35% Electric-DHW, 75% Electric-Dryer)	Top-Loading	95.0	0.0106
	Front-Loading	109.1	0.0124

The measure lives for refrigerators and freezers recycled without replacement are 5 years and 4 years, respectively, from the California Electronic Technical Reference Manual. These values represent 1/3 of the EUL of a new refrigerator or freezer.

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

- 1) ~~Energy Star Calculator, EPA research on available models. Accessed August 2018.  
[https://www.energystar.gov/sites/default/files/asset/document/appliance\\_calculator.xlsx](https://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx)~~
- 2) ~~ENERGY STAR Clothes Washers Product Specification Version 7.0.  
[https://www.energystar.gov/products/appliances/clothes\\_washers/key\\_product\\_criteria](https://www.energystar.gov/products/appliances/clothes_washers/key_product_criteria)~~
- 3) ~~Statewide average for all housing types from Pennsylvania Act 129 2018 Residential Baseline Study, 2018, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf).~~
- 4) ~~The percentage of total consumption that is used for the machine, water heating and dryer varies with efficiency. Percentages were developed using the above parameters and using the U.S. Department of Energy's Life Cycle Cost and Payback Period tool, available at: [http://www1.eere.energy.gov/buildings/appliance\\_standards/residential/clothes\\_washers\\_sup\\_port\\_stakeholder\\_negotiations.html](http://www1.eere.energy.gov/buildings/appliance_standards/residential/clothes_washers_sup_port_stakeholder_negotiations.html)~~
- 5) ~~Calculated using "Frequency of clothes washer use" and "Frequency of dryer use" data for the Mid-Atlantic region from U.S. Department of Energy, 2015 Residential Energy Consumption Survey (2015).  
<https://www.eia.gov/consumption/residential/data/2015/index.php?view=microdata>~~
- 6) ~~Metered data from Navigant Consulting "EmPOWER Maryland Draft Final Evaluation Report Evaluation Year 4 (June 1, 2012–May 31, 2013) Appliance Rebate Program." March 21, 2014, p. 36. Same value as used in and 2018 Mid-Atlantic TRM V 8.0. 1.04 hours/cycle derived from 254 cycles/yr and 265 hours/yr run time.~~
- 1) ~~Value from Clothes Washer Measure, Mid-Atlantic TRM 2014. Metered data from Navigant Consulting "EmPOWER Maryland Draft Final Evaluation Report Evaluation Year 4 (June 1, 2012 – May 31, 2013) Appliance Rebate Program." March 21, 2014, p. 36 California Electronic Technical Reference Manual. "Refrigerator or Freezer, Residential". Accessed December 2023. Weblink~~
- 2) ~~Based on a Cadmus survey of 510 PPL participants in PY8.~~
- 3) ~~Keeling, J., Bruchs, D. (2017). "Chapter 7: Refrigerator Recycling Evaluation Protocol. The Uniform Methods Project: Methods for Determining Energy-Efficiency Savings for Specific Measures". Section 4.4. National Renewable Energy Laboratory. Weblink~~
- 4) ~~Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink~~
- 5) ~~Greenblatt, J., Hopkins, A., Letschert, V., and Blasnik, M. (2012, April). "Energy use of US residential refrigerators and freezers: function derivation based on household and climate characteristics". Lawrence Berkeley National Lab. Weblink~~
- 6) ~~U.S. Department of Energy Compliance Certification Database. Accessed October 2021. Weblink~~
- 7) ~~ENERGY STAR-certified refrigerators. Accessed November 2021. Weblink~~
- 8) ~~ENERGY STAR-certified freezers. Accessed November 2011. Weblink~~

## 2.4.5 ENERGY STAR COOLERS

~~7)1)~~

- 8) ~~U.S. Department of Energy. 10 CFR Parts 429 and 430. Energy Conservation Program: Energy Conservation Standards for Residential Clothes Washers. Direct Final Rule. [https://www.ecfr.gov/cgi-bin/text-id.x?SID=86e70cbc87e5af18caca2e5c205bd107&mc=true&node=se10.3.430\\_132&rgn=div8](https://www.ecfr.gov/cgi-bin/text-id.x?SID=86e70cbc87e5af18caca2e5c205bd107&mc=true&node=se10.3.430_132&rgn=div8)~~

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### 2.4.5 ENERGY STAR CLOTHES DRYERS

Target Sector	Residential
Measure Unit	Clothes DryerCooler
Measure Life	1214 years <sup>Source 41</sup>
Vintage	Replace on Burnout
Vintage	Replace on Burnout

ENERGY STAR Clothes Dryers have a higher CEF (Combined Energy Factor) than standard dryers, and may incorporate a moisture sensor to reduce excessive drying of clothes and prolonged drying cycles.

#### ELIGIBILITY

~~THIS PROTOCOL DOCUMENTS THE ENERGY SAVINGS ATTRIBUTED TO PURCHASING AN ELECTRIC ENERGY STAR DRYER THAT MEETS OR EXCEEDS THE CEF<sub>ee</sub> REQUIREMENT IN TABLE 2-80 INSTEAD OF A STANDARD DRYER. IF A CUSTOMER SUBMITS A REBATE FOR A PRODUCT THAT HAS APPLIED FOR ENERGY STAR CERTIFICATION BUT HAS NOT YET BEEN CERTIFIED~~**ELIGIBILITY**

This measure is for the purchase and installation of a new cooler meeting ENERGY STAR or ENERGY STAR Most Efficient criteria. An ENERGY STAR cooler is 10% - 30% more efficient than the minimum federal government standard. Coolers are sometimes called beverage coolers, beverage refrigerators, wine chillers or wine fridges. They typically have glass fronts and operate at higher temperatures than refrigerators. There is currently no ENERGY STAR standard for refrigerator or freezer combination coolers.

#### ALGORITHMS

~~To determine resource savings, the per-unit estimates in the algorithms will be counted~~multiplied by the number of coolers. The number of coolers will be determined using market assessments and market tracking.

If the volume and configuration of a cooler is known, the baseline model's annual energy consumption (kWh<sub>base</sub>) may be determined using Table 2-98.

The efficient model's annual energy consumption (kWh<sub>ee</sub>) may be determined using manufacturers' test data for that product contingent upon its eventual certification as an the given model. Where test data is not available the algorithms in Table 2-98 for "ENERGY STAR measure. If at any point the product is rejected by maximum energy usage in kWh/year" may be used to determine the efficient energy consumption for a conservative savings estimate.

**ENERGY STAR**, the product is then ineligible for the program and savings will not be counted.<sup>64</sup> The target sector is residential. **Cooler**,

#### ALGORITHMS

<sup>64</sup>The Pennsylvania SWE and PUC TUS staff added this condition relating to certification that has been applied for but not yet received at the request of several of the Pennsylvania EDCs. EDCs will be responsible for tracking whether certification is granted.

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The energy savings are obtained through the following formulas:

$$\Delta kWh/yr = \left( \frac{1}{CEF_{base}} - \frac{1}{CEF_{ee}} \right) \times Load_{avg} \times Cycles_{wash} \times \%_{dry_{wash}}$$

$$\Delta kW_{peak} = \left( \frac{\frac{1}{CEF_{base}}}{Time_{base}} - \frac{\frac{1}{CEF_{ee}}}{Time_{ee}} \right) \times Load_{avg} \times CF$$

$$\Delta kWh = kWh_{base} - kWh_{ee}$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDF_w$$

**DEFINITION OF TERMS**

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Table 2-97: Terms, Values, and References for ENERGY STAR Refrigerators

Term	Unit	Value	Source
<u>kWh<sub>base</sub></u> , Annual energy consumption of baseline unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-99	EDC Data Gathering, 2
<u>kWh<sub>ee</sub></u> , Annual energy consumption of ENERGY STAR qualified unit	<i>kWh/yr</i>	EDC Data Gathering Default = Table 2-99	EDC Data Gathering, 3
<u>ETDF<sub>s</sub></u> , Summer peak Energy to Demand Factor	<i>kW/kWh</i>	0.0001354	4
<u>ETDF<sub>w</sub></u> , Winter peak Energy to Demand Factor	<i>kW/kWh</i>	0.0001014	4

Cooler energy consumption is characterized by volume, whether there are refrigerator or freezer compartments, and configuration (built-in, ice-maker). If this information is known, annual energy consumption (kWh<sub>base</sub>) of the “Federal Standard” may be determined using Table 2-98. The efficient model’s annual energy consumption (kWh<sub>ee</sub>) may be determined using manufacturer’s test data for the given model. 84: Terms, Values, and References for ENERGY STAR Clothes Dryers

Term	Unit	Values	Source
<u>Cycles<sub>wash</sub></u> , Number of washing machine cycles per year	<i>cycles/yr</i>	254 cycles/year	4
<u>Load<sub>avg</sub></u> , Weight of average dryer load, in pounds per load	<i>lbs/load</i>	Standard: 8.45 lbs/load Compact: 3.00 lbs/load	2
<u>%<sub>dry<sub>wash</sub></sub></u> , Percentage of homes with a dryer that use the dryer for every load	%	96% Or EDC data-gathering	4
<u>CEF<sub>base</sub></u> , Combined Energy Factor of baseline dryer, in lbs/kWh	<i>lbs/kWh</i>	Table 2-80 or EDC Data-Gathering	3
<u>CEF<sub>ee</sub></u> , Combined Energy Factor of ENERGY STAR dryer, in lbs/kWh	<i>lbs/kWh</i>	Table 2-80 or EDC Data-Gathering	2

$Time_{base}$ , Duration of baseline dryer drying cycle	Hours/cycle	EDC Data-Gathering Default = 1.0	Assumption
$Time_{ee}$ , Duration of efficient dryer drying cycle	Hours/cycle	EDC Data-Gathering Default = 1.0	Assumption
$CF$ , Coincidence Factor	Proportion	0.029	Based on CF assumption for Clothes Washers

Where test data is not available, the algorithm in Table 2-98 for “ENERGY STAR Maximum Energy Usage in kWh/year” may be used to determine efficient energy consumption for a conservative savings estimate.

The term “AV” in the equations refers to “Adjusted Volume” in ft<sup>3</sup>. For cooler-freezers, Categories beginning with C-9):

$$AV = Cooler Volume + Fresh Volume + 1.76 \times Freezer Volume$$

For all other categories:

$$AV = Cooler Volume + Fresh Volume$$

**Table 2-98: Combined Energy Factor for Federal Minimum Standard and ENERGY STAR DryersCoolers Maximum Annual Energy Consumption for Known Configuration and Volume<sup>62</sup>**

Product Type	$CEF_{base}$ (lbs/kWh)	$CEF_{ee}$ (lbs/kWh)
Vented Electric, Standard (4.4 ft <sup>3</sup> or greater capacity)	3.73	3.93
Vented Electric, Compact (120V) (less than 4.4 ft <sup>3</sup> capacity)	3.64	3.80
Vented Electric, Compact (240V) (less than 4.4 ft <sup>3</sup> capacity)	3.27	3.45

Cooler Configuration Class	Federal Standard Maximum Usage in kWh/yr	ENERGY STAR Maximum Energy Usage in kWh/yr
<b>Standard: 7.75 cubic feet or greater</b>		
2. Built-in	$7.88 \times AV + 155.8$	$5.52 \times AV + 109.1$
4. Freestanding	$7.88 \times AV + 155.8$	$7.09 \times AV + 140.2$
<b>Compact: less than 7.75 cubic feet</b>		
1. Built-in compact	$7.88 \times AV + 155.8$	$5.52 \times AV + 109.1$
3. Freestanding compact	$7.88 \times AV + 155.8$	$6.30 \times AV + 124.6$

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<sup>62</sup> Numbering convention (1, C-3A, etc.) of Federal standard and ENERGY STAR specifications included for clear reference to the standards as well as for correspondence to entries in the default savings table.

**DEFAULT SAVINGS**

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**Table 2-99: Default Energy Savings and Demand Reductions for ENERGY STAR Clothes Dryers**

Product Type	Energy Savings (kWh/yr)	Demand Reduction (kW)
Vented Electric, Standard (4.4 ft <sup>3</sup> or greater capacity)	27.8	0.0033
Vented Electric, Compact (120V) (less than 4.4 ft <sup>3</sup> capacity)	40.0	0.0042
Vented Electric, Compact (240V) (less than 4.4 ft <sup>3</sup> capacity)	41.5	0.0044

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**VALUES**

**EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of installation coupled with calculation of energy and demand savings using above algorithms.

**SOURCES**

1) Calculated using “Frequency of clothes washer use” and “Frequency of dryer use” data for the Mid-Atlantic region from ENERGY STAR Coolers<sup>63</sup> U.S. Department of Energy, 2015 Residential Energy Consumption Survey (2015). <https://www.eia.gov/consumption/residential/data/2015/index.php?view=microdata>

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Cooler Configuration Class	Assumed Adjusted Volume (cubic feet) <small>Source 5.6</small>	Conventional Unit Energy Usage in kWh/yr	ENERGY STAR Energy Usage in kWh/yr	$\Delta$ kWh/yr <sup>64</sup>	$\Delta$ kW <sub>summer peak</sub>	$\Delta$ kW <sub>winter peak</sub>
<b>Standard: 7.75 cubic feet or greater</b>						
2. Built-in	11.26	244.5	171.3	73	0.0099	0.0074
4. Freestanding	14.63	271.1	243.9	27	0.0037	0.0027
<b>Compact: less than 7.75 cubic feet</b>						
1. Built-in compact	3.97	187.1	131	56	0.0076	0.0057
3. Freestanding compact	3.82	185.9	148.7	37	0.0050	0.0038

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**EVALUATION PROTOCOLS**

- For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. Energy Star, “Clothes Dryers Key Product Criteria.” ENERGY STAR Specification for Clothes Dryers Version 1.0, Effective January 1, 2015. <https://www.energystar.gov/products/appliances/clothes-dryers/key-product-criteria>
- Federal Code of Regulations 10 CFR 430. <https://www.gpo.gov/fdsys/pkg/CFR-2017-title10-vol3/pdf/CFR-2017-title10-vol3-sec430-32.pdf>

<sup>63</sup> Lettering convention (1A, 2, etc) of Federal standard and ENERGY STAR specifications included for clear reference to the standards as well as for correspondence to entries in the default savings table.

<sup>64</sup> kWh/yr savings may differ from Conventional Usage – ENERGY STAR Usage by 1 kWh/yr due to rounding.



~~3) California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020,  
<http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>;  
Accessed December 2018.~~

### 2.4.6 HEAT PUMP CLOTHES DRYERS

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Per Clothes Dryer
<b>Measure Life</b>	12 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout, New Construction

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Heat pump clothes dryers are more energy-efficient than standard dryers. A conventional dryer heats air, passes it through the clothing drum, and exhausts the hot air. A heat pump dryer works by circulating hot air through the clothing drum, extracting moisture from the clothing that becomes condensation after passing over an evaporator coil, then reheating the air before it passes through the drum again. The heat pump dryer saves energy by recirculating the warm air, requiring less heat to reach the desired temperature, and because the process requires a lower air temperature overall to dry clothes.

#### ELIGIBILITY

This protocol documents the energy savings attributed to installing a heat pump clothes dryer that meets or exceeds the default  $CEF_{ee}$  requirements in Table 2-82. The target sector is residential.

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#### ALGORITHMS

The following algorithms shall be used to calculate the annual energy savings and coincident peak demand savings for this measure:

$$\Delta kWh = \left( \frac{1}{CEF_{base}} - \frac{1}{CEF_{ee}} \right) \times Load_{avg} \times Cycles_{wash} \times \% \frac{dry}{wash}$$

$$\Delta kW_{peak} = \left( \frac{\frac{1}{CEF_{base}}}{Time_{base}} - \frac{\frac{1}{CEF_{ee}}}{Time_{ee}} \right) \times Load_{avg} \times CF$$

#### DEFINITION OF TERMS

Table 2-84: Terms, Values, and References for Heat Pump Clothes Dryers

Term	Unit	Values	Source
$\Delta kWh$ , Annual Energy Savings	kWh/yr	Table 2-83	-
$\Delta kW_{peak}$ , Peak Demand Savings	kW	Table 2-83	-
$Cycles_{wash}$ , Number of washing machine cycles per year	cycles/yr	EDC Data Gathering Default = 254	2
$Load_{avg}$ , Weight of average dryer load	lbs/cycle	Standard = 8.45 Compact = 3.00	3
$\% \frac{dry}{wash}$ , Percentage of washed loads that get dried	%	Default = 96%	2
$CEF_{base}$ , Combined Energy Factor of baseline dryer, in lbs/kWh	lbs/kWh	EDC Data Gathering See $CEF_{base}$ of Table 2-80 in Sec. 0	4

$CEF_{hp}$ , Combined Energy Factor of heat pump dryer, in lbs/kWh	lbs/kWh	EDC Data Gathering Default: ≥4.4 ft <sup>3</sup> (std) = 4.50 <4.4 ft <sup>3</sup> (empct) = 4.74	5
$Time_{base}$ , Duration of baseline dryer drying cycle	Hours/cycle	EDC Data Gathering Default = 1.0	Assumption
$Time_{ee}$ , Duration of efficient dryer drying cycle	Hours/cycle	EDC Data Gathering Heat Pump = 1.2	6
CF, Coincidence Factor	None	EDC Data Gathering Default = 0.029	Based on CF assumption for Clothes Washers

Default Savings

**Table 2-85: Default Savings for Heat Pump Clothes Dryers**

Heat Pump Type	Energy Savings (kWh/yr)	Peak Demand Reduction (kW)
4.4 ft <sup>3</sup> or greater capacity	93.4	0.0203
Less than 4.4 ft <sup>3</sup> capacity, 120-V	46.8	0.0087
Less than 4.4 ft <sup>3</sup> capacity, 240-V	67.6	0.0112

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020.  
<http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>
- Calculated using “Frequency of clothes washer use” and “Frequency of dryer use” data for the Mid-Atlantic region from U.S. Department of Energy. 2015 Residential Energy Consumption Survey (2015).  
<https://www.eia.gov/consumption/residential/data/2015/index.php?view=microdata>
- Energy Star. “Clothes Dryers Key Product Criteria.” ENERGY STAR Specification for Clothes Dryers Version 1.0, Effective January 1, 2015.  
[https://www.energystar.gov/products/appliances/clothes\\_dryers/key\\_product\\_criteria](https://www.energystar.gov/products/appliances/clothes_dryers/key_product_criteria)
- U.S. Code of Federal Regulations, Part 430, Subpart C, *Energy and Water Conservation Standards*. <http://www.ecfr.gov/cgi-bin/text-idx?rgn=div8&node=10:3.0.1.4.18.3.9.2>
- ENERGY STAR, *Certified Clothes Dryers*.  
<https://www.energystar.gov/productfinder/product/certified-clothes-dryers/results>  
 (Examined the “ventless” dryers and removed dryers that were condensing and not heat pump. Then took the average CEF of the two different capacity bins.)

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- 6) ~~CLASP, SEDI and Ecova, Analysis of Potential Energy Savings from Heat Pump Clothes Dryers in North America, March 2013. [http://www.ecosresearch.com/wp-content/uploads/2015/12/2013\\_Analysis-of-Potential-Energy-Savings-from-Heat-Pump-Clothes-Dryers-in-North-America.pdf](http://www.ecosresearch.com/wp-content/uploads/2015/12/2013_Analysis-of-Potential-Energy-Savings-from-Heat-Pump-Clothes-Dryers-in-North-America.pdf)~~

#### **~~2.4.7 FUEL SWITCHING: ELECTRIC CLOTHES DRYER TO GAS CLOTHES DRYER~~**

- 1) California Electronic Technical Reference Manual. “Refrigerator or Freezer, Residential”. Accessed December 2023. Weblink
- 2) 10 CFR 430.32(aa) Weblink
- 3) U.S. EPA. (2014). ENERGY STAR Program Requirements Product Specifications for Consumer Refrigeration Products Version 5.1. Weblink
- 4) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink
- 5) DOE Compliance Certificate Database. Accessed July 2022. Weblink
- 6) ENERGY STAR-certified refrigerators. Accessed July 2022. Weblink

### 2.4.6 COOLER RECYCLING WITH AND WITHOUT REPLACEMENT

<b>Target Sector</b>	Residential Establishments
<b>Measure UnitLife</b>	Fuel Switch: Electric Clothes Dryer to Gas Clothes Dryer <u>Without Replacement:</u> <sup>Source 1</sup> 5 years <b>With Replacement:</b> 9 years
<b>Measure LifeVintage</b>	12 years <sup>Source 1</sup> Early Retirement, Early Replacement

#### ELIGIBILITY

<b>Vintage</b>	<b>Replace on Burnout</b>
----------------	---------------------------

Coolers are sometimes called beverage coolers, beverage refrigerators, wine chillers or wine fridges. They typically have glass fronts and operate at higher temperatures than refrigerators. This protocol outlines the recycling of a cooler manufactured prior to October 2019.

Consumer refrigeration appliance recycling programs are designed to save energy through the removal of old-but-operable appliances from service. By offering free pickup, providing incentives, and disseminating information about the operating cost of old appliances, these programs are designed to encourage consumers to:

- Discontinue the use of secondary refrigeration equipment
- Relinquish units when they are replaced (rather than keeping the old appliance as a secondary unit)
- Prevent the continued use of old refrigeration equipment in another household through a direct transfer (giving it away or selling it) or indirect transfer (resale on the used appliance market).

Commonly implemented by third-party contractors (who collect and decommission participating appliances), these programs generate energy savings associated to purchasing an through the retirement of inefficient appliances. The decommissioning process captures environmentally harmful refrigerants and foam and enables the recycling of the plastic, metal, and wiring components.

This protocol applies to both residential and non-residential sectors since consumer-grade cooler usage and energy consumption are assumed to be independent of customer rate class.<sup>65</sup>

This measure may be combined with ENERGY STAR gas clothes dryer to replace an electric dryer. The measure characterization and Coolers if the cooler is replaced with qualifying equipment.

#### ALGORITHMS

The total annual energy savings estimates are based (kWh/yr) achieved from recycling old-but-operable coolers are calculated using the following general algorithms:

#### Energy Savings

<sup>65</sup> For example, non-residential rate class usage cases include residential dwellings that are master-metered, usage in offices or any other applications that involve typical cooler usage.

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$$\Delta kWh = N \times (UEC - kWh_{ee}) \times PART_{USE}$$

Note that lifetime savings will be calculated with this same general algorithm but with an adjusted measure life.

### Unit Energy Consumption

Coolers were not federally regulated until October 2019. However, California Energy Commission Title 20 regulations for this product class were introduced in 2002,<sup>Source 3</sup> and remained unchanged and in effect until they were superseded by the federal standards.

Annual energy consumption (UEC) of the decommissioned cooler may be determined using manufacturers' test data for the given model. If test data are not available, annual unit energy consumption is equal to the derated maximum Title 20 annual energy consumption ( $\eta \times kWh_{recycled}$ ).<sup>66</sup> The algorithms in Table 2-101 may be used to determine  $kWh_{recycled}$ .

Note that if the unit is being recycled without replacement, the  $kWh_{ee}$  variable takes on the value of zero. The  $kWh_{ee}$  variable only applies to direct install replacement of the recycled cooler.

### Adjusted Volume (AV)

The adjusted volume equations below account for the greater load of freezer compartments compared to compartments for fresh food. For Category 1 and 1A "All-refrigerators", i.e; equipment with not more than 0.5 ft<sup>3</sup> of freezer volume:

$$AV = Cooler Volume + Fresh Volume + Freezer Volume$$

For all other categories:

$$AV = Cooler Volume + Fresh Volume + 1.76 \times Freezer Volume$$

### Part-Use Factor

When calculating default per unit kWh savings for a removed cooler, it is necessary to calculate and apply a "Part-Use" factor. "Part-Use" is an appliance recycling-specific adjustment factor used to convert the UEC into an average usage-per-person-and-per-unit deemed savings value. The UEC itself is not equal to the default savings value, because not all coolers would have operated year-round had they not been decommissioned through the program.

EDCs may use either a cooler-specific part-use, or that calculated for refrigerators. In Program Year 8, the Commission determined that the average number of people per household. Therefore, this is a deemed measure with identical savings applied to all installation instances, applicable across all housing types. removed refrigerator was plugged in and used 72.8% of the year.<sup>Source 5</sup> These are the default values for the part-use factor. EDCs may elect to calculate an EDC-specific part-use factor for a specific program year. In the event an EDC desires to calculate an EDC-specific part-use factor, EDCs should use the methodology described in section 4.4 of the DOE, Uniform Methods Project protocol.<sup>Source 4</sup>

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## ELIGIBILITY

This measure is targeted to residential customers that purchase an ENERGY STAR gas clothes dryer rather than an electric dryer.

## ALGORITHMS

$$DkWh = kWh_{base} - kWh_{gas} = 577 - 30 = 547$$

<sup>66</sup> This is results in a conservative savings estimate since equipment sold outside of California could exceed Title 20 levels.

$$DMMB_{tt} = -1.99$$

$$DkW_{peak} = \frac{\Delta kWh}{Cycles_{wash} \times \%_{wash} \times Time_{cycle}} \times CF = 0.066$$

**Peak Demand Savings**

Use the below algorithm to calculate the peak demand savings. Multiply the annual kWh savings by an Energy to Demand Factor (ETDF), which is supplied below.

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDF_w$$

**DEFINITION OF TERMS**

**Table 2-100: Terms, Values, and References for Fuel-Switching: Electric Clothes Dryer to Gas Clothes Dryer, Refrigerator and Freezer Recycling**

Term	Unit	Values	Source
<u>N</u> , The number of refrigerators recycled through the program	None	EDC Data Gathering	EDC Data Gathering
<u>UEC</u> , Annual energy consumption of the cooler being recycled	kWh/yr	EDC Data Gathering, or $\eta \times kWh_{recycled}$	EDC Data Gathering, 2, 3
<u><math>\eta</math></u> , Average fraction of rated usage + Title 20 Annual Energy Consumption. This is a measure of how much more efficient equipment on the market was than what Title 20 permitted.	%	89%	2
<u><math>kWh_{recycled}</math></u> , Maximum annual energy consumption of California Title 20 standard for the recycled unit	kWh/yr	Table 2-101	3
<u><math>kWh_{ee}</math></u> , Maximum annual energy consumption of ENERGY STAR qualified unit	kWh/yr	EDC Data Gathering Table 2-98 Default: Table 2-99	EDC Data Gathering, 7
<u>PART USE</u> , The portion of the year the average cooler would likely have operated if not recycled through the program	%	EDC Data Gathering According to Section 4.4 of UMP Protocol Default: Refrigerator= 72.8%	EDC Data Gathering, 5
<u>ETDF<sub>s</sub></u> , Summer peak Energy to Demand Factor	$\frac{kW}{kWh}$	0.0001354	6
<u>ETDF<sub>w</sub></u> , Winter peak Energy to Demand Factor	$\frac{kW}{kWh}$	0.0001014	6
<u>AV</u> , Adjusted Volume/calculated as described above	ft <sup>3</sup>	EDC Data Gathering Default: Recycled Compact=4.3 Recycled Standard=14.6	EDC Data Gathering, 2

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Cooler energy consumption is characterized by volume, whether there are refrigerator or freezer compartments, and configuration (built-in, ice-maker). Annual energy consumption may be



determined using manufacturer's test data for the given model, or if unavailable and the configuration details are known, using the algorithms in Table 2-101. Otherwise, the default values in Table 2-101 may be used.

**Table 2-101: Pre-2019 California Title 20 Maximum Annual Energy Consumption<sup>67</sup>**

<u>Cooler Configuration</u>	<u>kWh<sub>recycled</sub></u>	<u>Default</u>
<b>Standard: 7.75 cubic feet or greater</b>		
<u>2. Built-in</u>	<u><math>13.7 \times AV + 267</math></u>	<u>467</u>
<u>4. Freestanding</u>	<u><math>13.7 \times AV + 267</math></u>	<u>467</u>
<u>C-3A. Cooler with all-refrigerator - automatic defrost</u>	<u><math>17.4 \times AV + 344</math></u>	<u>598</u>
<u>C-3A-BI. Built-in cooler with all-refrigerator - automatic defrost</u>	<u><math>17.4 \times AV + 344</math></u>	<u>598</u>
<u>C-9. Cooler with upright freezers with automatic defrost without an automatic icemaker</u>	<u><math>17.4 \times AV + 344</math></u>	<u>598</u>
<u>C-9-BI. Built-in cooler with upright freezer with automatic defrost without an automatic icemaker</u>	<u><math>17.4 \times AV + 344</math></u>	<u>598</u>
<u>C-9I. Cooler with upright freezer with automatic defrost with an automatic icemaker</u>	<u><math>17.4 \times AV + 344</math></u>	<u>598</u>
<u>C-9I-BI. Built-in cooler with upright freezer with automatic defrost with an automatic icemaker</u>	<u><math>17.4 \times AV + 344</math></u>	<u>598</u>
<b>Compact: less than 7.75 cubic feet</b>		
<u>1. Built-in compact</u>	<u><math>13.7 \times AV + 267</math></u>	<u>326</u>
<u>3. Freestanding compact</u>	<u><math>13.7 \times AV + 267</math></u>	<u>326</u>
<u>C-13A. Compact cooler with all-refrigerator - automatic defrost</u>	<u><math>17.4 \times AV + 344</math></u>	<u>419</u>
<u>C-13A-BI. Built-in compact cooler with all-refrigerator - automatic defrost</u>	<u><math>17.4 \times AV + 344</math></u>	<u>419</u>
<b>Unknown Configuration</b>		
<u>Standard</u>	<u>=</u>	<u>467</u>
<u>Compact</u>	<u>=</u>	<u>326</u>
<u>Unknown</u>	<u>=</u>	<u>353</u>

**MEASURE LIFE**

Since coolers function similarly to refrigerators, the California Electronic Technical Reference Manual refrigerator EUL is used as a proxy. The measure life for refrigerators WITHOUT replacement is 5 years, representing 1/3 of the EUL of a new refrigerator and by extension cooler. The adjusted measure life of coolers recycled WITH replacement is 5 years for federal units and 9 years for ENERGY STAR units.

<sup>67</sup> Lettering convention (1, 1A, etc) of Federal standard and ENERGY STAR specifications included for clear reference to the standards as well as for correspondence to entries in the default savings table.

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**Adjusted Measure Life with Replacement Rationale:**

Consumer refrigeration appliance recycling with replacement programs commonly calculate savings over two periods, the RUL of the existing unit, and the remainder of the EUL of the efficient unit beyond the RUL of the existing unit. For the first period of savings (the RUL of the existing unit), the energy savings are equal to the savings difference between the recycled unit and the replacement unit: the RUL can be assumed to be 1/3 of the measure EUL of an ENERGY STAR cooler. For the second period of savings (the remaining EUL of the replacement unit), the energy savings are equal to the difference between a Federal Standard unit and the replacement unit.

The EUL of a new ENERGY STAR refrigerator or cooler is 14 years. However, a study of a low-income refrigerator replacement program for SDG&E (2006) found that among the program's target population, refrigerators are likely to be replaced less frequently than among average customers. As a result, the report updating the California DEER database recommended an EUL of 18 years for such programs.<sup>Source 8</sup>

To simplify the calculation of savings and remove the need to calculate different savings for each population, adjusted measure life values for the state can be used with the savings difference between the recycled baseline unit and the replacement unit over the adjusted measure life. These are provided in Table 2-102 below. The duration of each period (5.2 and 10.4) are based on weighting the aforementioned EULs of 14 and 18 years by the proportion of Pennsylvania's low-income population (40% at or below 150% of federal poverty level).<sup>Source 10</sup>

**Table 2-102: Adjusted Measure Life**

Replacement	RUL Savings	+ EUL Remainder Savings	= Total Savings	Equivalent Years (Total + RUL)
ENERGY STAR	$\frac{1}{3} \times 5.2 \times (314-148)$	$\frac{2}{3} \times 10.4 \times (203-148)$	1.437	9

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- 1) California Electronic Technical Reference Manual. "Refrigerator Recycling". Accessed December 2023. Weblink
- 2) SWE analysis of 143 wine chiller models in historic records (dated 2002–2013) of the California Energy Commission's Modernized Appliance Efficiency Database System, including 116 compact models and 27 standard models. Weblink
- 3) California Energy Commission 2015 Appliance Efficiency Regulations, Effective 2002. Accessed 7/7/2022. Weblink
- 4) Keeling, J., Bruchs, D. (2017). "Chapter 7: Refrigerator Recycling Evaluation Protocol. The Uniform Methods Project: Methods for Determining Energy-Efficiency Savings for Specific Measures". Section 4.4. National Renewable Energy Laboratory. Weblink
- 5) Based on a Cadmus survey of 510 PPL participants in PY8.
- 6) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

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7) [10 CFR 430.32\(aa\) Weblink](#)

8) [Seiden, K., Bruchs, D., Peters, J., Moran, D., Burdick, M. \(2006, July\). "2004–2005 Final Report: A Measurement and Evaluation Study of the 2004-2005 Limited Income Refrigerator Replacement & Lighting Program". Weblink](#)

9) [SWE analysis of 591 cooler models from EPA and DOE records, including 482 compact models \(82% class 3, 9% class C-13A, 6% class 1\) and 109 standard models \(80% class 4, 17% class 2\).](#)

a. [DOE Compliance Certificate Database. Accessed July 2022. Weblink](#)

b. [ENERGY STAR-certified refrigerators. Accessed July 2022. Weblink](#)

10) [U.S. Census Bureau, 2017-2021 American Community Survey 5-Year Estimates. Weblink](#)

### 2.4.7 RESIDENTIAL INDUCTION COOKTOP

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Induction Cooktop
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit, Replace on Burnout, or New Construction

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#### ELIGIBILITY

Electric induction cooktops are either a freestanding cooktop that heats cooking vessels using electrical induction or a range with an electric resistance oven and an electric induction cooktop. Electric induction cooktops save energy by heating the cookware directly as opposed to the surface of the range as seen in traditional electric resistance cooktops.

Electric induction cooktops may replace electric ovens with electric resistance cooktops or freestanding electric resistance cooktops.

#### ALGORITHMS

Total savings are calculated based on the increased cooking efficiency of an electric induction cooktop over an existing electric resistance cooktop. Cooking efficiency is defined as the ratio of energy absorbed by the object being heated (food, water, etc.) and the energy consumed by the appliance.

$$\Delta kWh = (AEC_{base} - AEC_{ee}) \times \%_{elec}$$

$$AEC_{base} = AEC_{ee} \times \left( \frac{Eff_{ee}}{Eff_{base}} \right)$$

$$\Delta kWh_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kWh_{winter\ peak} = \Delta kWh \times ETDF_w$$

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#### DEFINITION OF TERMS

Table 2-103: Terms, Values, and References for Electric Induction Cooktops

Term	Unit	Value	Sources
<u>AEC<sub>base</sub></u> , Annual Energy Consumption of a baseline electric cooktop	$\frac{kWh}{yr}$	<u>EDC Data Gathering of Nameplate data</u>	<u>EDC Data Gathering</u>
		Default = 209	Calculated
<u>AEC<sub>ee</sub></u> , Annual Energy Consumption of efficient induction cooktop	$\frac{kWh}{yr}$	<u>EDC Data Gathering of Nameplate Data</u>	<u>EDC Data Gathering</u>
		Default = 189	2
<u>Eff<sub>ee</sub></u> , Efficiency of electric induction cooktop	%	<u>EDC Data Gathering of Nameplate data</u>	<u>EDC Data Gathering</u>
		Default = 85%	3
<u>Eff<sub>base</sub></u> , Efficiency of baseline electric resistance cooktop	%	<u>EDC Data Gathering of Nameplate data</u>	<u>EDC Data Gathering</u>
		Default = 77%	3

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Term	Unit	Value	Sources
$ETDF_{s, \text{summer peak energy to demand factor}}$	$\frac{kW}{kWh}$	EDC Data Gathering	EDC Data Gathering
		Default = 0.0002153	4
$ETDF_{w, \text{winter peak energy to demand factor}}$	$\frac{kW}{kWh}$	EDC Data Gathering	EDC Data Gathering
		Default = 0.0002237	4
$\%_{elec, \text{electric cooktop penetration}}$	$\%$	EDC Data Gathering	EDC Data Gathering
		61%	5

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Default $kWh_{base}$ , Baseline annual electricity consumption of electric dryer, deemed	$\frac{kWh}{yr}$	577	2,3
$kWh_{gas}$ , Annual electricity consumption of gas dryer, deemed	$\frac{kWh}{yr}$	30	4
$DMMBTU$ , Weighted average gas fuel savings (negative indicates increase in consumption)	$MMBTU$	-4.99	5
$Cycles_{wash}$ , Number of washing machine cycles per year	$cycles/yr$	251	6
$\%_{dry, wash}$ , Percentage of homes with a dryer that use the dryer every time clothes are washed	$\%$	96%	6
$Time_{cycle}$ , Duration of average drying cycle in hours	hours	1	Assumption
CF, Coincidence Factor	Proportion	0.029	Based on CF assumption for Clothes Washers

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## DEFAULT SAVINGS

### SAVINGS ESTIMATES

Default savings for this measure are fully deemed and may be claimed using the algorithms above and the deemed variable inputs based on the default energy consumption and efficiencies for the efficient induction and baseline electric resistance measure.

$$\begin{aligned} \Delta kWh_{default} &= (AEC_{base, default} - AEC_{ee, default}) \times \%_{elec} \\ &= (209 - 189) \times 61\% \\ &= 12.24 kWh = 547 kWh/yr \\ \Delta kW &= 0.066 \end{aligned}$$

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### EVALUATION PROTOCOLS

The appropriate evaluation protocol is to verify installation and proper selection of deemed values.

### SOURCES

$$AEC_{base, default} = AEC_{ee, default} \times \left( \frac{Eff_{ee, default}}{Eff_{base, default}} \right)$$

$$\begin{aligned} &= 189 \times \left(\frac{85}{77}\right) \\ &= 209 \text{ kWh/yr} \end{aligned}$$

$$AEC_{ee, default} = 189 \text{ kWh/yr}$$

$$\begin{aligned} \Delta kW_{summer peak} &= \Delta kWh_{default} \times ETDf_s \\ &= 12.2 \times 0.0002153 \\ &= 0.0026 \text{ kW} \end{aligned}$$

$$\begin{aligned} \Delta kW_{winter peak} &= \Delta kWh_{default} \times ETDf_w \\ &= 12.2 \times 0.0002237 \\ &= 0.0027 \text{ kW} \end{aligned}$$

### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. California For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. Evaluation contractors may choose to propose independent assessments of the ESF factors to the SWE in their EM&V plans. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

- 14) Federal Register 10 CFR Parts 429 and 430. Vol. 81, No. 171. (2016, September). Measure life capped at 15 years per PA Act 129. Weblink
- 15) Assigned value for ENERGY STAR-certified Residential Induction Cooktops. QPL accessed 11/21/2023. Weblink
- 16) Livchak, D., Hedrick R., and Young, R. (2019, July). "Residential Cooktop Performance and Energy Comparison Study". Frontier Energy Report # 501318071-R0. Weblink
- 17) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink
- 1) NMR Group for the Pennsylvania Public Utilities Utility Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.
- 2)18) . (2024, March). 2023 Pennsylvania Statewide average for all housing types from Pennsylvania Act 129-2018 Act 129 Residential Baseline Study, 2018,<sup>68</sup> [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Page 145, Table 130. Weblink

<sup>68</sup> Statewide average of 3.12 EF for electric dryers, comparable to 3.77 CEF; q.v. the federal standard of 3.73 CEF at Table 73 in the ENERGY STAR Clothes Dryers section.

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## 2.4.8 ENERGY STAR CLOTHES WASHERS

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Clothes Washer
<b>Measure Life</b>	14 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout

This measure is for the purchase and installation of an ENERGY STAR clothes washer. ENERGY STAR clothes washers use less energy and hot water than non-qualified models.

### ELIGIBILITY

This protocol documents the energy savings attributed to purchasing an ENERGY STAR clothes washer that exceeds federal minimum efficiency standards.

### ALGORITHMS

The general form of the equation for the ENERGY STAR Clothes Washer measure savings algorithm is:

Total Savings \_\_\_\_\_ = Number of Clothes Washers × Savings per Clothes Washer

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of clothes washers.

Per unit energy and demand savings are given by the following algorithms:

$\Delta kWh = Cycles \times$

$$\left( \frac{CAPY}{IMEF_{base}} \times \left( CW_{base} + DHW_{base} \times \%_{ElecDHW} + Dryer_{base} \times \%_{ElecDryer} \times \%_{dry\ wash} \right) - \right. \\ \left. \left( \frac{CAPY}{IMEF_{ee}} \times \left( CW_{ee} + DHW_{ee} \times \%_{ElecDHW} + Dryer_{ee} \times \%_{ElecDryer} \times \%_{dry\ wash} \right) \right) \right)$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDF_w$$

Where IMEF is the integrated modified energy factor, which is the energy performance metric for clothes washers. IMEF is defined as:

*IMEF is the quotient of the cubic foot capacity of the clothes container, C, divided by the total clothes washer energy consumption per cycle, with such energy consumption expressed as the sum of the machine electrical energy consumption (M), the hot water energy consumption (E), the energy required for removal of the remaining moisture in the wash load (D), and the combined low-power mode energy consumption (L). The higher the value, the more efficient the clothes washer is.*<sup>Source 2</sup>

$$IMEF = \frac{C}{(M + E + D + L)}$$

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**DEFINITION OF TERMS**

**Table 2-104: Terms, Values, and References for ENERGY STAR Clothes Washers**

<u>Term</u>	<u>Unit</u>	<u>Value</u>	<u>Source</u>
<u>CAPY</u> , Clothes washer capacity	$ft^3$	<u>EDC Data Gathering</u> Default: <u>Table 2-105</u>	<u>EDC Data Gathering</u> , <u>2</u>
<u>IMEF<sub>base</sub></u> , Integrated Modified Energy Factor of baseline clothes washer	$\frac{ft^3}{(kWh/cycle)}$	<u>Table 2-105</u>	<u>7</u> , <u>10</u>
<u>IMEF<sub>ee</sub></u> , Integrated Modified Energy Factor of ENERGY STAR clothes washer	$\frac{ft^3}{(kWh/cycle)}$	<u>EDC Data Gathering</u> Default: <u>Table 2-105</u>	<u>EDC Data Gathering</u> , <u>3</u>
<u>Cycles</u> , Number of clothes washer cycles per year	$\frac{cycles}{yr}$	<u>178</u>	<u>6</u>
<u>CW<sub>base</sub></u> , % of total energy consumption for baseline clothes washer mechanical operation	%	<u>8.2%</u>	<u>5</u>
<u>CW<sub>ee</sub></u> , % of total energy consumption for ENERGY STAR clothes washer mechanical operation	%	<u>7.6%</u>	<u>5</u>
<u>DHW<sub>base</sub></u> , % of total energy consumption attributed to baseline clothes washer water heating	%	<u>10.8%</u>	<u>5</u>
<u>DHW<sub>ee</sub></u> , % of total energy consumption attributed to ENERGY STAR clothes washer water heating	%	<u>10.8%</u>	<u>5</u>
<u>%EtecDHW</u> , % of water heaters that are electric	%	<u>EDC Data Gathering</u> Default: <u>47%</u>	<u>EDC Data Gathering</u> , <u>4</u>
<u>Dryer<sub>base</sub></u> , % of total energy consumption for baseline clothes washer dryer operation	%	<u>81.0%</u>	<u>5</u>



<u>Term</u>	<u>Unit</u>	<u>Value</u>	<u>Source</u>
<u>Dryer<sub>ee</sub></u> , % of total energy consumption for ENERGY STAR clothes washer dryer operation	%	81.6%	5
<u>%<sub>ElecDryer</sub></u> , Percentage of dryers that are electric	%	EDC Data Gathering Default: 82%	EDC Data Gathering, 4
<u>%<sub>dry</sub></u> , Percentage of homes with a dryer that use the dryer every time clothes are washed	%	Default= 99% Or EDC data gathering	6
<u>ETDF<sub>s</sub></u> , Summer energy to Demand Factor	$\frac{kW}{kWh}$	0.0001475	8
<u>ETDF<sub>w</sub></u> , Winter energy to Demand Factor	$\frac{kW}{kWh}$	0.0001490	8

Federal standards for clothes washers through 2/29/28 are based on IMEF (ft<sup>3</sup>/kWh/cycle). Starting 3/1/28 the federal standards will be based on energy efficiency ratio (EER, lb/kWh/cycle).<sup>Source 9</sup>  
 Table 2-105 converts the 3/1/28 federal minimum EERs to IMEFs for use in the savings algorithm.

**Table 2-105: Federal Standards and ENERGY STAR Specifications for Clothes Washers through 2/29/28**

<u>Configuration<sup>69</sup></u>	<u>CAPY</u>	<u>IMEF<sub>base</sub></u> <u>through</u> <u>2/29/28</u>	<u>IMEF<sub>base</sub></u> <u>as of</u> <u>3/1/28</u>	<u>IMEF<sub>ee</sub></u>
Top-loading, > 2.5 ft <sup>3</sup>	5.0	1.57	2.06	2.06
Front-loading, 1.6 ft <sup>3</sup> ≤ 2.5 ft <sup>3</sup>	2.2	1.84	2.76	2.07
Front-loading, > 2.5 ft <sup>3</sup>	4.5	1.84	2.76	2.76

### **DEFAULT SAVINGS**

Table 2-106 displays default savings from clothes washers through 2/29/28. There are no default savings as of 3/1/28 when federal minimum efficiency standards meet or exceed ENERGY STAR Version 8.1 minimums. However, EDCs can still calculate savings using EDC-gathered data for ENERGY STAR clothes washers that exceed federal minimum efficiency standards.

**Table 2-106: Default Clothes Washer Savings through 2/29/28**

<u>Fuel Mix</u>	<u>Washer Type</u>	<u>ΔkWh</u>	<u>ΔkW<sub>summer peak</sub></u>	<u>ΔkW<sub>winter peak</sub></u>
Electric DHW/Electric Dryer	Top-loading, > 2.5 ft <sup>3</sup>	133.8	0.0197	0.0199
	Front-loading, 1.6 ft <sup>3</sup> ≤ 2.5 ft <sup>3</sup>	23.5	0.0035	0.0035
	Front-loading, > 2.5 ft <sup>3</sup>	144.0	0.0212	0.0214

<sup>69</sup> If configuration is front-loading and capacity is unknown, assume capacity > 2.5 ft<sup>3</sup>.

Electric DHW/Gas Dryer	Top-loading, > 2.5 ft3	28.2	0.0042	0.0042
	Front-loading, 1.6 ft3 ≤ 2.5 ft3	5.6	0.0008	0.0008
	Front-loading, > 2.5 ft3	29.3	0.0043	0.0044
Gas DHW/Electric Dryer	Top-loading, > 2.5 ft3	119.2	0.0176	0.0178
	Front-loading, 1.6 ft3 ≤ 2.5 ft3	20.9	0.0031	0.0031
	Front-loading, > 2.5 ft3	128.3	0.0189	0.0191
Gas DHW/Gas Dryer	Top-loading, > 2.5 ft3	13.6	0.0020	0.0020
	Front-loading, 1.6 ft3 ≤ 2.5 ft3	3.1	0.0005	0.0005
	Front-loading, > 2.5 ft3	13.6	0.0020	0.0020
Default (47% Electric DHW, 82% Electric Dryer)	Top-loading, > 2.5 ft3	107.1	0.0158	0.0159
	Front-loading, 1.6 ft3 ≤ 2.5 ft3	18.9	0.0028	0.0028
	Front-loading, > 2.5 ft3	115.0	0.0170	0.0171

## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

- 3) 2011-04 Technical Support Document: Energy Efficiency Program for Consumer Products and Commercial and Industrial Equipment. Residential Clothes Dryers and Room Air Conditioners, Chapter 7. Table 7.3.4: Electric Standard and Gas Clothes Dryer: Average Annual Energy Consumption Levels by Efficiency  
<https://www.regulations.gov/document?D=EERE-2007-BT-STD-0010-0053><sup>70</sup>
- 4) *Ibid.* Median annual electricity consumption of gas dryers
- 5) Negative gas fuel savings indicate increase in fuel consumption. Average annual consumption for ENERGY STAR qualified gas units as of 6/22/2015: 685.3kWh/yr. Scaling from 283 cycles/yr (national 2005 RECS) to 251×96%=241 cycles/yr (Mid-Atlantic 2015 RECS): 583.5 kWh/yr. Converting to MMBTU: 583.5×0.003412 = 1.99 MMBTU/yr.
- 1) DOE (2021). Residential Clothes Washers Life-Cycle Cost Analysis (LCC) Spreadsheets. Weblink
- 2) Median capacity of ENERGY STAR-certified models by configuration. Accessed December 2023. Weblink
- 3) U.S. EPA. (2021). ENERGY STAR Program Requirements Product Specification for Clothes Washers, Eligibility Criteria Version 8.1. Weblink

<sup>70</sup> Average annual electricity consumption of 3.73 and 3.81 CEF dryers scaled from 283 cycles/yr (national 2005 RECS) to 251×96%=241 cycles/yr (Mid-Atlantic 2015 RECS).

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- 4) [NMR Group for the Pennsylvania Public Utility Commission. \(2024, March\). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Page 122, Table 105 \(%ElecDHW\). Page 158, Table 149 \(%ElecDryer\). Weblink](#)
- 5) [The percentage of total energy consumption that is used for the machine, heating the hot water, or by the dryer varies depending on the efficiency of the unit. Values are based on a weighted average of top-loading and front-loading units by consumption data from source 1. Distribution of baseline top- and front-loading units from NMR Group for the Pennsylvania Public Utility Commission. \(2024, March\). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Page 151, Table 139. Weblink. Distribution of ENERGY STAR top- and front-loading units from ENERGY STAR-certified models. Accessed December 2023. Weblink](#)
- 6) [Calculated using “Frequency of clothes washer use” and “Frequency of dryer use” data for the Mid-Atlantic region Pennsylvania from U.S. Department of Energy-2015, 2020 Residential Energy Consumption Survey. Weblink](#)
- 7) [10 CFR 430.32\(g\)\(4\) Weblink](#)
- 8) [Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink](#)
- 9) [U.S. DOE. \(2024, March 15\). Direct final rule. Federal Register, 89 \(52\), pages 19,026-19,126. Weblink](#)
- 10) [U.S. DOE \(2024\). Life-Cycle Cost \(LCC\) Analysis RCW ECS Direct Final Rule Spreadsheet. Weblink](#)

### 2.4.9 ENERGY STAR CLOTHES DRYERS

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Clothes Dryer
<b>Measure Life</b>	14 years <sup>Source 3</sup>
<b>Vintage</b>	Replace on Burnout, New Construction

ENERGY STAR clothes dryers have a higher CEF (combined energy factor) than standard dryers. They save energy by using lower temperatures than standard dryers and incorporating a moisture sensor to reduce excessive drying of clothes and prolonged drying cycles.

ENERGY STAR clothes dryers that use heat pump technology have the highest CEFs. Whereas a conventional dryer heats air, passes it through the clothing drum, and exhausts the hot air, a heat pump dryer works by circulating hot air through the clothing drum, extracting moisture from the clothing that becomes condensation after passing over an evaporator coil, then reheating the air before it passes through the drum again. The heat pump dryer saves energy by recirculating the warm air, requiring less heat to reach the desired temperature, and because the process requires a lower air temperature overall to dry clothes.

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#### ELIGIBILITY

This protocol documents the energy savings attributed to purchasing an electric dryer that meets ENERGY STAR criteria. Different default CEF<sub>ee</sub>'s are provided for dryers that use heat pump technology (including hybrid heat pump dryers) and those that do not.

#### ALGORITHMS

The energy savings are obtained through the following formulas:

$$\Delta kWh = \left( \frac{1}{CEF_{base}} - \frac{1}{CEF_{ee}} \right) \times Load_{avg} \times Cycles_{wash} \times \%_{dry_{wash}}$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDF_w$$

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#### DEFINITION OF TERMS

**Table 2-107: Terms, Values, and References for ENERGY STAR Clothes Dryers**

Term	Unit	Values	Source
<u>Cycles<sub>wash, yr</sub></u> : Number of washing machine cycles per year	<u>cycles/yr</u>	178	5
<u>Load<sub>avg, lbs</sub></u> : Weight of average dryer load, in pounds per load	<u>lbs/load</u>	Standard: 8.45 Compact: 3.00	6
<u>%<sub>dry, wash</sub></u> : Percentage of homes with a dryer that use the dryer for every load	%	99% Or EDC data gathering	5, EDC data gathering

<u><math>CEF_{base}</math></u> , Combined Energy Factor of baseline dryer, in lbs/kWh	<u>lbs/kWh</u>	<u>Table 2-108 or EDC Data Gathering</u>	<u>2.7, EDC data gathering</u>
<u><math>CEF_{ee}</math></u> , Combined Energy Factor of ENERGY STAR dryer, in lbs/kWh	<u>lbs/kWh</u>	<u>Table 2-108 or EDC Data Gathering</u>	<u>1, EDC data gathering</u>
<u><math>ETDF_s</math></u> , Summer energy to Demand Factor	<u><math>\frac{kW}{kWh}</math></u>	<u>0.0001346</u>	<u>4</u>
<u><math>ETDF_w</math></u> , Winter energy to Demand Factor	<u><math>\frac{kW}{kWh}</math></u>	<u>0.0001350</u>	<u>4</u>

**Table 2-108: Combined Energy Factor for Federal Minimum Standard and ENERGY STAR Dryers**

<u>Product Type</u>	<u><math>CEF_{base}</math> through 2/29/28</u>	<u><math>CEF_{base}</math> starting 3/1/28</u>	<u><math>CEF_{ee}</math></u>
<u>Vented Electric, Standard (4.4 ft<sup>3</sup> or greater capacity)</u>	<u>3.73</u>	<u>3.93</u>	<u>No heat pump: 3.93 Hybrid: 4.50</u>
<u>Ventless Electric, Standard (4.4 ft<sup>3</sup> or greater capacity)</u>	<u>3.73</u>	<u>3.93</u>	<u>No heat pump: 3.93 Hybrid: 5.20 Heat pump: 9.75</u>
<u>Vented or Ventless Electric, Compact (120V) (less than 4.4 ft<sup>3</sup> capacity)</u>	<u>3.61</u>	<u>4.33</u>	<u>No heat pump: 3.80 Heat pump: 6.37</u>
<u>Vented Electric, Compact (240V) (less than 4.4 ft<sup>3</sup> capacity)</u>	<u>3.27</u>	<u>3.57</u>	<u>No heat pump: 3.45</u>
<u>Ventless Electric, Compact (240V) (less than 4.4 ft<sup>3</sup> capacity)</u>	<u>2.55</u>	<u>2.68</u>	<u>No heat pump: 2.68 Heat pump: 5.60</u>

**DEFAULT SAVINGS**

Table 2-109 displays default energy savings for ENERGY STAR clothes dryers through 2/29/28. Table 2-110 displays default energy savings for ENERGY STAR clothes dryers starting 3/1/28 when new federal minimum CEFs go into effect, at which point only clothes dryers with heat pump technology will be efficient enough to generate energy savings.

**Table 2-109: Default Energy Savings and Demand Reductions for ENERGY STAR Clothes Dryers through 2/29/28**

<u>Product Type</u>	<u><math>\Delta kWh</math></u>	<u><math>\Delta kW_{summer\ peak}</math></u>	<u><math>\Delta kW_{winter\ peak}</math></u>
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<u>Vented Electric, Standard Capacity</u>	<u>20.3</u>	<u>0.0027345</u>	<u>0.0027435</u>
<u>Vented Electric, Standard Capacity, Hybrid</u>	<u>68.3</u>	<u>0.0091945</u>	<u>0.0092247</u>
<u>Ventless Electric, Standard Capacity</u>	<u>20.3</u>	<u>0.0027345</u>	<u>0.0027435</u>
<u>Ventless Electric, Standard Capacity, Hybrid</u>	<u>112.9</u>	<u>0.0151902</u>	<u>0.0152402</u>
<u>Ventless Electric, Standard Capacity, Heat Pump</u>	<u>246.5</u>	<u>0.0331772</u>	<u>0.0332864</u>
<u>Vented or Ventless Electric, Compact Capacity, 120V, Heat Pump</u>	<u>63.5</u>	<u>0.0085405</u>	<u>0.0085686</u>
<u>Vented Electric, Compact Capacity, 240V</u>	<u>8.4</u>	<u>0.0011353</u>	<u>0.0011391</u>
<u>Ventless Electric, Compact Capacity, 240V</u>	<u>10.1</u>	<u>0.0013536</u>	<u>0.0013581</u>
<u>Ventless Electric, Compact Capacity, 240V, Heat Pump</u>	<u>112.9</u>	<u>0.0151982</u>	<u>0.0152483</u>

**Table 2-110: Default Energy Savings and Demand Reductions for ENERGY STAR Clothes Dryers as of 3/1/28**

<u>Product Type</u>	<u><math>\Delta kWh</math></u>	<u><math>\Delta kW_{summer\ peak}</math></u>	<u><math>\Delta kW_{winter\ peak}</math></u>
<u>Vented Electric, Standard Capacity, Hybrid</u>	<u>48.0</u>	<u>0.0064599</u>	<u>0.0064812</u>
<u>Ventless Electric, Standard Capacity, Hybrid</u>	<u>92.5</u>	<u>0.0124556</u>	<u>0.0124966</u>
<u>Ventless Electric, Standard Capacity, Heat Pump</u>	<u>226.2</u>	<u>0.0304427</u>	<u>0.0305429</u>
<u>Vented or Ventless Electric, Compact Capacity, 120V, Heat Pump</u>	<u>39.1</u>	<u>0.0052629</u>	<u>0.0052802</u>
<u>Ventless Electric, Compact Capacity, 240V, Heat Pump</u>	<u>102.9</u>	<u>0.0138446</u>	<u>0.0138902</u>

### **EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of installation coupled with calculation of energy and demand savings using the above algorithms.

### **SOURCES**

- 6)1) U.S. EPA. (2015). <https://www.eia.gov/consumption/residential/data/2015/index.php?view=microdataENERGY> STAR Program Requirements Product Specification for Clothes Dryers Version 1.1. Weblink
- 2) 10 CFR 430.32(h) Weblink
- 3) Energy Efficiency and Renewable Energy Office (2021). National Impact Preliminary Analysis Spreadsheets. U.S DOE. Weblink

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- 4) [Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink](#)
- 5) [Calculated using “Frequency of clothes washer use” and “Frequency of dryer use” data for Pennsylvania from U.S. Department of Energy, 2020 Residential Energy Consumption Survey. Weblink](#)
- 6) [10 CFR Appendix-D1-to-Subpart-B-of-Part-430 2.7.1 Weblink](#)
- 7) [U.S. DOE. \(2024, March 12\). Direct final rule. Federal Register, 89 \(49\), pages 18,164-18,243. Weblink](#)

### 2.4.82.4.10 ENERGY STAR DISHWASHERS

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Dishwasher
<b>Measure Life</b>	10 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout

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#### ELIGIBILITY

<b>Vintage</b>	Replace on Burnout
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#### ELIGIBILITY

This measure is for the purchase and installation of an ENERGY STAR dishwasher meeting ENERGY STAR eligibility criteria. ENERGY STAR dishwashers use less energy and hot water than non-qualified models.

#### ALGORITHMS

The general form of the measure savings equation for ENERGY STAR Dishwashers is:

$$\text{Total Savings} = \text{Number of Dishwashers} \times \text{Savings per Dishwasher}$$

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of dishwashers. The number of dishwashers will be determined using market assessments and market tracking. EDC data gathering is permitted for kWh<sub>ee</sub> provided that it is gathered from the ENERGY STAR qualified product list.

Per unit energy and demand savings algorithms for dishwashers utilizing electrically heated hot water:

$$\Delta \text{ kWh} = (kWh_{base} - kWh_{ee}) \times (\%kWh_{OP} + \%kWh_{heat} \times \%Electric_{DHW})$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDf_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDf_w$$

#### DEFINITION OF TERMS

$$\Delta kW_{peak} = \frac{\Delta kWh/yr}{HOU} \times CF$$

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#### DEFINITION OF TERMS



Table 2-111: Terms, Values, and References for ENERGY STAR Dishwashers

Term	Unit	Value	Source
$kWh_{base}$ , Annual energy consumption of baseline dishwasher	kWh/yr	Standard: 307 Compact: 222	1, 63
$kWh_{eae}$ , Annual energy consumption of ENERGY STAR qualified unit	kWh/yr	270EDC data gathering Defaults: Standard: 240 Compact: 155	1, 7EDC data gathering, 4
$\%kWh_{op}$ , Percentage of unit dishwasher energy consumption used for operation	%	44%	1
$\%kWh_{heat}$ , Percentage of dishwasher unit energy consumption used for water heating	%	56%	1
$\%Electric_{DHW}$ , Percentage of dishwashers assumed to utilize electrically heated hot water heaters that are electric	%	EDC Data Gathering Default = 31.747%	2EDC data gathering, 3
$HOU$ , Hours of use per year $ETDF_s$ , Summer energy to Demand Factor	hours/yr $\frac{kWh}{kWh}$	2340.0001699	35
$CF$ , Demand Coincidence Factor. The coincidence of average dishwasher demand to summer system peak $ETDF_w$ , Winter energy to Demand Factor	Proportion $\frac{kWh}{kWh}$	0.0260002640	4, 5

ENERGY STAR qualified dishwashers must use less than or equal to the water and energy consumption values given in Table 2-86. Note, as of May 30, 2013, ENERGY STAR compact dishwashers have the same maximum water and energy consumption requirements as the federal standard and therefore are not included in the TRM since there is not energy savings to be calculated for installation of an ENERGY STAR compact dishwasher in Table 2-112 and Table 2-113. A standard sized dishwasher is defined as any dishwasher that can hold 8 or more place settings and at least six serving pieces. Source 6 while compact size dishwashers have a capacity less than eight place settings plus six serving pieces. Source 6

Table 2-112: Federal Standard and ENERGY STAR v 67.0 Residential Dishwasher Standard

Product Type	Federal Standard <sup>Source 62</sup>		ENERGY STAR v 67.0 <sup>Source 74</sup>	
	Water (gallons per cycle)	Energy (kWh per year)	Water (gallons per cycle)	Energy (kWh per year)
Standard	≤ 5.0	≤ 307	≤ 3.52	≤ 270240
Compact	≤ 3.5	≤ 222	≤ 2.0	≤ 155

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The default savings values for electric and non-electric water heating and the default fuel mix from Table 2-87, Table 2-113. Note that default savings for standard and compact dishwashers are the same because the difference in consumption between the baseline and efficient models ( $kWh_{base} - kWh_{ee}$ ) is the same (67 kwh).

Table 2-113: Default Dishwasher Energy Savings (Standard and Compact)

Water Heating	$\Delta kWh/yr$	$\Delta kW_{peak} \Delta kW_{summer peak}$	$\Delta kW_{winter peak}$
Electric (%Electric <sub>DHW</sub> = 100%)	3767.0	0.0044101138	0.01769
Non-Electric (%Electric <sub>DHW</sub> = 0%)	46329.5	0.0048400501	0.00778
Default Fuel Mix (%Electric <sub>DHW</sub> = 43.47%)	22847.1	0.0025400800	0.01244

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### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

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### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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- 1) ENERGY STAR Appliances Calculator. Accessed July 2018. Energy Star Calculator, EPA research on available models. Accessed August 2018. [https://www.energystar.gov/sites/default/files/asset/document/appliance\\_calculator.xlsx](https://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx)
- 1) Statewide average for all housing types from ENERGY STAR (2016). Savings Calculator for ENERGY STAR Qualified Appliances. U.S. EPA. Weblink
- 2) 10 CFR 430.32(f) Weblink
- 2)3) NMR Group for the Pennsylvania Statewide Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study, 2018. Page 122, Table 105. Weblink
- 4) U.S. EPA. (2023). ENERGY STAR Program Requirements Product Specification for Residential Dishwashers Eligibility Criteria Version 7.0. Weblink
- 5) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink  
[https://www.energystar.gov/products/appliances/dishwashers/key\\_product\\_criteria](https://www.energystar.gov/products/appliances/dishwashers/key_product_criteria)

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- 3) ~~2014 Pennsylvania Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014\\_PA\\_Statewide\\_Act129\\_Residential\\_Baseline\\_Study.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-2014_PA_Statewide_Act129_Residential_Baseline_Study.pdf). HOU=(3 loads/week)×(52 weeks/yr)×(1.5 hours/load). 3 load/week comes from 2014 Baseline study. 1.5 hours/load is assumption used by Efficiency Vermont and Illinois Statewide TRMs~~
- 4) ~~Calculated from Itron eShapes, 8760 hourly data by end use for Missouri, as provided by Ameren. This is the CF value for ENERGY STAR Dishwashers from Illinois Statewide TRM Version 7.0, June 2018.~~
- 5) ~~Illinois Statewide Technical reference Manual for Energy Efficiency Version 7.0. Effective January 1, 2019. <http://www.ilsag.info/technical-reference-manual.html>~~
- 6) ~~US Department of ENERGY Website. Appliance and Equipment Standards. Accessed Aug. 2018. [https://www.ecfr.gov/cgi-bin/text-idx?SID=86e70cbc87e5af18caca2e5c205bd107&mc=true&node=se10.3.430\\_132&rgn=div8](https://www.ecfr.gov/cgi-bin/text-idx?SID=86e70cbc87e5af18caca2e5c205bd107&mc=true&node=se10.3.430_132&rgn=div8)~~
- 7) ~~Dishwashers Key product Criteria. Accessed Aug. 2018. [https://www.energystar.gov/products/appliances/dishwashers/key\\_product\\_criteria](https://www.energystar.gov/products/appliances/dishwashers/key_product_criteria)~~

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### 2.4.92.4.11 ENERGY STAR DEHUMIDIFIERS

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Dehumidifier
<b>Measure Life</b>	12 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout
<b>Vintage</b>	Replace on Burnout

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ENERGY STAR qualified dehumidifiers are ~~15 percent~~13% more efficient than non-qualified models due to more efficient refrigeration coils, compressors and fans.<sup>Source 2</sup> ENERGY STAR Most Efficient portable dehumidifiers are ~~23 percent~~over 20% more efficient than ~~standard products~~federal minimum standards.<sup>Source 67</sup>

#### ELIGIBILITY

**THIS PROTOCOL DOCUMENTS THE ENERGY AND DEMAND SAVINGS ATTRIBUTED TO PURCHASING AN ENERGY STAR OR ENERGY STAR MOST EFFICIENT DEHUMIDIFIER INSTEAD OF A STANDARD ONE.**  
**ELIGIBILITY**

~~This protocol documents the energy and demand savings attributed to purchasing an ENERGY STAR or ENERGY STAR Most Efficient dehumidifier instead of a standard one.~~ Dehumidifiers must meet ENERGY STAR Version 4.0 Product Specifications to qualify.<sup>Source 3</sup> The target sector is residential.

#### ALGORITHMS

The general form of the equation for the ENERGY STAR Dehumidifier savings algorithm is:

$$\text{Total Savings} = \text{Number of Dehumidifiers} \times \text{Savings per Dehumidifier}$$

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of dehumidifiers. The number of dehumidifiers will be determined using market assessments and market tracking.

Per unit energy and summer peak demand savings algorithms:

$$\Delta kWh = \left( \frac{CAPY \times 0.473 \frac{\text{liters}}{\text{pint}}}{24 \frac{\text{hours}}{\text{day}}} \right) \left( \frac{CAPY \times 0.473 \frac{\text{liters}}{\text{pint}}}{24 \frac{\text{hours}}{\text{day}}} \right) \times HOU \times \left( \frac{1}{L/kWh_{base}} - \frac{1}{L/kWh_{ee}} \right) \left( \frac{1}{IEF_{base}} - \frac{1}{IEF_{ee}} \right)$$

$$\Delta kWh_{summer peak} = \frac{\Delta kWh/yr}{HOU} \times CF$$

$$\Delta kWh_{winter peak} = 0$$

#### DEFINITION OF TERMS

**Table 2-114: Terms, Values, and References for ENERGY STAR Dehumidifier**

Term	Unit	Value	Sources
CAPY, Average capacity of the unit	$\frac{\text{pints}}{\text{day}}$	EDC Data Gathering	EDC Data Gathering
HOU, Annual hours of operation	$\frac{\text{hours}}{\text{yr}}$	1,6322,160	1
$\frac{\text{L}}{\text{kWh}_{\text{base}}}$ $\cdot$ $IEF_{\text{base}}$ , Baseline unit liters of water condensate per kWh consumed	$\frac{\text{liters}}{\text{kWh}}$	Table 2-89 Table 2-115	24
$\frac{\text{L}}{\text{kWh}_{\text{base}}}$ $\cdot$ $IEF_{\text{ee}}$ , ENERGY STAR qualified unit liters of water condensate per kWh consumed	$\frac{\text{liters}}{\text{kWh}}$	EDC Data Gathering Default: Table 2-90 or Table 2-91 Default: Table 2-115	EDC data gathering, 3, 56
CF, Demand Coincidence Factor Summer demand coincidence factor	Proportion	0.405	45

**Table 2-89**

Table 2-115 shows the federal standard minimum efficiency standards. Federal standards are effective as of June 13, 2019. Table 2-90 shows ENERGY STAR 45.0 standards effective as of October 25, 2016. Table 2-91 shows ENERGY STAR Most Efficient 2018 criteria, effective January 2018. Federal standards and ENERGY STAR Most Efficient criteria distinguish between portable dehumidifiers (designed to dehumidify a confined living space and plugged into an electrical outlet) and whole-home dehumidifiers (incorporated into the home's HVAC system and designed to dehumidify all conditioned spaces).

**Table 2-115: Dehumidifier Minimum Federal Efficiency Standards**

Type	Capacity (pints/day)	Federal Standard ( $\frac{\text{L}}{\text{kWh}_{\text{base}}}$ $\cdot$ $IEF_{\text{base}}$ )	ENERGY STAR ( $IEF_{\text{ee}}$ )	ENERGY STAR Most Efficient ( $IEF_{\text{ee}}$ )
Portable dehumidifier	≤ 25	≥ 1.30	≥ 1.57	≥ 1.75
	> 25 to ≤ 50	≥ 1.60	≥ 1.80	≥ 2.01
	> 50	≥ 2.80	≥ 3.30	≥ 3.40
Whole-home dehumidifier	Product Case Volume (ft <sup>3</sup> )	Federal Standard ( $\frac{\text{L}}{\text{kWh}_{\text{base}}}$ $\cdot$ $IEF_{\text{base}}$ )	ENERGY STAR ( $IEF_{\text{ee}}$ )	ENERGY STAR Most Efficient ( $IEF_{\text{ee}}$ )
	≤ 8	≥ 1.77	≥ 2.09	≥ 2.22
	> 8	≥ 2.41	≥ 3.30	≥ 3.81

**DEFAULT SAVINGS**

The annual energy usage and savings of an ENERGY STAR unit over the federal minimum standard are presented in Table 2-116 for each capacity range.

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**Table 2-116: Dehumidifier ENERGY STAR Standards Default Energy Savings**

	Product <sup>a</sup>	Capacity Range (pints/day or ft <sup>3</sup> )	Default Capacity (pints/day)	Federal Standard ENERGY STAR (L/kWh <sub>23°C</sub> ) (IEF)	Efficient (IEF)	ΔkWh/yr	ΔkW <sub>summer peak</sub>	ΔkW <sub>winter peak</sub>
ENERGY STAR	Portable	≤ 25 pints/day	25	1.30	1.57	141	0.0160	0.0206
	Portable	> 25 to ≤ 50 pints/day	50	1.60	1.80	148	0.0168	0.0216
	Whole house	≤ 8 ft <sup>3</sup>	84 <sup>b</sup>	1.77	≥ 2.0009	309	0.0351	0.0453
ENERGY STAR Most Efficient	Portable	≤ 25 pints/day	25	1.30	1.75	211	0.0239	0.0308
	Portable	> 25 to ≤ 50 pints/day	50	1.60	≥ 2.8001	271	0.0308	0.0397
	Whole house	≤ 8 ft <sup>3</sup>	84 <sup>b</sup>	1.77	2.22	410	0.0465	0.0599

**Table 2-93: Dehumidifier ENERGY STAR Most Efficient Criteria**

Type	Capacity (pints/day)	ENERGY STAR (L/kWh <sub>23°C</sub> )
Portable	< 75	≥ 2.20
Whole House	< 75	≥ 2.30

<sup>a</sup> There are no default values for portable humidifiers >50 pints/day or whole house dehumidifiers >8ft<sup>3</sup> because there were no ENERGY STAR qualified dehumidifiers with these capacities as of August 15, 2023.

**<sup>a</sup> Default SAVINGS**

The annual energy usage and savings of an ENERGY STAR unit over the federal minimum standard are presented in Table 2-92 for each capacity range based on the average capacity of ENERGY STAR whole home models as listed on August 15, 2023.

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values.

**Table 2-94: Dehumidifier Default Energy Savings**

Efficient Product <sup>71</sup>	Capacity Range (pints/day)	Default Capacity (pints/day)	Federal Standard (kWh/yr)	Efficient Standard (kWh/yr)	ΔkWh/yr	ΔkW <sub>peak</sub>
ENERGY STAR	≤ 25	25	1.3	2.0	216	0.05372
	> 25 to ≤ 50	50	1.6	2.0	204	0.04989
ENERGY STAR Most Efficient—Portable	≤ 25	25	1.3	2.2	253	0.06279
	> 25 to ≤ 50	50	1.6	2.2	274	0.06803

<sup>71</sup> As of November 16, 2018, Federal standards equal or exceed ENERGY STAR standards for portable dehumidifiers with capacity of >50 pints/day and for whole home dehumidifiers with product case volume > 8 ft<sup>3</sup>.

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Efficient Product <sup>71</sup>	Capacity Range (pints/day)	Default Capacity (pints/day)	Federal Standard (kWh/yr)	Efficient Standard (kWh/yr)	$\Delta kWh/yr$	$\Delta kW_{peak}$
ENERGY STAR Most Efficient—Whole House with product case volume $\leq 8 ft^3$	< 75	63 <sup>72</sup>	1.77	2.3	264	0.06547

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**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- 1) ENERGY STAR Appliance Savings Calculator. Accessed August, 2018. [https://www.energystar.gov/sites/default/files/asset/document/appliance\\_calculator.xlsx](https://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx)
- 2) US Department of ENERGY Website. Appliance and Equipment Standards. Accessed June 2014. [http://www1.eere.energy.gov/buildings/appliance\\_standards/product.aspx/productid/55](http://www1.eere.energy.gov/buildings/appliance_standards/product.aspx/productid/55)
- 1) Mattison, Lauren et al. (2012). "Dehumidifiers: A Major Consumer of Residential Electricity". Pages 9-208. The Cadmus Group. Weblink
- 2) U.S. EPA. (2019). ENERGY STAR Dehumidifiers Version 5.0 Cover letter. Weblink
- 3) U.S. EPA. (2019). ENERGY STAR Program Requirements Product Specification for Dehumidifiers, Eligibility Criteria Version 4.0. Accessed November 2, 2018. [https://www.energystar.gov/products/appliances/dehumidifiers/key\\_efficiency\\_criteria5.0](https://www.energystar.gov/products/appliances/dehumidifiers/key_efficiency_criteria5.0). Weblink
- 4) 10 CFR 430.32(v) Weblink
- 4)5) Dehumidifier Metering in PA and Ohio by ADM from 7/17/2013 to 9/22/2013. 31 Units Thirty-one units metered. Assumes all non-coincident peaks occur within window and that the average load during this window is representative of the June PJM days as well.
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- 6) ENERGY STAR Most Efficient 2019 memo. Accessed November 2, 2018. [https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Most%20Efficient%202019%20Memo\\_0.pdf](https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Most%20Efficient%202019%20Memo_0.pdf)
- 6) U.S. EPA. (2024). ENERGY STAR Most Efficient 2024 Dehumidifiers Recognition Criteria. Weblink
- 7) U.S. EPA. (2023). ENERGY STAR Most Efficient 2024 Final Criteria Recognition Letter. Weblink

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<sup>72</sup> Average of products listed on ENERGY STAR Most Efficient 2018—Dehumidifiers. <https://www.energystar.gov/most-efficient/mo-certified-dehumidifiers/> Accessed November 16, 2018.

**2.4.102.4.12 DEHUMIDIFIER RETIREMENT**

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Dehumidifier
<b>Measure Life</b>	4 years <sup>73</sup> years <sup>Source 7</sup>
<b>Vintage</b>	Early Retirement

This measure is defined as retirement and recycling without direct EDC replacement of an operable but older and inefficient room dehumidifier unit that would not have otherwise been recycled. The assumption is that these units will be permanently removed from the grid rather than handed down or sold for use in another location by another EDC customer, and furthermore that they would not have been recycled without this program. This measure is quite different from other energy-efficiency measures in that the energy/demand savings is not the difference between a pre- and post- configuration, but is instead the result of complete elimination of the existing dehumidifier.

**ELIGIBILITY**

The savings are not attributable to the customer that owned the dehumidifier, but instead are attributed to a *hypothetical user* of the equipment had it not been recycled. Energy and demand savings is the estimated energy consumption of the retired unit over its remaining useful life (RUL).

**ALGORITHMS**

Impacts are based only on the existing unit, and savings apply *only for the remaining useful life (RUL) of the unit*.

The energy savings and demand reduction of this measure were established using actual metered residential dehumidifier usage data.

The metered data was best fit with a polynomial which is second order in temperature humidity index and first order in capacity:<sup>Source 1</sup>

$$kWh = -8.36 \cdot 10^{-3} \times THI_{PJM}^2 + 1.19 \times THI_{PJM} + 4.07 \cdot 10^{-2} \times CAPY + -38.37$$

where:

$$THI_{PJM} = \begin{cases} DB - 0.55 \times (1 - RH) \times (DB - 58) & \text{for } DB \geq 58^\circ F \\ DB & \text{for } DB < 58^\circ F \end{cases}$$

Similarly, summer peak demand was modeled with the following capacity-dependent linear regression:<sup>Source 2</sup>

~~$$kW = \Delta kW_{summer\ peak} = 1.3 \cdot 10^{-3} \times CAPY + 1.07 \cdot 10^{-1}$$~~

$$\Delta kW_{winter\ peak} = 0$$

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<sup>73</sup> CA-DEER gives the following rule-of-thumb for remaining useful life: RUL = (1/3) X EUL. As the Energy Star Dehumidifier [replacement] uses an EUL of 12 years, we have a suggested RUL of (1/3) X 12 years = 4 years.



**DEFINITION OF TERMS**

**Table 2-117: Terms, Values, and References for Dehumidifier Retirement**

Term	Unit	Value	Sources
CAPY, Average capacity of the unit	$\frac{\text{pints}}{\text{day}}$	EDC Data Gathering Default: 51 pt/day	EDC Data Gathering. 3
THI, Temperature Humidity Index	-	Calculated	4
DB, Dry bulb temperature	$^{\circ}\text{F}$	See Source	5
RH, Relative humidity	%	See Source	5

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The results of the kWh calculation for typical dehumidifier capacities in each of the Climate Regions are presented in the following table. For capacity values not listed in the table, it is acceptable to calculate a value by linear interpolation of the savings values for the adjacent capacities.

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**Table 2-118: Dehumidifier Retirement Annual Energy Savings (kWh)**

Annual kWh Savings by Climate Region											
Climate Region	Reference City	Capacity (pints per day)									
		25	30	35	40	45	50	60	65	70	110
C	Allentown	628	656	684	712	740	768	824	852	881	1105
A	Bradford	386	404	422	440	458	476	512	530	547	691
G	Binghamton	470	492	513	534	556	577	620	641	663	834
I	Erie	557	582	607	632	656	681	731	756	781	979
E	Harrisburg	656	686	715	745	774	804	863	892	922	1158
D	Philadelphia	726	758	791	823	856	888	954	986	1019	1280
H	Pittsburgh	605	632	659	686	713	740	795	822	849	1066
B	Scranton	577	603	628	654	680	706	758	784	810	1016
F	Williamsport	651	680	709	738	767	797	855	884	913	1146

The summer peak kW reduction for recycling a dehumidifier was taken to be equal to the peak demand of the existing unit. These results are presented in the following table:

**Table 2-119: Dehumidifier Retirement Peak Demand Reduction (kW)**

Capacity	25	30	35	40	45	50	60	65	70	110
kW	0.1393	0.1458	0.1523	0.1588	0.1653	0.1718	0.1848	0.1913	0.1979	0.2499

**DEFAULT SAVINGS**

For programs that do not track capacity, an “unknown” category has been provided based on the weighted average capacity of dehumidifier sales data:

Table 2-120: Default Dehumidifier Retirement Annual Energy Savings (kWh)

Annual kWh Savings by Climate Region		
Region	Reference City	Default
C	Allentown	774
A	Bradford	479
G	Binghamton, NY	581
I	Erie	686
E	Harrisburg	810
D	Philadelphia	895
H	Pittsburgh	746
B	Scranton	711
F	Williamsport	802

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Table 2-121: Default Dehumidifier Retirement **Summer** Peak Demand Reduction (kW)

Capacity	Default
kWΔkW <sub>summer peak</sub>	0.1731

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### EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify retirement and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify retirement and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

### SOURCES

- 1) Dehumidifier Metering in PA and Ohio by ADM from 7/17/2013 to 9/22/2013. 31 Units metered; five-minute interval power data was recorded. 58% of the units were Energy Star rated.
- 2) Ibid., by Act 129 Peak Demand window
- 3) ~~Statewide average NMR Group for all housing types from the~~ Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 2018 Residential Baseline Study, 2018, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Page 164, Table 156. Weblink
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- 6) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

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7) CA DEER gives the following rule-of-thumb for remaining useful life:  $RUL = (1/3) \times EUL$ . As the Energy Star Dehumidifier [replacement] uses an EUL of 12 years, we have a suggested RUL of  $(1/3) \times 12 \text{ years} = 4 \text{ years}$ .

### 2.4.112.4.13 ENERGY STAR CEILING FANS

Target Sector	Residential Establishments
Measure Unit	Ceiling Fan Unit
Measure Life	1510 years for fan, <sup>Source 1</sup> See 2.1.1 for lighting
Vintage	Replace on Burnout

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Vintage	Replace on Burnout
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ENERGY STAR ceiling fans require a more efficient CFM/Watt rating than standard ceiling fans as well as ENERGY STAR qualified lighting for those with light kits included. Both of these features save energy compared to standard ceiling fans.

#### ELIGIBILITY

#### ELIGIBILITY

This protocol documents the energy savings attributed to installing an ENERGY STAR Version 4.0 ceiling fan (with or without a lighting kit) <sup>Source 2</sup> in lieu of a standard efficiency ceiling fan meeting the January 21, 2020 federal efficiency requirements. <sup>Source 2</sup> If a customer submits a rebate for a product that has applied for ENERGY STAR Certification but has not yet been certified, the savings will be counted for that product contingent upon its eventual certification as an ENERGY STAR measure. If at any point the product is rejected by ENERGY STAR, the product is then ineligible for the program and savings will not be counted.<sup>74</sup> The target sector primarily consists of single-family residences.<sup>3</sup>

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#### ALGORITHMS

The total energy savings is equal to the savings contribution of the fan plus the savings contribution of the lighting, if applicable. If the ENERGY STAR fan does not include a lighting kit, then  $\Delta kWh_{lighting} = 0$ . The energy and peak demand savings are obtained through the following formulas. These algorithms do not seek to estimate the behavioral change attributable to the use of a ceiling fan vs. versus a lower AC setting.

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The energy savings are obtained through the following formula:

$$\Delta kWh = -\Delta kWh_{fan} + \Delta kWh_{lighting}$$

$$\Delta kWh_{fan} = -DW_{fan} \Delta kWh = \Delta W_{fan} \times \frac{1 kW}{1,000 W} \frac{1}{1,000} \times HOU_{fan} \times 365 \frac{days}{yr}$$

$$\Delta kW_{summer peak} = \Delta kWh \times ETDF_s$$

$$\Delta kW_{winter peak} = \Delta kWh \times ETDF_w$$

<sup>74</sup> The Pennsylvania SWE and PUC TUS staff added this condition relating to certification that has been applied for but not yet received at the request of several of the Pennsylvania EDCs. EDCs will be responsible for tracking whether certification is granted.

### **DEFINITION OF TERMS**

~~$\Delta kWh_{lighting}$  =  $\Delta kWh$  from the ENERGY STAR Lighting section~~

~~Demand savings result from the lower connected load of the ENERGY STAR fan and ENERGY STAR lighting. Peak demand savings are estimated using a Coincidence Factor (CF):~~

~~$$\Delta kWh_{peak,total} = \Delta kWh_{peak,fan} + \Delta kWh_{peak,lighting}$$~~

~~$$\Delta kWh_{peak,fan} = DW_{fan} \times \frac{1 kW}{1,000 W} \times CF_{fan}$$~~

 ~~$\Delta kWh_{peak,lighting}$  =  $\Delta kWh_{peak}$  from the ENERGY STAR Lighting section~~

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**DEFINITION OF TERMS**

**Table 2-122: Terms, Values, and References for ENERGY STAR Ceiling Fans**

Component	Unit	Values	Source
$DW_{Fan} \Delta W_{fan}$ , Weighted average wattage reduction from ENERGY STAR ceiling fan	Watts	Default: See Table 2-99 Table 2-123	2, 3, 5, 64
$HOU_{fan}$ , fan daily hours of use	$\frac{hours}{day}$	EDC Data Gathering Default: 3.0 hours/day <sup>75</sup>	4 EDC data gathering, 1
$CF_{Fan} - ETD_{FS}$ , Summer energy to Demand Coincidence Factor	$\frac{kW}{kWh}$ Proportion	EDC Data Gathering Default SF Only: 0.094760001114	75
$CF_{lighting} - ETD_{WT}$ , Winter energy to Demand Coincidence Factor	$\frac{kW}{kWh}$ Proportion	See Section 2.1 SF Only: 0.0001788	75

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**Table 2-123: Assumed Wattage of ENERGY STAR Ceiling Fans on High Setting**

Ceiling Fan Type	Diameter, D (inches)	$DW_{Fan} \Delta W_{fan}$ (Watts)
Standard and Low-Mount High Speed Small Diameter (HSSD) Ceiling Fans	D ≤ 36	0
	36 < D < 78	23
	D ≥ 78"	31
Hugger Ceiling Fan <sup>77</sup>	36 < D < 78	33

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**DEFAULT SAVINGS**

**Table 2-124: Energy Savings and Peak Demand Reductions for ENERGY STAR Ceiling Fans**

Product Type (Fan Only)	Diameter, D (inches)	Energy Savings (kWh) $\Delta kW/h$	Demand Reduction (kW) $\Delta kW_{summer peak}$	$\Delta kW_{winter peak}$
Standard and Low-Mount High Speed Small Diameter (HSSD) Ceiling Fans	D ≤ 36	0.0	0.0000000	0.0000
	36 < D < 78	25.2	0.0020028	0.0045
	D ≥ 78	3433.9	0.0020038	0.0061
Hugger Ceiling Fan	36 < D < 78	36.1	0.0030040	0.0065

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**EVALUATION PROTOCOLS**

<sup>75</sup> The 3-hour/day for a ceiling fan is assumed here to be the same hours of use as a typical residential lightbulb, in absence of better data. EDCs are allowed to do research on hours of use for ceiling fans in lieu of using the 3 hours/day figure. It is likely that the hours of use for ceiling fans is different than that of residential lighting.

<sup>76</sup> Assumed same usage characteristics as lighting. EDCs are allowed to do research on Coincidence Factor for ceiling fans in lieu of using the 3 hours/day figure. It is likely that the hours of use for ceiling fans is different than that of residential lighting.

<sup>77</sup> The ENERGY STAR 4.0<sup>1</sup> specifications allow for hugger ceiling fans with blade spans of ≤ 36" and ≥ 78", however, as of December 2018/November 2023, there are no ENERGY STAR qualified products meeting those criteria. They were therefore omitted from this characterization.

The most appropriate evaluation protocol for this measure is verification of installation coupled with calculation of energy and demand savings using above algorithms.

#### SOURCES

- 1) ~~Residential and C&I Lighting and HVAC Report Prepared for SPWG, 2007, p. C-2.~~
- 2) ~~Energy and water conservation standards and their compliance dates. 10 C.F.R. § 430.32.~~
- 3) ~~See ENERGY STAR Ceiling Fans Work Paper 2018.12.5.xlsx for calculations and description of methodology.~~
- 4) ~~ENERGY STAR Lighting Fixture and Ceiling Fan Calculator. Updated September 2013.~~
- 1) ~~ENERGY STAR (2013). Savings Calculator for ENERGY STAR Qualified Light Fixtures & Ceiling Fans U.S. EPA. Weblink~~
- 5) ~~2) U.S. EPA. (2018). ENERGY STAR® Program Requirements Product Specification for Residential Ceiling Fans and Ceiling Fan Light Kits Eligibility Criteria Version 4.01. Weblink~~
- 3) ~~10 CFR 430.32(s) Weblink~~
- 6) ~~4) SWE analysis of ENERGY STAR-Certified Ceiling Fans | EPA ENERGY STAR. <https://www.energystar.gov/productfinder/product/certified-ceiling-fans/results>. Accessed 12/5/2018.18. Weblink~~
- 7) ~~EmPOWER Maryland 2012 Final Evaluation Report: Residential Lighting Program, Prepared by Navigant Consulting and the Cadmus Group, Inc., March 2013, Table 50.~~
- 5) ~~Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink~~

### 2.4.122.4.14 ENERGY STAR AIR PURIFIERS

Target Sector	Residential Establishments
Measure Unit	Number of Air Purifiers installed Purifier
Measure Life	9 years <sup>Source 1</sup>
Vintage	Replace on Burnout, Early Replacement, Retrofit, New Construction

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An air purifier (cleaner) is a portable electric appliance that removes dust and fine particles from indoor air. This measure characterizes the purchase and installation of a unit meeting the efficiency specifications of ENERGY STAR in place of or instead of a baseline model an ENERGY STAR unit that is more energy-efficient than a non-ENERGY STAR unit.

#### ELIGIBILITY

#### ELIGIBILITY

This measure targets residential customers who purchase and install an air purifier that meets ENERGY STAR specifications rather than installing a non-ENERGY STAR unit. In order to qualify, installed air purifiers must meet the following efficiency specifications of ENERGY STAR:

- Must produce a certified and exceed federal minimum 50 ft<sup>3</sup>/min Clean Air Delivery Rate (CADR) for Dust to be considered under this specification integrated energy factor (IEF) standards.
  - Minimum Performance Requirement: 2.0 CADR/Watt (Dust)
  - Standby Power Requirement: 2.0 Watts or less. Qualifying models that perform secondary consumer functions (e.g. clock, remote control) must meet the standby power requirement.
- UL Safety Requirement: Models that emit ozone as a byproduct of air cleaning must meet UL Standard 867 (ozone production must not exceed 50ppb)<sup>78</sup>

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#### ALGORITHMS

The following algorithms shall be used to calculate the annual energy savings and coincident peak demand savings for this measure:

$$\Delta kWh = \frac{CADR \times Hours \times \left( \frac{1}{CADR/W_{base}} - \frac{1}{CADR/W_{eff}} \right) + (POW_{base} - POW_{eff}) \times POHours}{1000}$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDf_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDf_w$$

#### DEFINITION OF TERMS

$$\Delta kWh = kWh_{base} - kWh_{ESTAR}$$

$$\Delta kW_{peak} = CF \times \frac{\Delta kWh}{HOURS}$$

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#### DEFINITION OF TERMS

<sup>78</sup> ENERGY STAR certification is sufficient to establish that an air purifier meets this requirement. No additional UL safety listing certification is required.



**Table 2-125: Terms, Values, and References for ENERGY STAR Air Purifier**

Term	Unit	Values	Source
$kWh_{Base}$ , Baseline kWh consumption per year	kWh/year	EDC Data Gathering Default = See Table 2-102	1
$kWh_{Star}$ , ENERGY STAR kWh consumption per year	kWh/year	EDC Data Gathering Default = See Table 2-102	1
<i>HOURS</i> , Average hours of use per year	Hours/year	EDC Data Gathering Default = 5,840	1
<i>CF</i> , Summer Peak Coincidence Factor	None	EDC Data Gathering Default = 0.67	1, 2

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**DEFAULT SAVINGS**

**Table 2-104: Energy Savings Calculation Default Values**

Clean Air Delivery Rate (CADR) (ft <sup>3</sup> /min)	CADR Used in Calculation	Baseline Unit Energy Consumption (kWh/yr)	ENERGY STAR Unit Energy Consumption (kWh/yr)	ΔkWh
<b>CADR 51-100</b>	75	441	148	293
<b>CADR 101-150</b>	125	733	245	488
<b>CADR 151-200</b>	175	1,025	342	683
<b>CADR 201-250</b>	225	1,317	440	877
<b>CADR Over 250</b>	275	1,609	537	1,072

<i>CADR</i> , Clean Air Delivery Rate	<i>CFM</i>	EDC Data Gathering	EDC data gathering
<i>Hours</i> , Average hours of use per year	<i>Hours/year</i>	EDC Data Gathering Default = 5,840	EDC data gathering. 1
$CADR/W_{base}$ , Clean Air Delivery Rate per watt for baseline unit	<i>CFM/W</i>	EDC Data Gathering Default = Table 2-126	2
$CADR/W_{eff}$ , Clean Air Delivery Rate per watt for efficient unit	<i>CFM/W</i>	EDC Data Gathering	EDC data gathering
$POW_{base}$ , Partial on mode power of baseline unit	<i>watts</i>	1.0	1
$POW_{eff}$ , Partial on mode power of efficient unit	<i>watts</i>	EDC Data Gathering	EDC data gathering

<u>POHours, Partial on mode hours per year</u>	<u>Hours/year</u>	<u>EDC Data Gathering Default = 2,920</u>	<u>EDC data gathering. 3</u>
<u>ETDF<sub>s</sub>, Summer energy to Demand Factor</u>	<u><math>\frac{kW}{kWh}</math></u>	<u>0.0001136</u>	<u>4</u>
<u>ETDF<sub>w</sub>, Winter energy to Demand Factor</u>	<u><math>\frac{kW}{kWh}</math></u>	<u>0.0001463</u>	<u>4</u>

Table 2-126 shows the federal minimum integrated energy factors.

**Table 2-126: Demand Savings Calculation Default Values; Air Purifier Federal Efficiency Standards**

<b>Clean Air Delivery Rate (CADR) (ft<sup>3</sup>/min)</b>	<b>CADR Used in Calculation</b>	<b>ΔkW<sub>peak</sub></b>
<b>CADR 51-100</b>	75	0.0336
<b>CADR 101-150</b>	125	0.0560
<b>CADR 151-200</b>	175	0.0784
<b>CADR 201-250</b>	225	0.1006
<b>CADR Over 250</b>	275	0.1230

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- 1) ENERGY STAR, ENERGY STAR Appliance Calculator, last updated October 2016. [https://www.energystar.gov/sites/default/files/asset/document/appliance\\_calculator.xlsx](https://www.energystar.gov/sites/default/files/asset/document/appliance_calculator.xlsx)
- 2) Assumes appliance use is equally likely at any hour of the day or night.

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<u>Product Capacity (CADR)</u>	<u>Integrated Energy Factor (PM<sub>2.5</sub> CADR/W)</u>
<u>10 ≤PM<sub>2.5</sub> CADR &lt;100</u>	<u>1.9</u>
<u>100 ≤PM<sub>2.5</sub> CADR &lt;150</u>	<u>2.4</u>
<u>PM<sub>2.5</sub> CADR ≥150</u>	<u>2.9</u>

### **SOURCES**

- 1) 16 hours per day \* 365 days per year. ENERGY STAR (2016). Savings Calculator for ENERGY STAR Qualified Appliances. U.S. EPA. Weblink
- 2) 10 CFR 430.32(ee) Weblink
- 3) (24 hours per day \* 365 days per year) – 5,840 run hours per year
- 4) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink

## 2.5 CONSUMER ELECTRONICS

### 2.5.1 ENERGY STAR OFFICE EQUIPMENT

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Office Equipment Device
<b>Measure Life</b> <sup>Source-1</sup>	Computer: 4 years Monitor: 4 years Fax: 4 years Printer: 5 years Copier: 6 years Multifunction Device: 6 years
<b>Vintage</b>	Replace-on-Burnout

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#### ELIGIBILITY

This protocol estimates savings for installing ENERGY STAR office equipment compared to standard efficiency equipment in residential applications. The measurement of energy and demand savings is based on a deemed savings value multiplied by the quantity of the measure. The target sector is primarily residential.

#### ALGORITHMS

The general form of the equation for the ENERGY STAR Office Equipment measure annual savings is:

$$\text{Total Savings} = \text{Number of Units} \times \text{Savings per Unit}$$

To determine resource savings, the per-unit estimates in the algorithms will be multiplied by the number of units. Per unit savings are primarily derived from the ENERGY STAR calculator for office equipment.

#### ENERGY STAR Computer

$$\Delta kWh = ESav_{COM}$$

$$\Delta kW_{peak} = DSav_{COM}$$

#### ENERGY STAR Fax Machine

$$\Delta kWh = ESav_{FAX}$$

$$\Delta kW_{peak} = DSav_{FAX}$$

#### ENERGY STAR Copier

$$\Delta kWh = ESav_{COP}$$

$$\Delta kW_{peak} = DSav_{COP}$$

#### ENERGY STAR Printer

$$\Delta kWh = ESav_{PRI}$$

$$\Delta kW_{peak} = DSav_{PRI}$$

**ENERGY STAR Multifunction Device**

$\Delta kWh$  \_\_\_\_\_ =  $ESav_{MUL}$   
 $\Delta kW_{peak}$  \_\_\_\_\_ =  $DSav_{MUL}$

**ENERGY STAR Monitor**

$\Delta kWh$  \_\_\_\_\_ =  $ESav_{MON}$   
 $\Delta kW_{peak}$  \_\_\_\_\_ =  $DSav_{MON}$

**DEFINITION OF TERMS**

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Table 2-106: Terms, Values, and References for ENERGY STAR Office Equipment

Term	Unit	Value	Sources
$ESav_{COM}$ - Electricity savings per purchased ENERGY STAR computer. $ESav_{FAX}$ - Electricity savings per purchased ENERGY STAR Fax Machine $ESav_{COP}$ - Electricity savings per purchased ENERGY STAR Copier $ESav_{PRI}$ - Electricity savings per purchased ENERGY STAR Printer $ESav_{MUL}$ - Electricity savings per purchased ENERGY STAR Multifunction Device $ESav_{MON}$ - Electricity savings per purchased ENERGY STAR Monitor		<i>kWh/yr</i>	See Table 2-105  1
$DSav_{COM}$ - Summer demand savings per purchased ENERGY STAR computer. $DSav_{FAX}$ - Summer demand savings per purchased ENERGY STAR Fax Machine $DSav_{COP}$ - Summer demand savings per purchased ENERGY STAR Copier $DSav_{PRI}$ - Summer demand savings per purchased ENERGY STAR Printer $DSav_{MUL}$ - Summer demand savings per purchased ENERGY STAR Multifunction Device $DSav_{MON}$ - Monitor		<i>kW/yr</i>	See Table 2-105  1

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**DEFAULT SAVINGS**

Table 2-107: ENERGY STAR Office Equipment Energy and Demand Savings Values

Measure	Energy Savings (ESav, kWh)	Demand Savings (DSav, kW)	Source	
Computer (Desktop)	449	0.0464	4	
Computer (Laptop)	22	0.0030	4	
Fax Machine (laser)	16	0.0022	4	
Copier (monochrome)	≤ 5 images/min	37	0.0050	1
	5 < images/min ≤ 15	26	0.0035	
	15 < images/min ≤ 20	10	0.0011	
	20 < images/min ≤ 30	42	0.0057	
	30 < images/min ≤ 40	50	0.0068	
	40 < images/min ≤ 65	181	0.0244	
	65 < images/min ≤ 82	372	0.0502	
	82 < images/min ≤ 90	469	0.0633	
> 90 images/min	686	0.0926		
Printer (laser, monochrome)	≤ 5 images/min	37	0.0050	1
	5 < images/min ≤ 15	26	0.0035	
	15 < images/min ≤ 20	24	0.0034	
	20 < images/min ≤ 30	42	0.0057	
	30 < images/min ≤ 40	50	0.0068	
	40 < images/min ≤ 65	181	0.0244	
	65 < images/min ≤ 82	372	0.0502	
	82 < images/min ≤ 90	542	0.0732	
> 90 images/min	686	0.0926		
Printer (Ink Jet)	6	0.0008	4	
Multifunction Device (laser, monochrome)	≤ 5 images/min	57	0.0077	4
	5 < images/min ≤ 10	48	0.0065	
	10 < images/min ≤ 26	52	0.0070	
	26 < images/min ≤ 30	93	0.0126	
	30 < images/min ≤ 50	248	0.0335	
	50 < images/min ≤ 68	420	0.0567	
	68 < images/min ≤ 80	597	0.0806	
> 80 images/min	764	0.1034		
Multifunction Device (Ink Jet)	6	0.0008	4	
Monitor	24	0.0032	4	

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer-specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

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## **SOURCES**

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1) **ENERGY STAR Office Equipment Calculator**

<http://www.energystar.gov/sites/default/files/asset/document/Office%20Equipment%20Calculator.xlsx> (Referenced latest version released in October 2016). Default values were used. Using a commercial office equipment load shape, the percentage of total savings that occur during the PJM peak demand period was calculated and multiplied by the energy savings. As of December 1, 2018, the published ENERGY STAR Office Equipment Calculator does not reflect the current specification for computers (ENERGY STAR® Program Requirements Product Specification for Computers Eligibility Criteria Version 7.1). V7.1 introduced modest improvements to both desktop and laptop computer efficiency. As a result, the savings values for computers presented in this measure entry reflect savings for V6-compliant models. This characterization should be updated when an updated ENERGY STAR Office Equipment Calculator becomes available.

### 2.5.22.5.1 ADVANCED POWER STRIPS

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Per Advanced Power Strip
<b>Measure Life</b>	5 years <sup>Source-4</sup>
<b>Measure Life</b>	5 years <sup>1</sup>
<b>Vintage</b>	Retrofit

Advanced Power Strips (APS) are surge protectors that contain a number of power-saver sockets. ~~There are two types of APS: Tier 1 and Tier 2. This measure develops equipment savings for both Tier 1 and Tier 2 APS installed for residential home entertainment centers (HEC) or home office applications.~~

Tier 1 APS have a master control socket arrangement and will shut off the items plugged into the controlled power-saver sockets when they ~~sense that~~ identify the appliance plugged into the master socket has been turned off. Conversely, the appliance plugged into the master control socket has to be turned on and left on for the devices plugged into the power-saver sockets to function.

Tier 2 APS deliver additional functionality beyond that of a Tier 1 unit, as Tier 2 units manage both standby and active power consumption. The Tier 2 APS manage standby power consumption by turning off devices from a control event; this could be a TV or other item powering off, which then powers off the controlled outlets to save energy. Active power consumption is managed by the Tier 2 unit by monitoring a user's engagement or presence in a room by either or both infrared remote signals sensing or motion sensing. ~~If after~~After a period of user absence or inactivity, The Tier 2 unit will shut off all items plugged into the controlled outlets, thus saving energy. There are two types of Tier 2 APS available on the market. Tier 2 Infrared (IR) detect signals sent by remote controls to identify activity, while Tier 2 Infrared-Occupancy Sensing (IR-OS) use remote signals as well as an occupancy sensing component to detect activity and sense for times to shut down. Due to uncertainty surrounding the differences in savings for each technology, the Tier 2 savings are blended into a single number.

#### ELIGIBILITY

This protocol documents the energy savings attributed to the installation of ~~Advanced Power Strips-APS~~. The most likely area of application is in residential spaces, i.e. single-family and multifamily homes. However, commercial applications are also appropriate for Advanced Power Strips (see Volume 3, Section 3.9.31 Advanced Power Strip Plug Outlets-[http://www.puc.pa.gov/filing\\_resources/issues\\_laws\\_regulations/act\\_129\\_information/technical\\_reference\\_manual.aspx](http://www.puc.pa.gov/filing_resources/issues_laws_regulations/act_129_information/technical_reference_manual.aspx)). The protocol considers usage of Advanced Power Strips ~~with home office systems~~for HEC and home ~~entertainment systems~~offices.

#### ALGORITHMS

The energy savings and demand reduction for Tier 1 and Tier 2 APS outlets are obtained from several recently conducted field studies, with the savings estimates applied to measured in-service rates (ISR) and realization rates (RR) to determine final savings.

The energy savings and demand reduction are calculated for both ~~home office~~HEC and home ~~entertainment office~~ use for Tier 1 strips, ~~and only for home entertainment use for Tier 2 strips.~~<sup>79</sup> ~~For Tier 1 strips, if~~ When possible, identify the equipment connected to the APS and apply the

<sup>79</sup> Tier 2 strips are typically installed only in home entertainment center applications.



associated energy reduction percentage (ERP). If the intended use of the power strip for a Tier 1 APS is not specified, or if multiple power strips are purchased, the algorithm for “unspecified use” should be applied. If it is known that the power strip is intended to be used for an entertainment center, the “entertainment center” algorithm should be applied, while the “home office” algorithm should be applied if it is being used in a home office setting. For Tier 2 strips, the end use is assumed to be a home entertainment center and the savings vary. Values for “unspecified use” are based on the type of Tier 2 strip, IR, IR-OS, or unspecified. Tier 2 APS savings are only identified for HEC as this is where they are typically installed for residential use.

**Tier 1 Advanced Power Strip:**

$$\Delta kWh_{t1\_unspecified} = Annual\_Usage_{unspecified} \times ERP_{t1\_unspecified} \times ISR \times RR$$

$$\Delta kWh_{t1\_entertainment} = Annual\_Usage_{entertainment} \times ERP_{t1\_entertainment} \times ISR \times RR$$

$$\Delta kWh_{t1\_office} = Annual\_Usage_{office} \times ERP_{t1\_office} \times ISR \times RR$$

$$\Delta kW_{peak, t1\_unspecified} = Load_{unspecified} \times ERP_{peak, t1\_unspecified} \times ISR$$

$$\Delta kW_{peak, t1\_entertainment} = Load_{entertainment} \times ERP_{peak, t1\_entertainment} \times ISR$$

$$\Delta kW_{peak, t1\_home\ office} = Load_{office} \times ERP_{peak, t1\_office} \times ISR$$

$$\Delta kWh = Annual\_Usage \times ERP_{T1} \times ISR \times RR$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDf_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDf_w$$

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**Tier 2 Advanced Power Strips:**

$$\Delta kWh_{t2} = Annual\_Usage_{entertainment} \times ERP_{t2} \times ISR \times RR$$

$$\Delta kW_{peak, t2} = Load_{entertainment} \times ERP_{peak, t2} \times ISR$$

**DEFINITION OF TERMS**

$$\Delta kWh = Annual\_Usage \times ERP_{T2} \times ISR \times RR$$

$$\Delta kW_{summer\ peak} = \Delta kWh \times ETDf_s$$

$$\Delta kW_{winter\ peak} = \Delta kWh \times ETDf_w$$

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**DEFINITION OF TERMS**

Table 2-127: Terms, Values, and References for Advanced Power Strips

Parameter	Unit	Value	Source
<i>Annual_Usage<sub>entertainment</sub></i> , Annual usage of home entertainment system <i>Annual_Usage</i>	kWh	474 See Table 2-128	13
<i>Annual_Usage<sub>office</sub></i> , Annual usage of home office system	kWh	399	4

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<i>Annual_Usage<sub>unspecified</sub></i> , Annual usage of unspecified end-use <sup>80</sup>	kWh	449	4
<i>Load<sub>entertainment</sub></i> , Demand of home entertainment system	kW	0.058	3
<i>Load<sub>office</sub></i> , Demand of home office system	kW	0.044	3
<i>Load<sub>unspecified</sub></i> , Demand of unspecified end-use	kW	0.052	3
<i>ERP<sub>energy</sub></i> , energy reduction percentage	%	See Table 2-107	4
<i>ERP<sub>peak</sub></i> , energy reduction percentage during peak period	%	See Table 2-107	4
<i>ISR</i> , In-service Rate	%	EDC Data Collection or see Table 2-107 Default = 72%	24
<i>RR</i> , Realization Rate	kWh%	0.92%	23
<i>ERP<sub>energy</sub></i> , energy reduction percentage	%	See Table 2-129	3
<i>ETDF<sub>s</sub></i> , Summer energy to demand factor	$\frac{kW}{kWh}$	0.0001136	5
<i>ETDF<sub>w</sub></i> , Winter energy to demand factor	$\frac{kW}{kWh}$	0.0001463	5

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The following table shows the Energy Reduction Percentage (ERP) and In-Service Rate (ISR) for each strip type and end use.

Table 2-128: Impact Factors for Advanced Power Strip Types: Annual Usage by End-use

Strip Type	End-Use	ERP Annual Usage (kWh)	ERP <sub>peak</sub>	ISR
Tier 1	Home Entertainment Center	27%471	20%	86%
Tier 1	Home Office	21%399	18%	86%
Tier 1	Unspecified	25%449	19%	86%
Tier 2	Home Entertainment Center	44%	41%	74%

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**DEFAULT SAVINGS**

Table 2-129: Default Savings Impact Factors for Advanced Power Strips Strip Types

APSS Strip Type	End-Use	Energy Savings (kWh) ERP <sub>s</sub>	Peak Demand Reduction (kW)
Tier 1	Home Entertainment Center	100.627%	0.010
Tier 1	Home Office	66.321%	0.007
Tier 1	Unspecified — use or multiple purchased	88.825%	0.009
Tier 2	Home Entertainment Center	141.144%	0.018

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**DEFAULT SAVINGS**

<sup>80</sup> Note that this was based on the MA RPLNC 173 APS Metering Study that determined Tier 1 APS to be used in home entertainment settings 69% of the time, and 31% in home office environments.

**Table 2-130: Default Savings for Advanced Power Strips**

<u>APS Type</u>	<u>End Use</u>	<u>Energy Savings (<math>\Delta kWh</math>)</u>	<u>Summer Peak Demand Reduction (<math>\Delta kW_{summer\ peak}</math>)</u>	<u>Winter Peak Demand Reduction (<math>\Delta kW_{winter\ peak}</math>)</u>
<u>Tier 1</u>	<u>Home Entertainment Center (HEC)</u>	<u>84.2</u>	<u>0.010</u>	<u>0.012</u>
<u>Tier 1</u>	<u>Home Office</u>	<u>55.5</u>	<u>0.006</u>	<u>0.008</u>
<u>Tier 1</u>	<u>Unspecified use or multiple purchased</u>	<u>74.4</u>	<u>0.008</u>	<u>0.011</u>
<u>Tier 2</u>	<u>Home Entertainment Center (HEC)</u>	<u>137.3</u>	<u>0.016</u>	<u>0.020</u>

**EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of installation coupled with assignment of stipulated energy savings.

**SOURCES**

- 1) ~~“RLPNC 17-3: Advanced California Electronic Technical Reference Manual. “Smart Connected Power Strip Metering Study,”. SWAP010-10. Accessed January 2024. Weblink [http://ma-eeac.org/wordpress/wp-content/uploads/RLPNC\\_173\\_APSMeteringReport\\_Revised\\_18March2019.pdf](http://ma-eeac.org/wordpress/wp-content/uploads/RLPNC_173_APSMeteringReport_Revised_18March2019.pdf)~~
- 2) ~~“(2018, October). “RLPNC 17-4 and 17-5: Products Impact Evaluation of In-service and Short-Term Retention Rates Study,” Massachusetts Programs Administrators and EEAC, (Oct. 2018),” [http://ma-eeac.org/wordpress/wp-content/uploads/RLPNC\\_1745\\_APSProductsSurveys\\_5Oct2018\\_Final.pdf](http://ma-eeac.org/wordpress/wp-content/uploads/RLPNC_1745_APSProductsSurveys_5Oct2018_Final.pdf) Weblink~~
- 3) ~~As reported in correspondence with authors of Source 1 and Source 2.~~
- 4) ~~California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.~~

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- 3) [NMR Group for Massachusetts Program Administrators and EEAC. \(2019, March\). "RLPNC 17-3: Advanced Power Strip Metering Study," pg. 3, Table 1. Weblink](#)
- 4) [Survey and on-site analysis of 17,718 APS installed in Pennsylvania PY13 and PY14 kit and direct install programs.](#)
- 5) [Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Residential, plug-loads Weblink](#)

## 2.6 BUILDING SHELL

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### 2.6.1 RESIDENTIAL AIR SEALING

Target Sector	Residential <del>Establishments</del> , limited to single family detached houses
Measure Unit	Residential Air Sealing
Measure Life	15 years <sup>Source 51</sup>
Vintage	Retrofit

Thermal shell air leaks are sealed through strategic use and installation of air-tight materials. Leaks are detected and leakage rates measured with the assistance of a blower-door test. This measure applies to the sealing of thermal shell air leaks in existing residential homes with a primary electric heating and/or cooling source.

#### ELIGIBILITY

This measure is applicable to single family detached (including manufactured and mobile homes) houses only.

The baseline for this measure is the existing air leakage as determined through approved and appropriate ~~test methods using a~~ blower door ~~testing methods~~. The baseline condition of a building upon first inspection significantly impacts the opportunity for cost-effective energy savings through air-sealing.

Air sealing materials and diagnostic testing should meet all qualification criteria for program eligibility. The initial and final tested leakage rates should be performed in such a manner that the identified reductions can be properly discerned, particularly in situations where multiple building envelope measures may be implemented simultaneously.

For example, if air sealing, duct sealing and insulation are all installed as a whole home retrofit, efforts should be made to isolate the CFM reductions ~~from of~~ each measure ~~individually~~. This may require performance of a blower door test between each measure installation. Alternatively, the baseline blower door test may be performed after the duct sealing is completed, then air sealing measures installed and the retrofit blower door test completed prior to installation of the new insulation.

In addition, ~~seasonal savings are capped at 40% of the building's heating/cooling load~~. <sup>Source 62</sup>

$$\Delta kWh_{cool} \leq 40\% \times CAPY_{cool} \times EFLH_{cool} \times \eta_{base}$$

$$\Delta kWh_{heat} \leq 40\% \times CAPY_{heat} \times EFLH_{heat} \times \eta_{base}$$

Furthermore, if:

$$CFM50_{ee} < \frac{3 ACH50 \times CondVol}{60 \text{ min/hr}}$$

additional testing and intervention is necessary to ensure adequate ventilation for occupants and combustion equipment. <sup>Source 3</sup> Lower rates can increase savings, but may require the introduction of new mechanical ventilation. The operating energy of this new equipment, as well as the energy loss from the induced ventilation should be deducted from the savings of this measure. In other

words. CFM50<sub>ee</sub> has an effective minimum equivalent to 3 ACH50 unless energy recovery ventilation is employed.

Finally, to ensure that the alterations do not result in a backdraft, post air-sealing combustion appliance zone (CAZ) testing should be considered for any homes with Category I (gravity-draft) exhaust equipment that undergo a significant reduction in infiltration.

## ALGORITHMS

To calculate  $\Delta kWh$  add together the cooling and heating savings calculated using the appropriate coefficients from Table 2-111 and Table 2-112 Table 2-132 and Table 2-133 for the matching equipment type and climate region in the algorithm below. For example, if a residence has gas heat with Central AC, there is no heating component to the savings calculations. If a residence has Electric Resistance heating and no AC, calculate the savings for “Baseboard” heating. Ductless installations such as baseboards and mini-split heat pumps should substitute 100% for  $\frac{Duct_{proto}}{Duct_{base}}$ . Values for  $Duct_{base}$  may be generated through measurement or by selecting an appropriate value from Table 2-31 Table 2-40 in Sec. 2.2.10.

The prototype variables in the savings equations for this measure do not refer to the baseline or efficient conditions of the home undergoing improvement. Instead, expressions of the form  $\frac{proto}{base}$  are used to scale the savings of the home being improved (*base*) to those of the prototype home which was based on statewide averages from the 20182022 Residential Baseline Study and used to derive the regressions below. This scaling accounts for differences in energy consumption resulting in deviations in HVAC equipment and distribution system efficiencies from those of the Baseline.

$$\Delta kWh_{cool} = \frac{\eta_{proto}}{\eta_{base}} \times \frac{Duct_{proto}}{Duct_{base}} \times \left( \frac{a_{cool}}{100,000} \times (CFM50_{base}^2 - CFM50_{ee}^2) + b_{cool} \times (CFM50_{base} - CFM50_{ee}) \right)$$

$$\Delta kWh_{heat} = \frac{\eta_{proto}}{\eta_{base}} \times \frac{Duct_{proto}}{Duct_{base}} \times \left( \frac{a_{heat}}{100,000} \times (CFM50_{base}^2 - CFM50_{ee}^2) + b_{heat} \times (CFM50_{base} - CFM50_{ee}) \right)$$

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{summer\ peak} = \Delta kWh_{cool} \div EFLH_{cool} \times CFCF_{cool}$$

$$\Delta kWh_{winter\ peak} = \Delta kWh_{heat} \div EFLH_{heat} \times CF_{heat}$$

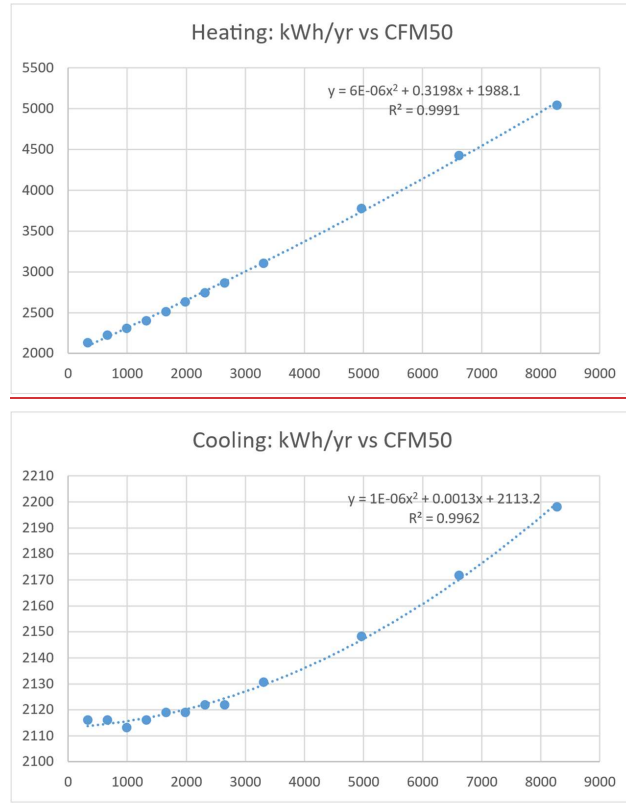
Note: The savings equations above are based on *quadratic* regressions because cooling the change in energy savings fall off quickly with changes for the same reduction in infiltration in heating dominated climates, whereas some heating technologies exhibit escalating savings varies with the initial condition, as in the well as climate and HVAC technology. In general, there is a larger benefit for an equivalent reduction of CFM50 in a home when tightening very loose building shells compared to homes with a lower initial infiltration rate. For example plot below. This, when starting from 6600 CFM50 in Figure 2-1, a 1650 CFM50 reduction yields 24 kWh/yr savings whereas starting from 2300 CFM50 results in small 9 kWh/yr savings. Since the coefficients for the squared infiltration reduction term, which are therefore so small, they are multiplied by 10<sup>5</sup> to simplify Table 2-111 and Table 2-112. Table 2-132 and Table 2-133. This scaling is later reversed in the savings calculations.

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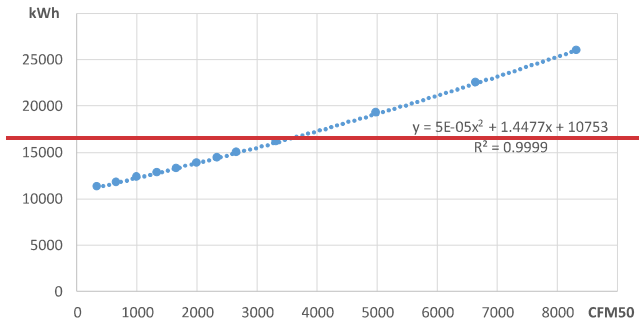
**Figure 2-1: Example Regressions for Ductless Mini-splits in Climate Region AD**



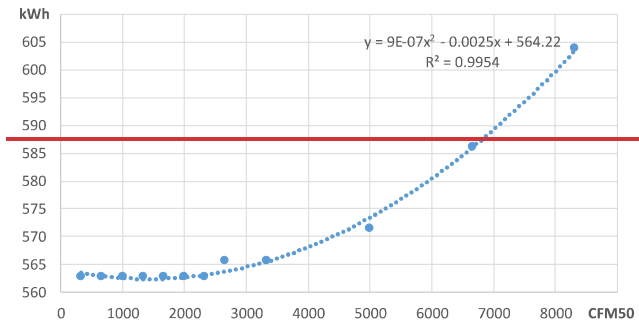
**DEFINITION OF TERMS**

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Heating: kWh per CFM50



Cooling: kWh per CFM50



**DEFINITION OF TERMS**

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Table 2-131: Terms, Values, and References for Residential Air Sealing

Term	Unit	Values	Source
$CFM50_{base}$ , Baseline infiltration at 50 Pa	$CFM_{50}$	Measured, EDC Data Gathering	EDC Data Gathering
$CFM50_{ee}$ , Infiltration at 50 Pa post air sealing	$CFM_{50}$	Measured, EDC Data Gathering	EDC Data Gathering
<i>CondVol</i> ; Conditioned volume of the home	<i>ft<sup>3</sup></i>	<u>Measured, EDC Data Gathering</u>	<u>EDC Data Gathering</u>
$Duct_{base}$ , Baseline duct efficiency	<i>None</i>	EDC Data Gathering: measured value, or appropriate value selected from <u>Table</u>	EDC Data Gathering

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		2-34 Table 2-40 in Sec. 2.2.92.2.10	
$Duct_{proto}$ , Prototype duct efficiency	<i>None</i>	Default: See Table 2-34 Table 2-40 in Sec. 2.2.92.2.10 for "R-2 Average Basement + 50% Conditioned"	14
$\eta_{base}$ , Baseline equipment efficiency	<i>varies</i>	Measured, EDC Data Gathering Default: $\eta_{proto}$	EDC Data Gathering
$\eta_{proto}$ , Prototype equipment efficiency	<i>varies</i>	See Table 2-110 See Table 2-151 in 2.6.5	25
$a_{system}$ , Unit Energy Savings per CFM50 <sup>2</sup> of air leakage reduction	$\frac{kWh/yr}{CFM_{50}^2}$	See Table 2-132	36
$b_{system}$ , Unit Energy Savings per CFM50 of air leakage reduction	$\frac{kWh/yr}{CFM_{50}}$	See Table 2-133	36
$EFLH_{cool}$ , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{yr}$	See $EFLH_{cool}$ in Vol. 1, App. A	47
$EFLH_{cool}$ , $EFLH_{heat}$ , Equivalent Full Load Cooling Hours of operation during the heating season for the average unit	$\frac{hours}{year}$	See $EFLH_{cool}$ , $EFLH_{heat}$ in Vol. 1, App. A	47
$CF_{demand}$ , Demand Coincidence Factor	<i>Proportion</i>	See $Summer CF$ in Vol. 1, App. A	47
$CF_{winter peak}$ , Winter demand Coincidence Factor	<i>Proportion</i>	See $Winter CF$ in Vol. 1, App. A	1
$CAPY_{cool}$ , The cooling capacity of the equipment being installed <sup>81</sup>	$kBTU/hr$	EDC Data Gathering	AEPS Application; EDC Data Gathering
$CAPY_{heat}$ , The heating capacity of the heat pump being installed <sup>82</sup>	$kBTU/hr$	EDC Data Gathering	AEPS Application; EDC Data Gathering

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### DEFAULT UNIT ENERGY SAVINGS COEFFICIENT & EQUIPMENT EFFICIENCY TABLES

Savings may be claimed using the algorithms above and the algorithm's input default values below, in conjunction with customer-specific blower door test data. Site specific data from blower door

<sup>81</sup> This data is obtained from the AEPS Application Form or EDC's data gathering based on the model number.  
<sup>82</sup> Ibid. This refers to the capacity of the heat pump and not any auxiliary electric resistance heat.

testing is required to be used in conjunction with these default energy savings values, as outlined in the algorithms.

**Table 2-132: Default Residential Equipment Efficiency**

	Cooling				Heating				
	ASHP	Central AC	Mini-split	GSHP	ASHP	Base-board	Electric Furnace	Mini-split	GSHP
Efficiency	15	12.1	14.9	16.6	8.5	1	1	8.9	3.6
Units	SEER	SEER	SEER	EER	HSPF	GOP	GOP	HSPF	GOP

**Table 2-143: Default Unit Energy Savings per Reduced CFM50<sup>2</sup> for Air Sealing**

Climate Region Reference City	<i>a<sub>cool</sub></i>				<i>a<sub>heat</sub></i>				
	ASHP	Central AC	GSHP Mini-split	GSHP Mini-split	ASHP	Base-board	Electric Furnace	GSHP Mini-split	Mini-split GSHP
C Allentown	0.042062	0.076021	0.09028	0.023097	5.0641445	1.166790	3.485317	0.9441396	0.413909
A Binghamton	0.028000	0.018086	0.087061	1.648046	3.3351159	1.2710103	4.6530287	0.986789	0.2931232
G Bradford	0.0432255	0.022660	0.0671547	0.064326	0.1121828	1.5155151	4.545540	1.173831	0.283709
I Erie	0.022062	0.004067	0.058021	0.027059	5.670952	1.318803	4.3091467	1.066706	0.3671314
E Harrisburg	0.079067	0.1251906	0.126013	0.066641	4.4801722	1.2423238	3.4804584	0.8862131	0.1121141
D Philadelphia	0.08148	0.121162	0.096202	0.002111	3.0780830	1.0043626	2.208806	0.792647	0.286649
H Pittsburgh	0.014000	0.053026	0.075	0.079068	4.6571264	1.1852548	2.778277	0.93940	0.4971405
B Scranton	0.004031	0.029023	0.086049	0.058068	4.845142	1.212354	4.0732606	0.958990	0.4111316
F Williamsport	0.03703	0.032020	0.104070	0.052067	5.1751921	1.1814028	3.4774553	0.9251740	0.3921662

**Table 2-133: Default Unit Energy Savings per Reduced CFM50 for Air Sealing**

Climate Region Reference City	<i>b<sub>cool</sub></i>				<i>b<sub>heat</sub></i>				
	ASHP	Central AC	GSHP Mini-split	Mini-split GSHP	ASHP	Base-board	Mini-split Electric Furnace	Electric Furnace GSHP	Mini-split GSHP
C Allentown	0.025021	0.033020	0.004007	0.007014	0.951833	1.966943	0.8642179	2.1380684	0.616553
A Binghamton	0.004000	0.004010	0.002014	0.007222	1.948141	2.393527	1.4482702	2.5990875	0.788795

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The heating or cooling loads for each system combination were then fitted with separate quadratic regressions, the coefficients of which are the UES values. Supporting files can be found at [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE\\_Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE_Phase3_Res_Baseline_Study_Rpt021219.pdf), used to calculate energy savings.

- 7) ~~Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service, <https://www.ecobee.com/donateyourdata/Weblink>.~~
- 4) ~~\_\_\_\_\_~~
- 5) ~~Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, GDS Associates, 2007~~
- 6) ~~"Residential Heating and Cooling Loads Component Analysis", Lawrence Berkley National Laboratory Building Technologies Department, 1999, <https://simulationresearch.lbl.gov/dirpubs/44636.pdf>~~

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## 2.6.2 WEATHER STRIPPING, CAULKING, AND OUTLET GASKETS

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Per Project
<b>Measure Life</b>	15 years
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit

Residential structures can lose significant amounts of heat through the infiltration of unconditioned outside air into the conditioned space. Infiltration enters conditioned spaces in a variety of ways: building joints, gaps in door and window frames, basement and attic penetrations (electrical and plumbing) and recessed light fixtures. Air sealing measures like adding weather stripping, caulking and installing outlet gaskets can reduce the amount of infiltration and the related heating and cooling for a building.

### ELIGIBILITY

To be eligible:

- Weather stripping must be installed on doors, windows, or attic hatches/doors.
- Caulking and/or spray foam sealant must be applied to window frames, door frames or plumbing/electrical penetrations.
- Gaskets must be installed on electrical outlets.

In addition, **this measure is limited to projects with less than 400 kWh of savings**. Projects with 400 kWh or more of savings should follow the Residential Air Sealing Residential Air Sealing section.

### ALGORITHMS

There are two approaches that can be utilized to estimate savings due to air sealing, one using algorithms requiring EDC data gathering, and a default savings method when data are unavailable. The annual energy and peak demand savings are obtained through the following formulas:

$$\Delta kW_{cool} = \frac{1.08 \times \Delta CFM_{50} \times CDD \times 24 \frac{hr}{day} \times ISR}{N \times SEER \times 1,000 \frac{Wh}{kWh}} \times LM \times DUA$$

$$\Delta kW_{cool} = \frac{1.08 \times \Delta CFM_{50} \times CDD \times 24 \times ISR}{N \times SEER2 \times 1,000} \times LM \times DUA \times F_{RAC} \times \%_{elec}$$

$$\Delta kW_{heat} = \frac{1.08 \times \Delta CFM_{50} \times HDD \times 24 \frac{hr}{day} \times ISR}{N \times HSPF \times 1,000 \frac{Wh}{kWh}}$$

$$\Delta kW_{heat} = \frac{1.08 \times \Delta CFM_{50} \times HDD \times 24 \times ISR}{N \times HSPF2 \times 1,000} \times \%_{elec}$$

$$\Delta kW_{h} = (\Delta kW_{cool} + \Delta kW_{heat}) < 400 kWh \quad \underline{\text{if}} > 400 kWh \text{ use Sec. 2.6.1}$$

$$\Delta kW_{summer\ peak} = \Delta kW_{cool} \times PCFETDF_{summer}$$

$$\Delta kW_{winter\ peak} = \Delta kW_{heat} \times ETDF_{winter}$$

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**Ground Source Heat Pumps (GSHP)**

GSHP efficiencies are typically calculated differently than air-source units

**Ground Source Heat Pumps (GSHP)**

GSHP efficiencies are typically calculated differently than air-source units, baseline and qualifying unit efficiencies should be converted as follows ~~should be converted as follows:~~

$$SEER = EER_g \times GSHPDF \times \cancel{GSEER}$$

$$HSPF = COP_g \times GSHPDF \times 3.412 \frac{\text{BTU}}{\text{W-h}}$$

**PTAC and PTHP**

$SEER = EER$

**DEFINITION OF TERMS**

$HSPF = COP_g \times GSHPDF \times 3.412 \frac{BTU}{Wh}$

**PTAC and PTHP**

$SEER = EER$

**DEFINITION OF TERMS**

Table 2-134: Terms, Values, and References for Weather Stripping

Term	Unit	Values	Source
$\Delta kWh_{cool}$ , Annual cooling energy savings	<i>kWh/year</i>	Calculated	-
$\Delta kWh_{heat}$ , Annual heating energy savings	<i>kWh/year</i>	Calculated	-
1.08, Conversion factor that converts CFM air (at 70°F) to BTU/hr-°F	$\frac{BTU \times min}{hr \times ^\circ F \times ft^3}$	1.08	-
$\Delta CFM_{50}$ , Reduction in air leakage at a test pressure of 50 Pascals	CFM	See Table 2-137	4, 42, 3
CDD, Cooling degree-days	°F-day/year	See CDD values in Vol. 1, App. A	404
HDD, Heating degree-days	°F-day/year	See HDD values in Vol. 1, App. A	404
ISR, In-service rate	None	Kit delivery: EDC Data Gathering Default: Direct install = 1 Kit delivery = 0.16	EDC Data Gathering 5
LM, Latent multiplier to convert the calculated sensible load to the total (sensible and latent) load	None	See Table 2-136	56
DUA, Discretionary use adjustment to account for uncertainty in predicting cooling system usage patterns of occupants	None	0.75	37
$F_{RAC}$ , Adjustment factor to relate sealed area to area served by room air conditioners	None	If Room AC = 0.24 If non-Room AC = 1.0	8
$\%_{cool}$ , percent of homes with comfort cooling	None	EDC Data Gathering Default = 67%	9
N, Correlation factor. This factor accounts for four environmental characteristics that may influence infiltration, which include climate,	None	See Table 2-135 Default = 16.7	210

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building height, wind shielding and building leakiness			
<del>SEER</del> , <del>SEER2</del> , Cooling system seasonal efficiency	$\frac{Btu}{W \cdot h}$	EDC Data Gathering Default: Gathering Default: 13.9, or See Early Replacement values in Table 2-10 in Sec. 2-2.42.2.1	711, 15
% <del>elec</del> , percent of homes with electric primary heating fuel	None	EDC Data Gathering Default = 36%	9
<del>HSPF</del> , <del>HSPF2</del> , Heating system seasonal efficiency	$\frac{Btu}{W \cdot h}$	EDC Data Gathering Default: 7.75, or See Early Replacement values in Table 2-10 in Sec. 2-2.42.2.1	711, 15
<del>ETDF<sub>summer</sub></del> , Summer energy to demand factor	kW/kWh	0.0005272	12
<del>ETDF<sub>winter</sub></del> , Winter energy to demand factor	kW/kWh	0.0003398	12
<del>EER</del> <del>EERg</del> , Energy Efficiency Ratio of a GSHP, this is measured differently than EER of an air source heat pump and must be converted	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default = 17.1	-13
<del>GOP</del> <del>COP</del> , Coefficient of Performance. This is a measure of the efficiency of a ground source heat pump	None	EDC Data Gathering Default = 3.6	-13
<del>GSEER</del> , Factor used to determine the SEER of a GSHP based on its EERg	$\frac{BTU}{W \cdot h}$	4.02	8
<del>GSPK</del> , Factor to convert EERg to the equivalent EER of an air conditioner to enable comparisons to the baseline unit	Proportion	0.8416	8
<del>GSHPDF</del> , Ground Source Heat Pump De-rate Factor	Proportion	0.885	914
<del>PCF</del> , Peak demand savings conversion factor	kW/kWh	0.000017 (1.7 × 10 <sup>-5</sup> )	6

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Table 2-135: Correlation Factor <sup>Source 210</sup>

Shielding/Stories	1	1.5	2	3
Well-shielded	22.2	20.0	17.8	15.5
Normal	18.5	16.7	14.8	13.0
Exposed	16.7	15.0	13.3	11.7



**Table 2-136: Latent Multiplier Values by Climate Reference City** [Source 6](#)

Climate Region	Reference City	LM
C	Allentown	9.0
A	Binghamton, NY	6.75
G	Bradford	16.0
I	Erie	13.0
E	Harrisburg	5.6
D	Philadelphia	7.8
H	Pittsburgh	7.3
B	Scranton	9.3
F	Williamsport	9.5

**Table 2-137: Typical Reductions in Leakage** [Source 1](#)[Sources 2,3](#)

Technology	Application	$\Delta$ CFM50 <a href="#">Source 45</a>
Weather Stripping	Single Door	25.5 CFM/door
	Double Door	0.73 CFM/ft <sup>2</sup>
	Casement Window	0.036 CFM/lf of crack
	Double Horizontal Slider, Wood	0.473 CFM/lf of crack
	Double-Hung	1.618 CFM/lf of crack
	Double-Hung, with Storm Window	0.164 CFM/lf of crack
	Average Weatherstripping	0.639 CFM/lf of crack
Caulking	Piping/Plumbing/Wiring Penetrations	10.9 CFM each
	Window Framing, Masonry	1.364 CFM/ft <sup>2</sup>
	Window Framing, Wood	0.382 CFM/ft <sup>2</sup>
	Door Frame, Masonry	1.018 CFM/ft <sup>2</sup>
	Door Frame, Wood	0.364 CFM/ft <sup>2</sup>
	Average Window/Door Caulking	0.689 CFM/lf of crack
<i>Average Window/Door Caulking and Weather Stripping</i>		<i>0.664 CFM/lf of crack</i>
Gasket	Electrical Outlets	6.491 CFM each

## DEFAULT SAVINGS

If the information needed to utilize the algorithms is unavailable, the default savings listed below may be used. The default savings are based on a home with a [12.413.9](#) SEER CAC and electric resistance heat (COP=1). ~~The default savings assume direct install~~ [heating HSPF](#) of measures. ~~To~~

use default savings for kit delivery measures, EDCs must determine an ISR multiplier through independent research, 7.75. <sup>Source 15</sup>

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Table 2-138, Table 2-139, Table 2-140 present default savings for direct install measures. These savings assume an ISR of 1.0. Cooling savings assume the home has comfort cooling and heating savings assume the home has electric heating.

Table 2-141, Table 2-142, and Table 2-143 present default savings for measures delivered via kit. These savings assume an ISR of 0.16, %<sub>cool</sub> of 0.67 and %<sub>elec</sub> of 0.36. <sup>Source 5, Source 9</sup>

**Table 2-138: Default Annual Energy Savings – Direct Installation**

Climate Region	Reference City	Cooling Savings (kWh)			Heating Savings (kWh)		
		Caulked Penetrations (per pen.)	Weather Stripping, Caulking and Sealing (per 10 lf)	Outlet Gaskets (per gasket)	Caulked Penetrations (per pen.)	Weather Stripping, Caulking and Sealing (per 10 lf)	Outlet Gaskets (per outlet)
C	Allentown	8.618	5.250	5.132	11.199	6.822	6.669
A	Binghamton, NY	2.471	1.505	1.471	15.300	9.321	9.111
G	Bradford	4.148	2.527	2.470	15.667	9.544	9.330
I	Erie	9.529	5.805	5.675	12.596	7.673	7.501
E	Harrisburg	6.349	3.868	3.781	10.666	6.497	6.352
D	Philadelphia	10.324	6.289	6.148	9.489	5.781	5.651
H	Pittsburgh	5.731	3.491	3.413	11.869	7.230	7.068
B	Scranton	7.190	4.380	4.282	12.166	7.411	7.245
F	Williamsport	7.519	4.580	4.477	12.176	7.418	7.251

**Table 2-139: Default Summer Peak Demand Savings – Direct Installation**

Climate Region	Reference City	Caulked Penetrations (ΔkW/pen.)	Weather Stripping, Caulking and Sealing (ΔkW/10 lf)	Outlet Gaskets (ΔkW/gasket)
C	Allentown	0.0045676	0.0027824	0.0027200
A	Binghamton, NY	0.0013095	0.0007977	0.0007798
G	Bradford	0.0021984	0.0013392	0.0013092
I	Erie	0.0050504	0.0030766	0.0030075
E	Harrisburg	0.0033649	0.0020498	0.0020038
D	Philadelphia	0.0054718	0.0033333	0.0032585
H	Pittsburgh	0.0030373	0.0018502	0.0018087
B	Scranton	0.0038110	0.0023215	0.0022694
F	Williamsport	0.0039848	0.0024275	0.0023730

**Table 2-140: Default Winter Peak Demand Savings – Direct Installation**

Climate Region	Reference City	Caulked Penetrations (ΔkW/ pen.)	Weather Stripping, Caulking and Sealing (ΔkW/10 lf)	Outlet Gaskets (ΔkW/gasket)
C	Allentown	0.0038075	0.0023194	0.0022674
A	Binghamton, NY	0.0052021	0.0031690	0.0030979
G	Bradford	0.0053268	0.0032449	0.0031721
I	Erie	0.0042825	0.0026088	0.0025503
E	Harrisburg	0.0036264	0.0022091	0.0021595
D	Philadelphia	0.0032264	0.0019654	0.0019213
H	Pittsburgh	0.0040354	0.0024582	0.0024031
B	Scranton	0.0041363	0.0025197	0.0024632
F	Williamsport	0.0041400	0.0025220	0.0024654

**Table 2-141: Default Annual Energy Savings – Kit Delivery**

Climate Region	Reference City	Cooling Savings (kWh)			Heating Savings (kWh)		
		Caulked Penetrations (per pen.)	Weather Stripping, Caulking and Sealing (per 10 lf)	Outlet Gaskets (per gasket)	Caulked Penetrations (per pen.)	Weather Stripping, Caulking and Sealing (per 10 lf)	Outlet Gaskets (per outlet)
C	Allentown	7.3170.924	4.4570.563	4.3570.550	28.1780.645	17.1650.393	16.7809.384
A	Binghamton, NY	2.8750.265	1.7520.161	1.7120.158	34.9970.881	21.3190.537	20.8410.525
G	Bradford	3.4330.445	2.0910.271	2.0440.265	40.9300.902	24.9330.550	24.3740.537
I	Erie	7.9171.022	4.8230.622	4.7140.608	32.2070.726	19.6190.442	19.1790.432
E	Harrisburg	6.6030.681	4.0220.415	3.9320.405	30.4660.614	18.5590.374	18.1430.366
D	Philadelphia	9.4261.107	5.7420.674	5.6130.659	23.9710.547	14.6020.333	14.2750.325
H	Pittsburgh	5.6660.614	3.4520.374	3.3740.366	29.0140.684	17.6740.416	17.2780.407
B	Scranton	5.9280.771	3.6110.470	3.5300.459	30.5560.701	18.6140.427	18.1960.417
F	Williamsport	7.2840.806	4.4370.491	4.3380.480	28.5810.701	17.4110.427	17.0200.418

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**Table 2-142: Default Summer Peak Demand Savings – Kit Delivery**

Climate Region	Reference City	Caulked Penetrations (ΔkW/ pen.)	Weather Stripping, Caulking and Sealing (ΔkW/10 lf)	Outlet Gaskets (ΔkW/gasket)
C	Allentown	0.0004896	0.0002983	0.0002916
A	Binghamton, NY	0.0001404	0.0000855	0.0000836
G	Bradford	0.0002357	0.0001436	0.0001403
I	Erie	0.0005414	0.0003298	0.0003224
E	Harrisburg	0.0003607	0.0002197	0.0002148
D	Philadelphia	0.0005866	0.0003573	0.0003493
H	Pittsburgh	0.0003256	0.0001983	0.0001939
B	Scranton	0.0004085	0.0002489	0.0002433
F	Williamsport	0.0004272	0.0002602	0.0002544

**Table 2-143: Default Winter Peak Demand Savings – Kit Delivery**

Climate Region	Reference City	Caulked Penetrations (ΔkW/ pen.)	Weather Stripping, Caulking and Sealing (ΔkW/10 lf)	Outlet Gaskets (ΔkW/gasket)
C	Allentown	0.00012440002193	0.00007580001336	0.00007440001306
A	Binghamton, NY	0.00004890002996	0.00002980001825	0.00002940001784
G	Bradford	0.00005840003068	0.00003560001869	0.00003480001827
I	Erie	0.00013460002467	0.00008200001503	0.00008040001469
E	Harrisburg	0.00011220002089	0.00006840001272	0.00006680001244
D	Philadelphia	0.00016020001858	0.00009760001132	0.00009540001107
H	Pittsburgh	0.00009630002324	0.00005870001416	0.00005740001384
B	Scranton	0.00010080002383	0.00006440001451	0.00006000001419
F	Williamsport	0.00012380002385	0.00007540001453	0.00007370001420

## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures. For kit delivery, EDCs should estimate in-service rate through customer surveys.

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- 2) ENERGY STAR Home Sealing Specification, Version Chapter 26: Ventilation and Infiltration, Table 1.0, October 2001.  
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- 3) Energy Center of Wisconsin, "Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research," May 2008.  
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<http://energyconservatory.com/wp-content/uploads/2014/07/Blower-Door-model-3-and-4.pdf>
- 4) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)
- 5) Weighted average of ISRs from surveys of FirstEnergy customers that received outlet gaskets in kits in PY13 and PY14.
- 5) LM values calculated as total load (sensible + latent) divided by sensible load, from sensible and latent values in Harriman et al. (1997, November). ASHRAE Journal "Dehumidification and Cooling Loads from Ventilation Air." ASHRAE Journal, November 1997.  
<https://energy.mo.gov/sites/energy/files/harriman-dehumidification-and-cooling-loads-from-ventilation-air.pdf>
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- 7) For all systems excluding ground source heat pumps: Energy Center of Wisconsin. (2008, May). Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research. Weblink
- 8) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Weblink. Average home conditioned floor area = 2,019 ft<sup>2</sup>; average number of room AC units per home = 1.74; average Room AC capacity = 7,161 BTU/hr. Per ENERGY STAR Room AC sizing chart (Weblink), 7,161 BTU/hr of cooling serves approximately 283 ft<sup>2</sup>.  $F_{RAC} = (283 \text{ ft}^2 \times 1.74)/(2,019 \text{ ft}^2) = 0.24$ .
- 9) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study.  
[http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Due, Pg 111, table 93. Weblink.
- 10) The N factor methodology was developed by Lawrence Berkeley Lab to convert air flow measurements taken at 50 pascal pressure (from blower door tests) to natural air changes. The N factors presented here are taken from Krigger, J. and Dorsi, C. (2004), "Residential Energy: Cost Savings and Comfort for Existing Buildings", pg 284.
- 11) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Pg 115, table 97, pg. 120, table 103. Weblink. Air source heat pump efficiencies calculated using 2023 Pennsylvania Residential Baseline Study data. Federal minimum efficiencies for GSHP due to small sample size for GSHP in residential baseline study.

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- 12) [Wilson et al. 2021. End-Use Load Profiles for the lowest U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink](#)
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- 14) [McQuay. \(2002\). Application Guide 31-008, Geothermal Heat Pump Design Manual. Engineering Estimate - See System Performance of Ground Source Heat Pumps](#)
- 7) 15) [NMR Group for the Pennsylvania Public Utility Commission. \(2024, March\). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Weblink. 7.75 HSPF value is an average performance efficiency of all electric heating systems, including both resistance and heat pump technologies.](#)
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### 2.6.3 CEILING/ATTIC, WALL, FLOOR AND RIM JOIST INSULATION

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Per Project
<b>Measure Life</b>	15 years <sup>Sources 1, 2</sup>
<b>Vintage</b>	Retrofit
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit, New Construction

This protocol covers the calculation of energy and demand savings associated with insulating ceilings/attics, walls, floors above vented crawlspaces, and rim joists in residential buildings with a primary electric heating and/or cooling source.

#### ELIGIBILITY

##### Ceiling/Attic or Wall Insulation

This measure applies to installation/retrofit of new or additional insulation in a ceiling/attic, or walls of existing residential homes ~~or apartment units in multifamily complexes with a primary electric heating and/or cooling source~~. The installation must achieve a finished ceiling/attic insulation rating of R-49 or higher, and/or must add wall insulation of at least an R-6 or greater rating. <sup>Source 12</sup>

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##### Floor Insulation

This measure ~~requires~~ applies to the installation of new insulation to the floors of existing residential buildings with vented (unconditioned) crawlspaces ~~and a primary electric heating and/or cooling source~~. The installation must achieve a finished floor insulation R-value of R-30 or higher, except for homes in IECC Climate Zone 4, where R-19 is permissible. <sup>Source 12</sup>

##### Rim Joist Insulation

This measure ~~protocol~~ applies to the installation of new insulation in the rim joists of residential homes. This includes the rim joists of unvented crawlspaces and the rim joists between the first and second floor of a residence. ~~The insulation should have either a minimum R-10 continuous insulated sheathing on the interior or exterior of the home, or R-13 cavity insulation at the interior of the rim joist. Because of the difficulty of a proper air-sealed installation, using fiberglass batts between the joists is not usually recommended. The insulation should be sprayed foam or rigid foam.~~ <sup>Source 3</sup>

##### Required R-values

For retrofit applications, the new insulation must achieve R-values that meet or exceed ENERGY STAR recommendations. <sup>Source 2</sup> ENERGY STAR guidance is based on the 2021 IECC. <sup>Source 3</sup>

For new construction applications, the insulation must achieve R-values exceeding the 2021 IECC.

#### ALGORITHMS

The annual energy and peak demand savings are obtained through the following formulas. Note that these equations are applied separately for each ceiling / attic, wall, floor, and rim joist component upgraded.

$$\begin{aligned}
 \cancel{DKWh_{cool,component}} \Delta kW h_{cool} &= \left( \frac{1}{R_{base}} - \frac{1}{R_{re}} \right) \times A_{component} \times (1 - FF) A \times (1 - FF) \\
 &\times \frac{24 \frac{hr}{day} \times CDD \times DUA}{SEER \times 1,000 \frac{Wh}{kWh}} \times \frac{24 \times CDD \times DUA}{SEER \times 1,000} \times F_{RAC}
 \end{aligned}$$

$$\Delta kWh_{heat, component} = \left( \frac{1}{R_{base}} - \frac{1}{R_{ee}} \right) \times A_{component} \times (1 - FF) \times A \times (1 - FF) \times F_{RAE} \times AHF \times \frac{24 \frac{hr}{day} \times HDD}{HSPF \times 1,000 \frac{W}{kW}} \times \frac{24 \times HDD}{HSPF \times 1,000}$$

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$$\Delta kWh_{heat} = \Delta kWh_{cool} + \Delta kWh_{heat}$$

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$$\Delta kWh_{summer peak} = \sum_{components} \Delta kWh_{cool} + \Delta kWh_{heat} = \Delta kWh_{cool} \times ETDF_{summer}$$

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$$\Delta kWh_{winter peak} = \frac{\Delta kWh_{cool}}{EFLH_{cool}} \times CF = \Delta kWh_{heat} \times ETDF_{winter}$$

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**Ground Source Heat Pumps (GSHP)**

GSHP efficiencies are typically calculated differently than air-source units, baseline and qualifying unit efficiencies should be converted as follows should be converted as follows:

$$SEER = EER_g \times GSHPDF \times GSER$$

$$HSPF = COP_g \times GSHPDF \times 3.412 \frac{BTU}{Wh}$$

**PTAC and PTHP**

~~PTAC and PTHP~~  
 $SEER = EER$

**DEFINITION OF TERMS**

~~DEFINITION OF TERMS~~

Table 2-144: Terms, Values, and References for Basement Wall Insulation

Term	Unit	Values	Source
$\Delta kWh_{cool}$ , Annual cooling energy savings	kWh/year	Calculated	-
$\Delta kWh_{heat}$ , Annual heating energy savings	kWh/year	Calculated	-
<del><math>R_{base}</math>, R-value of existing insulation</del>	<del><math>^{\circ}F \cdot ft^2 \cdot hr / BTU</math></del>	<del>EDC Data-Gathering Default: Table 2-120</del>	<del>9, 10</del>
<del><math>R_{agg}</math>, R-value of insulation added</del>	<del><math>^{\circ}F \cdot ft^2 \cdot hr / BTU</math></del>	<del>EDC Data-Gathering Default: Table 2-120</del>	<del>9, 10</del>
<del><math>A</math>, Area of component being insulated</del>	<del><math>ft^2</math></del>	<del>EDC Data-Gathering</del>	<del>-</del>
<del><math>FF</math>, Framing factor, designed to account for space that is occupied by framing</del>	<del>None</del>	<del>If externally applied or non-floor component = 0% If studs and cavity = 12%</del>	<del>4</del>
<del><math>CDD</math>, Annual cooling degree-days, base 65°F</del>	<del><math>^{\circ}F \cdot day / year</math></del>	<del>See <math>CDD</math> in Vol 1., App. A</del>	<del>15</del>
<del><math>HDD</math>, Annual heating degree-days, base 65°F</del>	<del><math>^{\circ}F \cdot day / year</math></del>	<del>See <math>HDD</math> in Vol 1., App. A</del>	<del>15</del>
<del><math>EFLH_{cool}</math>, Equivalent full-load cooling hours</del>	<del>Hours/year</del>	<del>See <math>EFLH_{cool}</math> in Vol 1., App. A</del>	<del>14</del>
<del><math>DUA</math>, Discretionary use adjustment to account for uncertainty in predicting cooling system usage patterns of occupants</del>	<del>None</del>	<del>0.75</del>	<del>5</del>
<del><math>SEER</math>, Cooling system seasonal efficiency</del>	<del><math>\frac{Btu}{Wh}</math></del>	<del>EDC Data-Gathering Default: See Early Replacement values in Table 2-8 in Sec. 2.2.1</del>	<del>6</del>

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Term	Unit	Values	Source
<i>HSPF<sub>s</sub></i> , Heating system seasonal efficiency	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: See Early Replacement values in Table 2-8 in Sec. 2.2.1	6
<i>F<sub>AREA}</sub></i> , Adjustment factor to relate insulated area to area served by room air conditioners	None	If Room AC = 0.38 If non-Room AC = 1.0	7
<i>COP<sub>g</sub></i> , Coefficient of Performance. This is a measure of the efficiency of a heat pump	None	EDC Data Gathering	-
<i>EER<sub>g</sub></i> , Energy Efficiency Ratio of a GSHP, this is measured differently than EER of an air source heat pump and must be converted	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default = 16.6	-
<i>GSEER</i> , Factor used to determine the SEER of a GSHP based on its <i>EER<sub>g</sub></i>	$\frac{BTU}{W \cdot h}$	1.02	42
<i>GSPK</i> , Factor to convert <i>EER<sub>g</sub></i> to the equivalent EER of an air conditioner to enable comparisons to the baseline unit	Proportion	0.8416	42
<i>GSHPDF</i> , Ground Source Heat Pump Derate Factor	Proportion	0.885	43
<i>CF</i> , Coincidence factor	None	See <i>CF</i> in Vol. 1, App. A	44
<i>AHF</i> , Adjustment for cooling savings to account for inaccuracies in engineering algorithms.	None	1.21 if adding attic ins., 1.0 if not	8

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$R_{base}$ , <u>R-value of existing insulation</u>	$\frac{^{\circ}\text{F} \cdot \text{ft}^3 \cdot \text{hr}}{\text{BTU}}$	Retrofit: EDC Data Gathering or Default: <u>Table 12</u>	EDC Data Gathering Various
		New Construction: <u>Table 2-146</u>	<u>3</u>
$R_{ee}$ , <u>R-value after adding new insulation</u>	$\frac{^{\circ}\text{F} \cdot \text{ft}^3 \cdot \text{hr}}{\text{BTU}}$	Retrofit: EDC Data Gathering or Default: <u>Table 2-145</u>	EDC Data Gathering <u>2</u>
		New Construction: EDC Data Gathering	
$A$ , <u>Area of component being insulated</u>	$\text{ft}^2$	EDC Data Gathering	-
$FF$ , <u>Framing factor, designed to account for space that is occupied by framing</u>	<u>None</u>	If continuous = 0% If stud-cavity = 25%	<u>11</u>
$CDD$ , <u>Annual cooling degree-days, base 65°F</u>	$^{\circ}\text{F}\text{-day/year}$	See $CDD$ in Vol 1., App. A	<u>12</u>
$HDD$ , <u>Annual heating degree-days, base 65°F</u>	$^{\circ}\text{F}\text{-day/year}$	See $HDD$ in Vol 1., App. A	<u>12</u>
$DUA$ , <u>Discretionary use adjustment to account for uncertainty in predicting cooling system usage patterns of occupants</u>	<u>None</u>	<u>0.75</u>	<u>13</u>
$SEER$ , <u>Cooling system seasonal efficiency</u>	$\frac{\text{BTU}}{\text{W} \cdot \text{h}}$	EDC Data Gathering Default: See Early Replacement or New Construction values (as appropriate) in <u>Table 2-10</u> in Sec. 2.2.1	<u>14</u>
$HSPF$ , <u>Heating system seasonal efficiency</u>	$\frac{\text{BTU}}{\text{W} \cdot \text{h}}$	EDC Data Gathering Default: See Early Replacement or New Construction values (as appropriate) in <u>Table 2-10</u> in Sec. 2.2.1	<u>14</u>
$F_{RAC}$ , <u>Adjustment factor to relate insulated area to area served by room air conditioners</u>	<u>None</u>	If Room AC = <u>0.24</u> If non-Room AC = <u>1.0</u>	<u>15</u>
$COP_g$ , <u>Coefficient of Performance. This is a measure of the efficiency of a ground source heat pump</u>	<u>None</u>	EDC Data Gathering Default = <u>3.6</u>	<u>16</u>
$EER_g$ , <u>Energy Efficiency Ratio of a GSHP, this is measured differently than EER of an air source heat pump and must be converted</u>	$\frac{\text{BTU}}{\text{W} \cdot \text{h}}$	EDC Data Gathering Default = <u>17.1</u>	<u>16</u>
$GSHPDF$ , <u>Ground Source Heat Pump De-rate Factor</u>	<u>Proportion</u>	<u>0.885</u>	<u>17</u>
$ETDF_{summer}$ , <u>Summer energy to demand factor</u>	$\text{kW/kWh}$	<u>0.0005272</u>	<u>18</u>
$ETDF_{winter}$ , <u>Winter energy to demand factor</u>	$\text{kW/kWh}$	<u>0.0003398</u>	<u>18</u>

**Table 2-145: Retrofit Default Base and Energy Efficient (Insulated) R-R-Values**

Component	Existing Condition	Value ( $\frac{^{\circ}F \cdot ft^2 \cdot hr}{Btu}$ )
$R_{cell,base}$ , Assembly R-value of ceiling/attic before retrofit	Un-insulated attic	5
	4.5" (R-13) of existing attic insulation	16
	6" (R-19) of existing attic insulation	22
	10" (R-30) of existing attic insulation	30
$R_{cell,ee}$ , Assembly R-value of ceiling/attic after retrofit	Retrofit to R-49 total attic insulation	49
$R_{wall,base}$ , Assembly R-value of wall before retrofit	Assumes existing, un-insulated wall with 2x4 studs @ 16" o.c., w/ wood/vinyl siding	5
$R_{wall,ee}$ , Assembly R-value of wall after retrofit	Assumes adding R-6 per DOE recommendations	11
$R_{floor,base}$ , R-value of floor before retrofit	Thermal resistance of existing floor insulation above crawlspace	3.96
$R_{floor,ee}$ , R-value of floor after retrofit	Thermal resistance of insulation added to floor above crawlspace	EDC Data Gathering
$R_{rimjoist,base}$ , R-value of rim joist before retrofit	Baseline R-value of rim joist	2.5
$R_{rimjoist,ee}$ , R-value of rim joist after retrofit	R-value of installed spray foam or rigid foam insulation applied to rim joist	EDC Data Gathering

**DEFAULT SAVINGS**

There are no default savings for this measure.

Component	Description	Value ( $\frac{^{\circ}F \cdot ft^2 \cdot hr}{Btu}$ )	Source
$R_{cell,base}$ , Assembly R-value of ceiling/attic before retrofit	Un-insulated attic	5	4, 5
	4.5" (R-13) of existing attic insulation	16	4, 5
	6" (R-19) of existing attic insulation	22	4, 5
	10" (R-30) of existing attic insulation	30	4, 5
	Vaulted ceiling insulation, primarily consisting of fiberglass batts	22.9	6
	Default unknown: flat ceiling insulation, typically consisting of fiberglass batts	27.3	7
$R_{cell,ee}$ , Assembly R-value of ceiling/attic after retrofit	Retrofit to R-60 total attic insulation	60	2
$R_{wall,base}$ , Assembly R-value of wall before retrofit	Un-insulated wall with 2x4 studs @ 16" o.c., w/ wood/vinyl siding	5	4, 5
	Default unknown: primarily batt insulated 2x4 stud cavity	13	8

<u><math>R_{wall,ee}</math>, Assembly R-value of wall after retrofit</u>	<u>Add R10 insulative wall sheathing beneath the new siding</u>	<u>15</u>	<u>2</u>
<u><math>R_{floor,base}</math>, R-value of floor before retrofit</u>	<u>Thermal resistance of existing floor above crawlspace</u>	<u>4</u>	<u>4.5</u>
	<u>Default unknown: primarily uninsulated floors with some homes having fiberglass batts installed</u>	<u>6.9</u>	<u>9</u>
<u><math>R_{floor,ee}</math>, R-value of floor after retrofit</u>	<u>IECC climate zone 4</u>	<u>19</u>	<u>2</u>
	<u>IECC climate zone 5</u>	<u>30</u>	
<u><math>R_{rimjoist,base}</math>, R-value of rim joist before retrofit</u>	<u>Thermal resistance of existing rim joist</u>	<u>2.5</u>	<u>4.5</u>
	<u>Default unknown: mix of uninsulated and insulated homes. Insulation primarily fiberglass batt type.</u>	<u>7.4</u>	<u>10</u>
<u><math>R_{rimjoist,ee}</math>, R-value of rim joist after retrofit</u>	<u>IECC climate zone 4: Add R10 insulative wall sheathing or R13 batt</u>	<u>12.5</u>	<u>2</u>
	<u>IECC climate zone 5: Add R15 insulative wall sheathing or R19 batt</u>	<u>17.5</u>	

**Table 2-146: New Construction Baseline R-Values (2021 IECC)**

<u>IECC Climate Zone</u>	<u>Ceiling R-Value</u>	<u>Wood Frame Wall R-Value</u>	<u>Floor R-Value</u>	<u>Rim Joist R-Value</u>
<u>4</u>	<u>60</u>	<u>30 or</u>	<u>19</u>	<u>10ci or 13</u>
<u>5</u>		<u>20&amp;5ci or</u> <u>13&amp;10ci or</u> <u>0&amp;20ci</u>	<u>30</u>	<u>15ci or</u> <u>19 or</u> <u>13&amp;5ci</u>

Notes on reading values in Table 2-146:

- Wood Frame Wall R-value: The first value is cavity insulation; the second value is continuous insulation. Therefore, as an example, “20 & 5ci” means R-20 cavity insulation plus R-5 continuous insulation.
- Rim Joist R-Value, Climate Zone 4: “10ci or 13” means R-10 continuous insulation on the interior or exterior surface of the wall or R-13 cavity insulation on the interior side of the wall.
- Rim Joist R-Value, Climate Zone 5: “15ci or 19 or 13 13&5ci” means R-15 continuous insulation on the interior or exterior surface of the wall; or R-19 cavity insulation on the interior side of the wall; or R-13 cavity insulation on the interior of the wall in addition to R-5 continuous insulation on the interior or exterior surface of the wall.

## EVALUATION PROTOCOLS

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

- 1) GDS Associates, Inc., (2007). Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures, 2007.  
[https://library.cee1.org/system/files/library/8842/CEE\\_Eval\\_MeasureLifeStudyLights%2526HVAGGDS\\_1Jun2007.pdf](https://library.cee1.org/system/files/library/8842/CEE_Eval_MeasureLifeStudyLights%2526HVAGGDS_1Jun2007.pdf) Weblink. Measure life for insulation is 25 years. Note that PA Act 129 savings can be claimed for no more than 15 years, thus the 15 year measure life.
- 2) State of Ohio Energy Efficiency Technical Reference Manual, prepared for the Public Utilities Commission of Ohio by Vermont Energy Investment Corporation. August 6, 2010.
- 3) Minnesota Department of Commerce, Home Envelope, An Energy Guide to Help You Keep the Outside Out and the Inside In.  
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- 5) Energy Center of Wisconsin, "Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research,"  
[https://focusonenergy.com/sites/default/files/centralairconditioning\\_report.pdf](https://focusonenergy.com/sites/default/files/centralairconditioning_report.pdf)
- 6) For all systems excluding ground source heat pumps: Pennsylvania Act 129 2018 Residential Baseline Study, [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Due to small sample size in residential baseline, the lowest efficiency options available in BEopt were chosen as defaults for ground source heat pumps.
- 7) From PECO baseline study, average home size = 2,323 ft<sup>2</sup>, average number of room AC units per home = 2.1. Average Room AC capacity = 10,000 BTU/hr per ENERGY STAR Room AC Calculator, which serves 425 ft<sup>2</sup> (average between 400 and 450 ft<sup>2</sup> for 10,000 BTU/hr unit per ENERGY STAR Room AC sizing chart).  $F_{RAC} = (425 \text{ ft}^2 \times 2.1) / (2,323 \text{ ft}^2) = 0.39$ .
- 8) Illinois Statewide Technical Reference Manual, Version 7.0. September 28, 2018.  
<http://www.ilsag.info/technical-reference-manual.html>.
- 2) ENERGY STAR Recommended Home Insulation R-Values. Accessed February 2023. Weblink.
- 3) 2021 International Energy Conservation Code, Table R402.1.3: Insulation Minimum R-values and Fenestration Requirements by Component. Weblink
- 9) Used eQuest 3.64 to derive roof assembly R-values. When insulation is added between the joists as in most insulation up to R-30 (10"), the assembly R-value is based on a parallel heat transfer calculation of the insulation and joists, rather than a series heat transfer.
- 10) 2009 ASHRAE, (2009). Fundamentals, Chapter 25 and 26. Method from "Total Thermal Resistance of a Flat Building Assembly" in Chapter 25. Values from Chapter 26: interior air film = 0.68, 1.5" wooden rim joist = 1.65, exterior air film = 0.17. Total = 2.50 °F-ft<sup>2</sup>/hBTU Thermal resistance values from Chapter 26.

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- 41) ~~2015 International Energy Conservation Code, Table R402.1.2: Insulation and Fenestration Requirements by Component. <https://codes.iccsafe.org/content/IECC2015/chapter-4-re-residential-energy-efficiency>~~
- 42) ~~VEIC estimate. Extrapolation of manufacturer data.~~
- 13) ~~McQuay Application Guide 31-008, Geothermal Heat Pump Design Manual, 2002. Engineering Estimate – See System Performance of Ground Source Heat Pumps~~
- 6) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.3.6: Vaulted Ceiling R-value. [Weblink](#)~~
- 7) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.3.3: Flat Ceiling R-value. [Weblink](#)~~
- 8) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.2.3: Conditioned to Ambient Walls Average R-value. [Weblink](#)~~
- 9) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.4.3: Frame Floor R-value. [Weblink](#)~~
- 10) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.5.3: Foundation Wall R-value. [Weblink](#). Results in the referenced study are presented for foundation walls, which are applied in this TRM as the best proxy for rim joist insulation.~~
- 11) ~~ASHRAE. (2021). Fundamentals. Chapter 27, pg 27.3.~~
- 12) ~~Based on the Phase III SWE team’s analysis of regional HVAC runtime data collected from ecobee’s Donate Your Data research service ([Weblink](#)) and updated based on the latest CDD and HDD values from NOAA’s 15-year annual climate Normals (2006–2020) ([Weblink](#))~~
- 13) ~~Energy Center of Wisconsin, (2008, May). “Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research.” Pg 31. [Weblink](#)~~
- 14) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. [Weblink](#). Air source heat pump efficiencies calculated using 2023 Pennsylvania Residential Baseline Study data. Federal minimum efficiencies for GSHP due to small sample size for GSHP in baseline study.~~
- 15) ~~NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. [Weblink](#). Average home conditioned floor area = 2,019 ft<sup>2</sup>; average number of room AC units per home = 1.74; average Room AC capacity = 7,161 BTU/hr. Per ENERGY STAR Room AC sizing chart ([Weblink](#)), 7,161 BTU/hr of cooling serves approximately 283 ft<sup>2</sup>.  $F_{RAC} = (283 \text{ ft}^2 \times 1.74) / (2,019 \text{ ft}^2) = 0.24$ .~~
- 16) ~~Federal minimum efficiency standards, based on ASHRAE 90.1-2019. [Weblink](#).~~
- 17) ~~McQuay Application Guide 31-008, Geothermal Heat Pump Design Manual, 2002. Engineering Estimate - See System Performance of Ground Source Heat Pumps.~~
- 18) ~~Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. [Weblink](#)~~

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- ~~14) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. <https://www.ecobee.com/donateyourdata/>~~
- ~~15) PA SWE Team Calculations with data from the National Solar Radiation Database, 1991–2005 Update: Typical Meteorological Year 3. NREL. [http://rredc.nrel.gov/solar/old\\_data/nsrdb/1991-2005/tmy3/by\\_state\\_and\\_city.html](http://rredc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html)~~



### 2.6.4 BASEMENT OR CRAWL SPACE WALL INSULATION

Target Sector	Residential <del>Establishments</del>
Measure Unit	Insulation Addition
Measure Life	15 years <sup>Source 1</sup>
Vintage	Retrofit, <u>New Construction</u>

This protocol covers the calculation of energy and demand savings associated with insulating foundation walls in basements and crawl spaces in residential homes. Cooling savings are only produced from insulation improvements to above-grade portions of the wall, since the below-grade portions are expected to be cooler than the temperature set point of the building. Heating savings will be produced from the entire insulation improvement, though in varying quantities depending on whether above or below grade.

#### ELIGIBILITY

This measure protocol applies to the installation of insulation to the walls of basements or unvented crawl space walls in existing residential buildings.

Research has shown that vented crawlspaces that are sealed and insulated operate similarly to basements in providing benefits such as energy savings, comfort, moisture control, long-term durability, and healthier air quality. <sup>Source 2</sup> Sealing the crawl space must follow the required PA building codes, including covering the earth with a Class I vapor retarder and providing ventilation of at least 1cfm per 50 ft<sup>2</sup> of crawlspace. In addition, sealing of the crawlspace must not block access to the space.

Basement In 2021 IECC Climate Zone 4, basement or crawl space insulation should have either a minimum R-10 continuous insulated sheathing insulation on the interior or exterior of the home, or R-13 cavity insulation aton the interior of the home. In IECC Climate Zone 5, basement or crawl space wall in IECC Climate Zone 4, and R-insulation should have either a minimum of R-15 continuous insulation on the interior or exterior of the home, or R-19 cavity insulation in zones 5 or 6 on the interior of the home, or R-13 cavity insulation on the interior of the home and R-5 continuous insulation. <sup>Source 3</sup>

#### ALGORITHMS

Savings are due to a reduction in cooling and heating requirements due to insulation.

$$\begin{aligned}
 \Delta kWh &= \Delta kWh_{cool} + \Delta kWh_{heat} \\
 \Delta kWh &= \Delta kWh_{cool} + \Delta kWh_{heat} \\
 \Delta kWh_{cool} &= \left( \frac{1}{R_{base}} - \frac{1}{R_{base} + R_{ee}} \right) \left( \frac{1}{R_{base,ag}} - \frac{1}{R_{base,ag} + R_{ee}} \right) \\
 &\quad \times \frac{L \times H_{ag} \times (1 - FF) \times CDD \times 24 \frac{Btu}{day}}{SEER \times 1,000 \frac{Wh}{kWh}} \\
 \Delta kWh_{heat} &= \frac{L \times H_{ag} \times (1 - FF) \times CDD \times 24}{SEER \times 1,000} \times DUA \times F_{RAC}
 \end{aligned}$$

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$$\begin{aligned}
 \Delta kW_{heat} &= \left\{ \left( \frac{1}{R_{base}} - \frac{1}{R_{base} + R_{ee}} \right) \times H_{ag} \right. \\
 &\quad \left. + \left( \frac{1}{R_{base} + R_{earth}} - \frac{1}{R_{base} + R_{earth} + R_{ee}} \right) \times H_{bg} \right\} \\
 &\quad \times \frac{L \times (1 - FF) \times HDD \times 24 \frac{hr}{day}}{HSPF \times 1,000 \frac{Wh}{kW}} \times AF \\
 &= \left\{ \left( \frac{1}{R_{base,ag}} - \frac{1}{R_{base,ag} + R_{ee}} \right) \times H_{ag} \right. \\
 &\quad \left. + \left( \frac{1}{R_{base,bg}} - \frac{1}{R_{base,bg} + R_{ee}} \right) \times H_{bg} \right\} \\
 &\quad \times \frac{L \times (1 - FF) \times HDD \times 24}{HSPF \times 1,000}
 \end{aligned}$$

$$\Delta kW_{summer\ peak} = \frac{\Delta kW_{cool}}{EFLH_{cool}} \times CF = \Delta kW_{cool} \times ETDf_{summer}$$

$$\Delta kW_{winter\ peak} = \Delta kW_{heat} \times ETDf_{winter}$$

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**Ground Source Heat Pumps (GSHP)**

GSHP efficiencies are typically calculated differently than air-source units, baseline and qualifying unit efficiencies should be converted as follows **should be converted as follows:**

$$SEER = EER_g \times GSHPDF \times GSER$$

$$HSPF = COP_g \times GSHPDF \times 3.412 \frac{BTU}{Wh}$$

**PTAC and PTHP**

$$SEER = EER$$

**DEFINITION OF TERMS**

$$HSPF = COP_g \times GSHPDF \times 3.412 \frac{BTU}{Wh}$$

**PTAC and PTHP**

$$SEER = EER$$

**DEFINITION OF TERMS**

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Table 2-147: Terms, Values, and References for Basement or Crawl Space Insulation

Term	Unit	Values	Source
$\Delta kWh_{cool}$ Annual cooling energy savings	kWh/year	Calculated	=
$\Delta kWh_{heat}$ Annual heating energy savings	kWh/year	Calculated	=
$R_{base}$ , $R_{base,ag}$ baseline R-value of foundation wall above grade	$\frac{^{\circ}F \cdot ft^2 \cdot h}{BTU}$	EDC Data Gathering Default = existing nominal R-value + 1; Minimum = 1. (An uninsulated wall is assumed to be R-1.)	4 EDC Data Gathering
		Uninsulated: R-1.47	4
		Default/unknown: R-8.9	14
		Retrofit:	
		New Construction: IECC climate zone 4: 10ci or 13	3
		IECC climate zone 5: 15ci or 19 or 13&5ci	
$R_{EAFW}$ , $R_{base,bg}$ the combined average R-value for the thermal resistance of the wall and Earth at the height of insulated foundation wall below grade ( $H_{bg}$ )	$\frac{^{\circ}F \cdot ft^2 \cdot h}{BTU}$	Table 2-148	53, 4
$R_{ee}$ , R-value of installed spray foam, rigid foam, or cavity insulation applied to foundation wall	$\frac{^{\circ}F \cdot ft^2 \cdot h}{BTU}$	EDC Data Gathering	EDC Data Gathering
$L$ , total length of all perimeter foundation wall around the entire insulated perimeter walls receiving new insulation	ft	EDC Data Gathering	EDC Data Gathering
$H_{ag}$ , height of insulated foundation wall above grade	ft	EDC Data Gathering	EDC Data Gathering

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Term	Unit	Values	Source
$H_{bg}$ , height of insulated foundation wall below grade	ft	EDC Data Gathering	EDC Data Gathering
$FF$ , framing factor, adjustment to account for area of framing when cavity insulation is used	Proportion	If externally applied continued = 0% If studs and cavity stud-bay cavity = 25%	65
$CDD$ , cooling degree days matched to basement or crawlspace condition (conditioned/unconditioned). Insulation in unconditioned spaces is modeled by reducing the degree days to reflect the smaller but non-zero contribution to heating and cooling load.	$^{\circ}F\text{-day}$	See CDD in Vol. 1 App. A	136
$HDD$ , heating degree days matched to basement or crawlspace condition (conditioned/unconditioned). Insulation in unconditioned spaces is modeled by reducing the degree days to reflect the smaller but non-zero contribution to heating and cooling load.	$^{\circ}F\text{-day}$	See HDD in Vol. 1 App. A	136
$DUA$ , Discretionary Use Adjustment, adjustment for times when AC is not operating even though conditions may call for it	Proportion	0.75	7
$F_{RAC}$ , Adjustment factor to relate insulated area to area served by room air conditioners	None	If Room AC = 0.3824 If non-Room AC = 1.0	148
$SEER$ , Cooling system seasonal efficiency	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: See Early Replacement or New Construction values (as appropriate) in Table 2-10 in Sec. 2.2.1	89
$HSPF$ , Heating system seasonal efficiency	Proportion	EDC Data Gathering Default: See Early Replacement or New Construction values (as appropriate) in Table 2-10 in Sec. 2.2.1	89
<del><math>AF</math>, adjustment factor, accounts for prescriptive engineering algorithms overestimating savings</del>	<del>Proportion</del>	<del>0.88</del>	<del>9</del>
<del><math>GOPCOP_g</math>, Coefficient of Performance. This is a measure of the efficiency of a ground source heat pump</del>	<del>None</del>	<del>EDC Data Gathering Default = 13.6</del>	<del>-10</del>
<del><math>EEREER_g</math>, Energy Efficiency Ratio of a GSHP, this is measured differently than EER of an air source heat pump and must be converted</del>	<del><math>\frac{BTU}{W \cdot h}</math></del>	<del>EDC Data Gathering Default = 17.1</del>	<del>-10</del>

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Term	Unit	Values	Source
<i>GSEER</i> , Factor used to determine the SEER of a GSHP based on its EERg	$\frac{BTU}{Wh}$	1.02	44
<i>GSPK</i> , Factor to convert EERg to the equivalent EER of an air conditioner to enable comparisons to the baseline unit	Proportion	0.8416	44
<i>GSHPDF</i> , Ground Source Heat Pump De-rate Factor	Proportion	0.885	4211
<i>EFLH<sub>cool</sub></i> , equivalent full load hours of air conditioning <i>ETDF<sub>summer</sub></i> , Summer energy to demand factor	$\frac{hourskWh}{Wh}$	0.0005272 EDC Data Gathering or See <i>EFLH<sub>cool</sub></i> in Vol. 1 App. A	12 EDC Data Gathering 40
<i>CF</i> , coincidence factor <i>ETDF<sub>winter</sub></i> , Winter energy to demand factor	$\frac{ProportionkWh}{kWh}$	See <i>CF</i> in Vol. 1 App. A A0.0003398	4012

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Table 2-148 should be used to determine the average thermal resistance of the combined wall and Earth ( $R_{Earth}R_{base,bg}$ ) at the height of foundation wall below grade ( $H_{bg}$ ). Use a crawl space wall that is 5 ft in height as an example of proper use of the table. If the crawl space wall is 5 ft in height and 1 ft is above grade ( $H_{ag} = 1$  ft), then the remaining 4 ft are below grade ( $H_{bg} = 4$  ft). To determine the  $R_{Earth}R_{base,bg}$  for that below-grade wall height, look for the column for  $H_{bg} = 4$  ft in Table 2-148.  $R_{base,bg}$  in this example is therefore 6.424.26 °F-ft<sup>2</sup>-h/BTU.

Table 2-148: Below-grade R-values (°F-ft<sup>2</sup>-h/BTU) for combined Earth and basement wall

$H_{bg}$ (ft)	Retrofit				New Construction <sup>Source 13</sup>				
	0No Existing Insulation <sup>Source 4</sup>	1Unknown Existing Insulation <sup>Source 15</sup>	2	3	4IECC Climate Zone 4	5IECC Climate Zone 5	6	7	8
	1	2.31	9.71	12.31	17.31				
2	3.47	6.42	7.46	8.46	13.0	18.02	9.5	10.6	9
3	3.66	11.06	13.66	18.66					
4	4.26	11.66	14.26	19.26					
5	4.81	12.21	14.81	19.81					
6	5.35	12.75	15.35	20.35					
7	5.88	13.28	15.88	20.88					
8	6.37	13.77	16.37	21.37					

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**DEFAULT SAVINGS**

There are no default savings for this measure.

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values. For projects using customer specific data for open variables, the appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with

verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

## SOURCES

- 1) Measure Life Report, Residential and Commercial/Industrial Lighting and HVAC Measures Prepared for The New England State Program Working Group, <http://library.cee1.org/content/measure-life-report-residential-and-commercialindustrial-lighting-and-hvac-measures>. Weblink. Measure life for insulation is 25 years. Note that PA Act 129 savings can be claimed for no more than 15 years, thus the 15 year measure life.
- 2) USDOE, Guide to Closing and Conditioning Ventilated Crawlspace, <http://www.nrel.gov/docs/fy13osti/54859.pdf>. Weblink.
- 3) 2015/2021 International Energy Conservation Code, Table R402.1.23: Insulation Minimum R-values and Fenestration Requirements by Component. <https://codes.iccsafe.org/content/IECC2015/chapter-4-re-residential-energy-efficiency>. Weblink. 20ci or 13" means R-10 continuous insulation (ci) on the interior or exterior surface of the wall or R-13 cavity insulation on the interior side of the wall. "15ci or 19 or 13&5ci" means R-15 continuous insulation (ci) on the interior or exterior surface of the wall; or R-19 cavity insulation on the interior side of the wall; or R-13 cavity insulation on the interior of the wall in addition to R-5 continuous insulation on the interior or exterior surface of the wall.
- 4) 2017 ASHRAE. (2021). Fundamentals, Table 16—Wall Conduction Time Series; total R = 0.95 for aChapter 18, pg 18.44. ASHRAE assumes an uninsulated concrete wall built as an R-value of 1.47. R<sub>bg</sub> values are calculated from 200mm LW-CMU with fill insulation.
- 5) Illinois Statewide Technical Reference Manual, Version 7.0. September 28, 2018. <http://www.ilsag.info/technical-reference-manual.html>
- 6) CEC 2001A. "Characterization of Framing Factors for Low Rise Residential Building Envelopes U<sub>avg,bw</sub> Values in California"—Public Interest Energy Research Program: Final Report, Publication Number: 500-02-002, Dec 2001. <http://www.energy.ca.gov/reports/2002-09-06-500-02-002.PDF> Table 22 on page 18.44.
- 5) ASHRAE. (2021). Fundamentals. Chapter 27, p 27.3.
- 6) Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service (Weblink) and updated based on the latest CDD and HDD values from NOAA's 15-year annual climate Normals (2006–2020) (Weblink)
- 7) Energy Center of Wisconsin, May (2008 metering study; May). "Central Air Conditioning in Wisconsin, A Compilation of Recent Field Research", p34. <http://cleanefficientenergy.org/resource/central-air-conditioning-wisconsin-compilation-recent-field-research/>. Pg 31. Weblink.
- 8) For all systems excluding ground source heat pumps: NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 2018 Residential Baseline Study. [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Due. Weblink. Average home conditioned floor area = 2,019 ft<sup>2</sup>; average number of room AC units per home = 1.74; average Room AC capacity = 7,161 BTU/hr. Per ENERGY STAR Room AC sizing chart (Weblink), 7,161 BTU/hr of cooling serves approximately 283 ft<sup>2</sup>.  $F_{RAC} = (283 \text{ ft}^2 \times 1.74) / (2,019 \text{ ft}^2) = 0.24$ .
- 9) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Pg 115, table 97, pg. 120, table 103. Weblink. Air source heat pump efficiencies calculated using 2023 Pennsylvania Residential Baseline Study data. Federal minimum efficiencies for GSHP due to small sample size for GSHP in residential baseline, the lowest study.

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- 8)10) Federal minimum efficiency options available in BEopt were chosen as defaults for ground source heat pumps standards, based on ASHRAE 90.1-2019. Weblink.
- 9) “Home Energy Services Impact Evaluation”, August 2012. Based on comparing algorithm derived savings estimate and evaluated bill analysis estimate. <http://ma-eeac.org/wordpress/wp-content/uploads/Home-Energy-Services-Impact-Evaluation-Report-Part-of-the-Massachusetts-2011-Residential-Retrofit-and-Low-Income-Program-Area-Evaluation.pdf>
- 10) Based on the Phase III SWE team’s analysis of regional HVAC runtime data collected from ecobee’s Donate Your Data research service. <https://www.ecobee.com/donateyourdata/>
- 11) VEIC estimate. Extrapolation of manufacturer data.
- 12)11) McQuay. (2002). Application Guide 31-008, Geothermal Heat Pump Design Manual, 2002. Engineering Estimate - See System Performance of Ground Source Heat Pumps
- 13) PA SWE Team Calculations with data from the National Solar Radiation Database, 1991–2005 Update: Typical Meteorological Year 3. NREL. [http://redc.nrel.gov/solar/old\\_data/nsrdb/1991-2005/tmy3/by\\_state\\_and\\_city.html](http://redc.nrel.gov/solar/old_data/nsrdb/1991-2005/tmy3/by_state_and_city.html)
- 14) From PECO baseline study, average home size = 2,323 ft<sup>2</sup>, average number of room AC units per home = 2.1. Average Room AC capacity = 10,000 BTU/hr per ENERGY STAR Room AC Calculator, which serves 425 ft<sup>2</sup> (average between 400 and 450 ft<sup>2</sup> for 10,000 BTU/hr unit per ENERGY STAR Room AC sizing chart).  $F_{RAC} = (425 \text{ ft}^2 \times 2.1) / (2,323 \text{ ft}^2) = 0.38$ .
- 12) Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink
- 13) Default new construction below grade R-values are the sum of the uninsulated wall assembly in the retrofit case and the code minimum continuous insulation R-value.
- 14) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.5.3: Foundation Wall R-value. Weblink. The R-8.9 value is the sum of the wall materials (R-1.47) and average added insulation presented in the residential baseline study (R-7.4).
- 15) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 Residential Baseline Study. Section 6.5.3: Foundation Wall R-value. Weblink. In retrofit cases where it is unknown whether there is existing insulation present on the basement wall, add R-7.4 to the below-grade uninsulated retrofit R-value.

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## 2.6.5 ENERGY STAR WINDOWS

Target Sector	Residential Establishments
Measure Unit	Window Area
Measure Life	(15 max, but 20 for TRC) years <sup>Source 1</sup>
Vintage	Retrofit

### ELIGIBILITY

This protocol documents the energy savings for replacing existing windows in a residence with ENERGY STAR [version 7](#) certified windows. [Source 2](#)

### ALGORITHMS

$$\Delta kWh = \Delta kWh_{cool} + \Delta kWh_{heat}$$

$$\Delta kWh_{cool} = \text{Area of Window } ft^2 \times \frac{\eta_{proto}}{\eta_{base}} \times UES_{region,system}^{a_{cool}} \times \text{overlap}$$

$$\Delta kWh_{heat} = \text{Area of Window } ft^2 \times \frac{\eta_{proto}}{\eta_{base}} \times UES_{region,system}^{a_{heat}} \times \text{overlap}$$

$$AKW = \frac{\Delta kWh_{cool}}{EFLH_{cool}} \times CF$$

$$AKW_{summer} = \frac{\Delta kWh_{cool}}{EFLH_{cool}} \times CF_{summer}$$

$$AKW_{winter} = \frac{\Delta kWh_{heat}}{EFLH_{hea}} \times CF_{winter}$$

Energy savings depend on three components: a unit energy savings value (UES) [coefficient](#) ( $a_{cool}$  or  $a_{heat}$ ) developed from prototype home energy models, the ratio of the efficiency of the cooling and heating equipment in the home to the values in the prototype home ( $\frac{\eta_{proto}}{\eta_{base}}$ ), and [THE eligible](#) window area. To calculate energy savings, look up the efficiency value for the applicable equipment type in [THE EARLY REPLACEMENT VALUES IN TABLE 2-8 IN SEC. 2.2, Table 2-151](#). This is  $\frac{\eta_{proto}}{\eta_{base}}$ . For  $\frac{\eta_{proto}}{\eta_{base}}$ , use the corresponding value for the equipment in the home, or the default value of  $\frac{\eta_{proto}}{\eta_{base}}$  (i.e., a ratio of 1). Calculate the ratio. Then look up the [VALUE FOR UES IN TABLE 2-124\(a\)](#) for the correct equipment type and climate [REFERENCE CITY, region in Table 2-150](#). Multiply these values by the window area to get cooling or heating savings.

### DEFINITION OF TERMS

Non-centralized cooling systems such as room air conditioners and mini-splits include an additional factor representing the overlap between the fraction of a home's conditioned floor area (CFA) served by these systems that also receive upgraded windows. For instance, if two bedrooms each representing 15% of CFA are cooled with room ACs, but only one of the room's windows are

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upgraded, then overlap is 15%. If both bedrooms receive new windows, then overlap is 30%. (Upgraded windows in other parts of the home also reduce cooling load however, calculating their contributions is non-trivial. Consequently, these effects are omitted for simplicity and to allow for conservative results when an imprecise overlap is used.)

**DEFINITION OF TERMS**

**Table 2-149: Terms, Values, and References for ENERGY STAR Windows**

Term	Unit	Value	Sources
$UE_{S_{region,system}}$ , Climate-region dependent electricity savings for efficient glazing	$\frac{kWh}{ft^2}$	See Table 2-124	2
$\eta_{base}$ , Baseline heating or cooling equipment efficiency	varies	Measured, EDC Data Gathering Default: $\eta_{PROTO}$	
$\eta_{PROTO}$ , Prototype heating or cooling equipment efficiency	varies	See Early Replacement values in Table 2-8 in Sec. 2.2.1	3
$EFLH_{cool}$ , Equivalent Full Load Cooling hours	$\frac{hours}{year}$	See $EFLH_{cool}$ in Vol. 1, App. A	4
$CF$ , Demand Coincidence Factor	Proportion	See $CF$ in Vol. 1, App. A	4

<b>Term</b>	<b>Unit</b>	<b>Value</b>	<b>Sources</b>
<u><math>a_{cool}</math></u> , Climate region dependent electricity savings for efficient glazing	$\frac{kWh}{ft^2}$	See Default Unit Energy Savings Coefficient & Equipment Efficiency Tables Table 2-150	<u>3</u>
<u><math>a_{heat}</math></u> , Climate region dependent heating electricity savings for efficient glazing	$\frac{kWh}{ft^2}$	See Default Unit Energy Savings Coefficient & Equipment Efficiency Tables Table 2-150	<u>3</u>
<u><math>\eta_{base}</math></u> , Baseline heating or cooling equipment efficiency	varies	Measured, EDC Data Gathering Default: $\eta_{proto}$	-
<u><math>\eta_{proto}</math></u> , Prototype heating or cooling equipment efficiency	varies	See Table 2-151	<u>4</u>
<u>overlap</u> , Fraction of conditioned floor area served by HVAC with upgraded windows	<u>Proportion</u>	Measured, EDC Data Gathering Default: 100% for ASHP, CAC, GSHP, baseboard & electric furnace 0% for Mini-split, Room AC	-
<u><math>EFLH_{cool}</math></u> , Equivalent Full Load Hours of operation during the cooling season for the average unit	$\frac{hours}{year}$	See <u><math>EFLH_{cool}</math></u> in Vol. 1, App. A	<u>5</u>
<u><math>EFLH_{heat}</math></u> , Equivalent Full Load Hours of operation during the heating season for the average unit	$\frac{hours}{yr}$	See <u><math>EFLH_{cool}</math></u> in Vol. 1, App. A	<u>5</u>
<u><math>CF_{summer}</math></u> , Summer demand Coincidence Factor	<u>Proportion</u>	See <u>Summer CF</u> in Vol. 1, App. A	<u>5</u>
<u><math>CF_{winter}</math></u> , Winter demand Coincidence Factor	<u>Proportion</u>	See <u>Winter CF</u> in Vol. 1, App. A	<u>5</u>

**DEFAULT UNIT ENERGY SAVINGS COEFFICIENT & EQUIPMENT EFFICIENCY TABLES**

**Table 2-150: Default  $UE_{region,system}$  unit energy savings – kWh per Square Foot of Replaced Window**

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Reference City	Cooling				Heating				
	ASHP	Central AC	Mini-split	GSHP	ASHP	Electric Furnace	Base-board	Mini-split	GSHP
Allentown	0.66	1.50	0.59	0.57	2.86	3.40	3.12	2.10	0.95
Binghamton	0.46	0.65	0.47	0.36	4.50	4.60	4.28	3.56	1.27
Bradford	0.35	1.10	0.34	0.25	5.57	5.54	7.86	4.63	1.58
Erie	0.54	0.54	0.46	0.41	4.07	4.84	4.07	3.42	1.35
Harrisburg	0.75	0.82	0.73	0.66	2.84	3.91	3.17	2.40	1.06
Philadelphia	0.86	0.83	0.76	0.86	1.68	2.53	5.85	1.31	0.68
Pittsburgh	0.66	0.66	0.64	0.60	3.06	3.82	3.06	2.28	1.07
Scranton	0.59	0.68	0.67	0.50	3.36	3.83	3.55	2.58	1.06
Williamsport	0.65	0.46	0.61	0.58	2.99	3.47	5.08	2.19	0.96

Climate Region	$a_{cool}$					$a_{heat}$				
	ASHP	Central AC	GSHP	Mini-split	Room AC	ASHP	Base-board	Electric Furnace	GSHP	Mini-split
A	0.23	0.18	0.12	0.13	0.26	2.52	6.39	6.80	2.00	2.21
B	0.31	0.38	0.20	0.27	0.52	1.93	4.96	5.25	1.43	1.36
C	0.41	0.49	0.30	0.30	0.66	1.75	4.59	4.80	1.29	1.24
D	0.70	0.76	0.60	0.51	1.05	0.83	2.59	2.35	0.76	0.56
E	0.60	0.63	0.38	0.42	0.90	1.00	2.76	2.71	0.68	0.71
F	0.34	0.39	0.24	0.27	0.56	1.89	5.00	5.15	1.39	1.39
G	0.13	0.15	0.08	0.06	0.19	2.64	6.74	7.22	2.51	2.45
H	0.33	0.37	0.22	0.27	0.52	1.97	5.12	5.38	1.49	1.44
I	0.31	0.36	0.19	0.26	0.49	2.15	5.43	5.90	1.61	1.59

**Table 2-151: Prototype Residential Equipment Efficiency ( $\eta_{proto}$ )**

	ASHP	Baseboard	Central AC	Electric Furnace	GSHP	Mini-split	Room AC
Cooling	15 SEER/ 14.3 SEER2	=	13.2 SEER/ 12.9 SEER2	=	23.9 EER	18.9 SEER/ 17.5 SEER2	10.7 EER/ 10.6 CEER
Heating	8.5 HSPF/ 7.3 HSPF2	1.0 COP	=	1.0 COP	4.2 COP	10.0 HSPF/ 8.6 HSPF2	=

**EVALUATION PROTOCOLS**

The appropriate evaluation protocol is to verify installation and proper application of TRM protocol along with verification of open variables. The Pennsylvania Evaluation Framework provides specific guidelines and requirements for evaluation procedures.

**SOURCES**

- 1) ~~California Public Utilities Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>. Accessed December 2018.~~
- 1) California Electronic Technical Reference Manual. "Effective Useful Life and Remaining Useful Life". Accessed December 2023. Weblink
- 2) U.S. EPA. (2022). ENERGY STAR Program Requirements for Residential Windows, Doors, and Skylights Version 7.0 Specification. Weblink
- 2)3) Based on modelling using BEopt v2.8.0 performed by NMR Group, Inc. Unit energy savings were calculated by modeling a prototypical Pennsylvania single family detached house with statewide average characteristics determined through the Pennsylvania Act 129 20182023 Residential Baseline Study; 0.44 U / 0.52 SHGC. Simulations for each equipment-climate

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region combination were performed for ~~plain double-pane (0.49 U, 0.56 SHGC) and triple-pane ENERGY STAR (version 7 windows using 0.2725 U, / 0.2630 SHGC) windows, as representative specifications for climate regions D & E, and 0.21 / 0.32 SHGC for the remaining regions.~~ The difference in heating and cooling ~~loads were~~consumption was then apportioned evenly among the 322305 square feet of windows in the prototype home yielding the UES values.

3)4) NMR Group for the Pennsylvania Public Utility Commission. (2024, March). 2023 Pennsylvania Statewide Act 129 2018 Residential Baseline Study. [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3\\_Res\\_Baseline\\_Study\\_Rpt021219.pdf](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE-Phase3_Res_Baseline_Study_Rpt021219.pdf). Weblink

4)5) ~~Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service.~~ Based on the Phase III SWE team's analysis of regional HVAC runtime data collected from ecobee's Donate Your Data research service. <https://www.ecobee.com/donateyourdata/> Weblink

## 2.7 WHOLE HOME

### 2.7.1 RESIDENTIAL NEW CONSTRUCTION

<b>Target Sector</b>	Residential Establishments
<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Multiple
<b>Measure Life</b>	Varies
<b>Vintage</b>	New Construction

#### ELIGIBILITY

This protocol documents the energy savings attributed to improvements to the construction of residential buildings compared to the baseline of a minimally code-compliant building, as calculated by the appropriate energy modeling software. This measure may be applied to attached or detached single-family homes and to multifamily residential buildings ~~that meet the following requirements:~~<sup>Source 12</sup>

- ~~All units must be individually metered.~~
- ~~Each unit must have its own residential-grade heating, cooling, and water heating equipment.~~
- ~~The building must be under 6 stories.~~

~~Dwelling units must comprise at least 80% of the occupiable<sup>83</sup> space of the building.<sup>84</sup> Mixed-use buildings are also eligible where the dwelling units and residential use common space combined exceed 50% of the building's square footage. Parking garage square footage is excluded from this calculation.~~<sup>Source 1</sup>

~~• Multifamily buildings of 4 stories and higher are subject to the commercial building code and hence have different baseline specifications than buildings subject to residential building code requirements. Savings for multifamily buildings may be claimed only for savings generated in the residential spaces of the building.~~

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#### ALGORITHMS

Energy and peak demand savings for Residential New Construction ~~programs~~measures will be calculated by comparing outputs of energy models of the as-designed unit or building to a minimally code-compliant baseline unit or building. The characteristics of the baseline unit or building thermal envelope and/or system characteristics shall be based on the current state-adopted ~~2021~~ International Energy Conservation Code (IECC) ~~2015~~<sup>85</sup>.<sup>Source 2</sup>

~~Modeled~~For single-family homes and individual dwelling units, ~~modeled~~ energy and peak demand savings shall be produced ~~by~~with a RESNET accredited ~~software program~~<sup>86</sup>software<sup>Source 3</sup> or the Passive House ~~accreditation~~accredited software packages (Passive House Planning

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<sup>83</sup> Per ASHRAE 62.2-2010, occupiable space is any enclosed space inside the pressure boundary and intended for human activities or continual human occupancy, including, but not limited to, areas for living, sleeping, dining, and cooking, toilets, closets, halls, storage and utility areas, and laundry areas.

<sup>84</sup> For mixed-use buildings, exclude the retail/commercial area when determining the square footage of the building.

<sup>85</sup> International Code Council, Inc. (2015). 2015 International Energy Conservation Code. Retrieved from International Code Council: [https://codes.iccsafe.org/content/IECC2015?site\\_type=public](https://codes.iccsafe.org/content/IECC2015?site_type=public)

<sup>86</sup> See the RESNET National Registry of Accredited Rating Software Programs for a complete listing: <http://www.resnet.us/professional/programs/energy-rating-software>

Package<sup>87</sup>Package<sup>Source 4</sup> and WUFI Passive<sup>88</sup>Passive<sup>Source 5</sup>), though both Passive House tools require the user to separately model the code baseline reference design to calculate energy and demand savings.

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For multifamily buildings, savings may be calculated by modeling the building's individual units using any approved software. Savings may also be calculated for the entire building using Passive House accreditation software, or under RESNET multifamily sampling protocols.<sup>89</sup>

For multifamily buildings, modeled energy savings shall be produced at the building level with whole building modeling tools as designated by the ENERGY STAR Multifamily New Construction Program (eQUEST, DOE2.1, Energy Plus, Carrier HAP, Open Studio, and Trane Trace 700).<sup>Source 6</sup> Alternatively, RESNET accredited software<sup>Source 3</sup> or the Passive House accreditation software packages (Passive House Planning Package<sup>Source 4</sup> and WUFI Passive<sup>Source 5</sup>) may be used to model energy savings for each residential dwelling unit archetype, where dwelling archetype can be defined by one or more key metrics such as bedroom/bathroom counts or square footage ranges.

Energy savings will be calculated from the software output using the following algorithm:

*Energy savings of the qualified unit/building (kWh/yr)*

$$\Delta kWh = kWh_{base} - kWh_{ee}$$

Peak demand savings are based on reduction in peak cooling loads. Neither the RESNET accredited software nor Passive House accreditation software allow calculations of peak demand savings for end uses other than cooling equipment, which is assumed to be active during the peak period. Additional demand savings may be claimed under this measure, but these additional demand savings must be calculated using the algorithms from the applicable measure elsewhere in the TRM. For example, to claim demand savings from a refrigerator, demand savings for that end use must be calculated using the demand savings algorithms in Sec. 2.4.1 ENERGY STAR Refrigerators. Claiming additional demand savings may require additional EDG data collection than required to generate the energy model.

If the modeling software provides building-level outputs of hourly energy consumption (an 8760 load profile), then coincident peak demand savings may be calculated by averaging the hourly energy savings during the TRM defined peak demand time period. The TRM peak demand time period is defined in Volume 1.

If the modeling software does not provide building-level outputs of hourly energy consumption, the system peak electric demand savings will be calculated from the software's calculated from the software output with annual energy savings and the following algorithm:

*Coincident system peak electric demand savings (kW)*

*Peak demand of the baseline home/unit*

$$\frac{PL_{base}}{EER_{base}}$$

<sup>87</sup> <http://www.passivehouseacademy.com/index.php/shop-us>

<sup>88</sup> <http://www.phius.org/software-resources/wufi-passive-and-other-modeling-tools/wufi-passive-3-0>

<sup>89</sup> At the time of publication, RESNET standards for multifamily inspection and sampling were still under development, though they are expected to be adopted before this TRM takes effect. See <http://conference2018.resnet.us/data/energymeetings/presentations/How%20Standards%20are%20Evolving%20to%20Better%20Address%20Multifamily%20Ratings%20.pdf>

$$\text{Peak demand of the qualifying home/unit} = \frac{P_{L_{eeg}}}{EER_{eeg}}$$

Coincident system peak electric demand savings (kW)

$$\Delta kW_{\text{peak}} = (\text{Peak demand of the baseline home/unit} - \text{Peak demand of the qualifying home/unit})$$

$$\Delta kW_{\text{peak, summer}} = \Delta kWh \times ETDf_{\text{summer}}$$

$$\Delta kW_{\text{peak, winter}} = \Delta kWh \times ETDf_{\text{winter}}$$

### DEFINITION OF TERMS

A summary of the input values and their data sources follows:

Table 2-152: Terms, Values, and References for Residential New Construction

Term	Unit	Value	Sources
<i>kWh<sub>base</sub></i> , Annual energy consumption of the baseline home/unit/building.	<i>kWh</i>	Software Calculated	47
<i>kWh<sub>ee</sub></i> , Annual energy consumption of the qualifying home/unit/building.	<i>kWh</i>	Software Calculated	28
<i>P<sub>L<sub>base</sub></sub></i> , Estimated peak cooling load of the baseline home/unit. <i>ETDf<sub>s</sub></i> , Summer energy to demand factor	<i>kBTU/hr/kW/kWh</i>	Software Calculated 0.0001376	39
<i>P<sub>L<sub>ee</sub></sub></i> , Estimated peak cooling load for the qualifying home/unit. <i>ETDf<sub>w</sub></i> , Winter energy to demand factor	<i>kBTU/hr/kW/kWh</i>	Software Calculated 0.0001967	59
<i>EER<sub>base</sub></i> , Energy Efficiency Ratio of the baseline unit.	$\frac{BTU}{W-h}$	EDC Data Gathering Default: $0.0229 \times \frac{SEER_{base}^2 + 1.1522}{SEER_{base}}$	4
<i>EER<sub>ee</sub></i> , Energy Efficiency Ratio of the qualifying unit.	$\frac{BTU}{W-h}$	EDC Data Gathering Default: $0.0229 \times \frac{SEER_{ee}^2 + 1.1522}{SEER_{ee}}$	4
<i>SEER<sub>base</sub></i> , Seasonal Energy Efficiency Ratio of the baseline unit.	$\frac{BTU}{W-h}$	13 14 (ASHRAE)	8
<i>SEER<sub>ee</sub></i> , SEER associated with the HVAC system in the qualifying home.	$\frac{BTU}{W-h}$	EDC Data Gathering	6
<i>V<sub>r</sub></i> , Rated storage volume of baseline water heater	<i>gallons</i>	EDC Data Gathering	EDC Data Gathering
Model inputs for baseline home	<i>Varies</i>	Less than 4 stories: See Table 2-128, Table 2-153 and Table 2-154 4 stories and higher: See Table 2-130, Table 2-156 and Table 2-134, Table 2-157	

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The following table lists the building envelope characteristics of the baseline reference home based on 2015 IECC for the three climate zones in Pennsylvania.

Table 2-153: Baseline Insulation and Fenestration Requirements by Component for Buildings Less Than 4 Stories (Equivalent U-Factors)<sup>Source 10</sup>

IEC Climate Zone	Fenestration U-Factor	Skylight U-Factor	Glazed Fenestration SHGC	Ceiling U-Factor	Frame Wall U-Factor	Mass Wall U-Factor	Floor U-Factor	Base ment Wall U-Factor	Slab R-Value & Depth	Crawl Space Wall U-Factor
4A4	0.3530	0.55	0.02640	0.06024	0.045	0.098	0.047	0.059	10-210	
5A5	0.3230	0.55	0.02640	0.06024	0.045	0.082	0.033	0.050	10-210	
6A	0.32			0.55	0.026	0.045	0.060	0.033	10-210	

Climate Region D and York County are CZ4A, Climate Region A and G are CZ6A, everything else is CZ5

Table 2-154: Residential New Construction Baseline Building Values for Buildings Less Than 4 Stories

Data Point	Value	Source
Air Infiltration Rate	53.0 ACH <sub>50</sub> for the whole house	711
Duct Leakage	4 CFM <sub>25</sub> (4 cubic feet per minute per 100 square feet of conditioned space when tested at 25 pascals)	711
Duct Insulation	Supply and return ducts in attics shall be insulated to a minimum of R-8. Within ceiling insulation: R-8. Other locations not completely inside thermal envelope: R-8 where ≥3" in diameter and a minimum of R-6 where <3" in diameter. All other ducts not located completely inside the building thermal envelope shall be insulated to a minimum of R-6 where ≥3" in diameter and a minimum of R-4.2 where <3" in diameter.	711
Duct Location	50% in conditioned space, 50% unconditioned space	Program Design
Mechanical Ventilation	A continuous whole-house ventilation system with efficiency of 2.8 CFM/Watt and airflow defined by Table M1507.3.3(1) of 2015-IRCHRV/ERV/Air handler = 1.2 CFM/Watt In-line supply or exhaust = 3.8 CFM/Watt Other (< 90 CFM) = 2.8 CFM/Watt Other (≥ 90 CFM) = 3.5 CFM/Watt	4112
Lighting	Use baseline wattage as defined in the ENERGY STAR Lighting section. Use baseline wattage as defined in the Residential LED Lighting section of the TRM (2.1.1), Table 2-2 for the residential units, and Lighting Improvement section (3.1.1) and New Construction Lighting section (3.1.2) of the TRM for common spaces	
Appliances	Use baseline values as defined in applicable TRM measure for each appliance.	

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Data Point	Value	Source
Thermostat <u>SetbackType</u>	<u>MaintainProgrammable, with ability to maintain zone temperature down to 55 °F (13 °C) or up to 85 °F (29 °C)</u>	<u>711</u>
Temperature Set Points	Heating: 70°F Cooling: 78°F	<u>711</u>
<b>Heating Efficiency</b>		
Furnace	80% AFUE	<u>813</u>
Gas Fired Steam Boiler	82% AFUE	<u>813</u>
Gas Fired Hot Water Boiler	84% AFUE	<u>813</u>
Oil Fired Steam Boiler	85% AFUE	<u>813</u>
Oil Fired Hot Water Boiler	86% AFUE	<u>813</u>
<u>Combo Water Heater</u>	<u>76% AFUE (recovery efficiency)</u>	<u>8</u>
ASHP, GSHP, PTHP	<u>SeeFor residential units, see New Construction values in Table 2-8Table 2-10 in Sec. 2.2.4.2.2.1. For ductless heat pumps, use value for ASHP.</u> <u>For common areas, see New Construction values in Table 3-24 in Sec. 3.2.1. For ductless heat pumps, use value for ASHP.</u>	
<b>Cooling Efficiency</b>		
All types	<u>SeeFor residential units, see New Construction values in Table 2-10 in Sec. 2.2.4.2.2.1. For ductless heat pumps, use value for ASHP.</u> <u>For common areas, see New Construction values in Table 3-24 in Sec. 3.2.1. For ductless heat pumps, use value for ASHP. For Chillers, see values in Table 3-29 in Sec. 3.2.3.</u>	
<b>Domestic WH Efficiency</b>		
Electric	See volume and load dependent values in <u>Table 2-47in Table 2-61 in Sec. 2.3.4.2.3.1</u>	<u>9</u>
Natural Gas	See volume and load dependent values in <u>Table 2-132</u>	<u>913</u>
Additional Water Heater Tank Insulation	155 None	

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**Table 2-132: Baseline Insulation and Fenestration Requirements by Component for Buildings 4 Stories or Higher (Equivalent U-Factors)**<sup>Source 13</sup>

Building Element	IECC Climate Zone		
	4A	5A	6A
Fixed Fenestration U-Factor	0.38	0.38	0.36
Operable Fenestration U-Factor	0.45	0.45	0.43
Skylight U-Factor	0.50	0.50	0.50
Roof U-Factor, Insulation entirely above roof deck	0.032	0.032	0.032
Roof U-Factor, Metal building	0.035	0.035	0.035
Roof U-Factor, Attic and other	0.027	0.027	0.027
Above-Grade Wall U-Factor, Mass	0.090	0.080	0.071
Above-Grade Wall U-Factor, Metal building	0.052	0.052	0.052
Above-Grade Wall U-Factor, Metal framed	0.064	0.064	0.057
Above-Grade Wall U-Factor, Wood framed and other	0.064	0.064	0.051
Below-Grade Wall C-Factor	0.119	0.119	0.119
Floor U-Factor, Mass	0.074	0.064	0.057
Floor U-Factor, Joist/framing	0.033	0.033	0.033
Slab-on-grade Floors, F-Factor, Unheated	0.54	0.54	0.52
Slab-on-grade Floors, F-Factor, Heated	0.65	0.65	0.58

**Table 2-133: Residential New Construction Baseline Building Values for Buildings 4 Stories or Higher**

Data Point	Value	Source
Air Infiltration Rate	0.4 cfm/ft <sup>2</sup>	14
Duct Insulation	Supply and return ducts and plenums shall be insulated with a minimum of R-6 insulation where located in unconditioned spaces and where located outside the building with a minimum of R-8 insulation in Climate Zone 4A and a minimum of R-12 insulation in Zones 5A and 6A. Where located within the building envelope assembly, the duct or plenum shall be separated from the building exterior or unconditioned or exempt spaces by a minimum of R-8 insulation in Climate Zone 4A and a minimum of R-12 insulation in Zones 5A and 6A.	15
Mechanical Ventilation	0.35 ACH but not less than 15 cfm/person	16
Lighting	Use baseline wattage as defined in the ENERGY STAR Lighting section.	
Appliances	Use baseline values as defined in applicable TRM measure for each appliance.	
Thermostat Setback	Maintain zone temperature down to 55 °F (13 °C) or up to 85 °F (29 °C)	7

Data Point	Value	Source
Temperature Set Points	Heating: 70°F Cooling: 78°F	7
<b>Heating Efficiency</b>		
Furnace	80% AFUE	8
Gas-Fired Steam Boiler	82% AFUE	8
Gas-Fired Hot Water Boiler	84% AFUE	8
Oil Fired Steam Boiler	85% AFUE	8
Oil Fired Hot Water Boiler	86% AFUE	8
Combo Water Heater	76% AFUE (recovery efficiency)	8
ASHP, GSHP, PTHP	See New Construction values in Table 2-8 in Sec. 2.2.1. For ductless heat pumps, use value for ASHP.	
<b>Cooling Efficiency</b>		
All types	See New Construction values in Table 2-8 in Sec. 2.2.1. For ductless heat pumps, use value for ASHP.	
<b>Domestic WH Efficiency</b>		
Electric	See volume and load dependent values in Table 2-47 in Sec. 2.3.4	9
Natural Gas	See volume and load dependent values in Table 2-132	9
Additional Water Heater Tank Insulation	None	

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Table 2-134155: Minimum Residential Baseline Gas-Fired Uniform Energy Factors Based on Storage Volume and Draw Pattern

V <sub>i</sub> : Rated Storage Volume (gallons)	Draw Pattern	Max. Daily Hot Water Draw (gallons)	First Hour Rating (FHR) (gallons)	UEF Calculation
≥20 gal and ≤55 gal	Very Small	10	0 ≤ FHR < 18	0.3456 -(0.0020×V <sub>i</sub> )
	Low	38	18 ≤ FHR < 51	0.5982-(0.0019×V <sub>i</sub> )
	Medium	55	51 ≤ FHR < 75	0.6483-(0.0017×V <sub>i</sub> )
	High	84	FHR ≥ 75	0.6920-(0.0013×V <sub>i</sub> )
>55 gal and ≤120 gal	Very Small	10	0 ≤ FHR < 18	0.6470-(0.0006×V <sub>i</sub> )
	Low	38	18 ≤ FHR < 51	0.7689-(0.0005×V <sub>i</sub> )
	Medium	55	51 ≤ FHR < 75	0.7897-(0.0004×V <sub>i</sub> )
	High	84	FHR ≥ 75	0.8072-(0.0003×V <sub>i</sub> )
Instantaneous ≤2 gal and >50 kBtu/h	Very Small	10	0 ≤ FHR < 18	0.80
	Low	38	18 ≤ FHR < 51	0.81
	Medium	55	51 ≤ FHR < 75	0.81
	High	84	FHR ≥ 75	0.81

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**Table 2-156: Baseline Insulation and Fenestration Requirements by Component for Buildings 4 Stories or Higher (Equivalent U-Factors)**<sup>Source 14</sup>

Building Element	IECC Climate Zone	
	4	5
Fixed Fenestration U-Factor	0.36	0.36
Operable Fenestration U-Factor	0.45	0.45
Skylight U-Factor	0.50	0.50
Roof U-Factor, Insulation entirely above roof deck	0.032	0.032
Roof U-Factor, Metal building	0.035	0.035
Roof U-Factor, Attic and other	0.021	0.021
Above Grade Wall U-Factor, Mass	0.104	0.090
Above Grade Wall U-Factor, Metal building	0.052	0.050
Above Grade Wall U-Factor, Metal framed	0.064	0.055
Above Grade Wall U-Factor, Wood framed and other	0.064	0.051
Below Grade Wall C-Factor	0.119	0.119
Floor U-Factor, Mass	0.057	0.057
Floor U-Factor, Joist/framing	0.033	0.033
Slab-on-grade Floors, F-Factor, Unheated	0.52	0.52
Slab-on-grade Floors, F-Factor, Heated	0.62	0.62

**Table 2-157: Residential New Construction Baseline Building Values for Buildings 4 Stories or Higher**

Data Point	Value	Source
Air Infiltration Rate	0.3 cfm/ft <sup>2</sup>	15
Duct Insulation	Unconditioned spaces = R-6 Outside building = R-8 (zone 4) R-12 (zone 5)	16
Mechanical Ventilation	0.35 ACH but not less than 15 cfm/person	17
Lighting	Use baseline wattage as defined in the Residential LED Lighting section of the TRM (2.1.1), Table 2-2 for the residential units, and Lighting Improvement section (3.1.1) and New Construction Lighting section (3.1.2) of the TRM for common spaces	
Appliances	Use baseline values as defined in applicable TRM measure for each appliance.	
Thermostat Setback	Maintain zone temperature down to 55 °F (13 °C) or up to 85 °F (29 °C)	11
Temperature Set Points	Heating: 70°F Cooling: 78°F	11
<b>Heating Efficiency</b>		

Data Point	Value	Source
Warm air furnace, gas fired	81% E <sub>t</sub>	18
Warm air furnace, oil fired	82% E <sub>t</sub>	18
Boiler, hot water, gas fired	82% AFUE (< 300,000 Btu/h) 80% E <sub>t</sub> (≥ 300,000 Btu/h and ≤ 2,500,000 Btu/h) 82% E <sub>c</sub> (>2,500,000 Btu/h)	18
Boiler, hot water, oil fired	84% AFUE (< 300,000 Btu/h) 82% E <sub>t</sub> (≥ 300,000 Btu/h and ≤ 2,500,000 Btu/h) 84% E <sub>c</sub> (>2,500,000 Btu/h)	18
Boiler, steam, gas fired	80% AFUE (< 300,000 Btu/h) 79% E <sub>t</sub> (≥ 300,000 Btu/h)	18
Boiler, steam, oil fired	82% AFUE (< 300,000 Btu/h) 81% E <sub>t</sub> (≥ 300,000 Btu/h)	18
ASHP, GSHP, PTHP	For residential units, see New Construction values in Table 2-10 in Sec. 2.2.1. For ductless heat pumps, use value for ASHP. For common areas, see New Construction values in Table 3-24 in Sec. 3.2.1. For ductless heat pumps, use value for ASHP.	
<b>Cooling Efficiency</b>		
All types	For residential units, see New Construction values in Table 2-10 in Sec. 2.2.1. For ductless heat pumps, use value for ASHP. For common areas, see New Construction values in Table 3-24 in Sec. 3.2.1. For ductless heat pumps, use value for ASHP. For Chillers, see values in Table 3-29 in Sec. 3.2.3.	
<b>Domestic WH Efficiency</b>		
Electric	See volume and load dependent values in in Table 2-61 in Sec. 2.3.1	
Natural Gas	See volume and load dependent values in  155	19
Additional Water Heater Tank Insulation	None	

E<sub>t</sub> = Thermal Efficiency; E<sub>c</sub> = Combustion Efficiency

**Table 2-158: Minimum Commercial Baseline Gas- and Oil-Fired Uniform Energy Factors Based Fuel Type and Draw Pattern**

Equipment (specifications)	Draw Pattern	Max. Daily Hot Water Draw (gallons)	First Hour Rating (FHR) (gallons)	UEF Calculation*	
				Equipment Manufactured Before October 6, 2026	Equipment Manufactured After October 6, 2026
Gas-fired storage	Very Small	10	0 ≤ FHR < 18	0.2674 – (0.0009 × V <sub>r</sub> )	0.5374 – (0.0009 × V <sub>r</sub> )

Equipment specifications)	Draw Pattern	Max. Daily Hot Water Draw (gallons)	First Hour Rating (FHR) (gallons)	UEF Calculation*	
				Equipment Manufactured Before October 6, 2026	Equipment Manufactured After October 6, 2026
(>75 kBtu/h and ≤105 kBtu/h and ≤120 gal)	Low	38	18 ≤ FHR < 51	$0.5362-(0.0012 \times V_r)$	$0.8062-(0.0012 \times V_r)$
	Medium	55	51 ≤ FHR < 75	$0.6002-(0.0011 \times V_r)$	$0.8702-(0.0011 \times V_r)$
	High	84	FHR ≥ 75	$0.6597-(0.0009 \times V_r)$	$0.9297-(0.0009 \times V_r)$
Oil-fired storage (>105 kBtu/h and ≤40 kBtu/h and ≤120 gal)	Very Small	10	0 ≤ FHR < 18	$0.2932-(0.0015 \times V_r)$	$0.2932-(0.0015 \times V_r)$
	Low	38	18 ≤ FHR < 51	$0.5596-(0.0018 \times V_r)$	$0.5596-(0.0018 \times V_r)$
	Medium	55	51 ≤ FHR < 75	$0.6194-(0.0016 \times V_r)$	$0.6194-(0.0016 \times V_r)$
Electric instantaneous (>12 kW and ≤58.6 kW and ≤2 gal)	High	84	FHR ≥ 75	0.80	0.80
	Medium	55	51 ≤ FHR < 75	0.80	0.80
	Low	38	18 ≤ FHR < 51	0.80	0.80
Very Small	10	0 ≤ FHR < 18	0.80	0.80	

\* Vr is the rated storage volume (in gallons)

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify installation and proper selection of default values.

**SOURCES**

- 1) ENERGY STAR Multifamily New Construction Program Decision Tree. (2021, May). Weblink
- 2) International Code Council. (2021). 2021 International Energy Conservation Code, Effective Use of the International Energy Conservation Code, Introduction. Weblink
- 3) See the RESNET National Registry of Accredited Rating Software Programs for a complete listing: Weblink
- 4) Passive House Planning Package. Weblink
- 5) WUFI Passive. Weblink
- 6) See the ENERGY STAR Multifamily New Construction Simulation Guidelines for guidance on qualifying software: Weblink
- 1) Calculation of annual energy consumption of a baseline home from the home energy rating tool based on the reference home energy characteristics.
- 2) Calculation of annual energy consumption of an energy-efficient home from the home energy rating tool based on the qualifying home energy characteristics
- 3) Calculation of peak load of baseline home from the home energy rating tool based on the reference home energy characteristics.
- 4) "Methodology for Calculating Cooling and Heating Energy Input Ratio (EIR) from the Rated Seasonal Performance Efficiency (SEER OR HSPF)" (Kim, Baltazar, Haberl). April 2013 Accessed December 2018. <http://oaktrust.library.tamu.edu/bitstream/handle/1969.1/152118/ESL-TR-13-04-01.pdf>

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- ~~5)8) Calculation of peak load of energy efficient home from the home energy rating tool based on the qualifying home energy characteristics.~~
- ~~6) SEER of HVAC unit in energy efficient qualifying home.~~
- ~~9) 2015 Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. Weblink~~
- ~~10) 2021 International Energy Conservation Code Table R402.1.2 Maximum Assembly U-Factors and Fenestration Requirements presents the R-Value requirements of Table R402.1.3 in an equivalent U-Factor format. Users may choose to follow Table R402.1.2 instead. 2021 IECC supersedes this table in case of discrepancy. Additional requirements per §R402 of 2021 IECC must be followed even if not listed here. Weblink~~
- ~~7)11) 2021 International Energy Conservation Code §R401-R404.  
<https://codes.iccsafe.org/content/IECC2015/chapter-4-re-residential-energy-efficiency>  
Weblink~~
- ~~12) 2021 International Residential Code, Table N1103.6.2(R403.6.2): Whole-Dwelling Mechanical Ventilation System Fan Efficacy. Weblink~~
- ~~13) Electronic Code of Federal Regulations, 10 CFR Part 430, Subpart C, §430.32, "Energy and water conservation standards and their compliance dates." Weblink.~~
- ~~8) 2021 International Energy Conservation Program for Consumer Products: Energy and Water Conservation Standards." [https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.430#se10.3.430\\_132](https://www.ecfr.gov/cgi-bin/retrieveECFR?n=pt10.3.430#se10.3.430_132). Current as Code Tables C402.4 and C402.1.4. Users may choose to follow Table C402.1.3 instead of November 13, 2018.~~
- ~~9) US Federal Standards for Residential Water Heaters. Effective April 16, 2015.  
<https://www.ecfr.gov/cgi-bin/retrieveECFR?n=sp10.3.430.c&r=SUBPART>~~
- ~~10)14) 2015 International Energy Conservation Code Table R402.1.4 Equivalent U-Factors presents the R-Value requirements of Table R402.1.2 in an equivalent U-Factor format. Users may choose to follow Table R402C402.1.2 instead. 20154. 20121 IECC supersedes this table in case of discrepancy. Additional requirements per §R402C402 of 201520121 IECC must be followed even if not listed here.  
<https://codes.iccsafe.org/content/IECC2015/chapter-4-re-residential-energy-efficiency>Weblink~~
- ~~11) 2015 International Residential Code, Table M1507.3.3(1): Continuous Whole-House Mechanical Ventilation System Airflow Rate Requirements.  
<https://codes.iccsafe.org/content/IRC2015/chapter-15-exhaust-systems>~~
- ~~12) EPA ENERGY STAR Multifamily New Construction Program Decision Tree, Version 1.4.  
[https://www.energystar.gov/sites/default/files/asset/document/MFHR%20Flowchart\\_v1%204-Mar2020.pdf](https://www.energystar.gov/sites/default/files/asset/document/MFHR%20Flowchart_v1%204-Mar2020.pdf)~~
- ~~13) 2015 International Energy Conservation Code Table C402.1.4 Equivalent U-Factors presents the R-Value requirements of Table C402.1.3 in an equivalent U-Factor format. Users may choose to follow Table C402.1.3 instead. 2015 IECC supersedes this table in case of discrepancy. Additional requirements per §C402 of 2015 IECC must be followed even if not listed here. <https://codes.iccsafe.org/content/IECC2015/chapter-4-ce-commercial-energy-efficiency>.~~
- ~~14) 2015 International Energy Conservation Code §C403.2.9.  
<https://codes.iccsafe.org/content/IECC2015/chapter-4-ce-commercial-energy-efficiency>.~~
- ~~15) 20152021 International Energy Conservation Code §C402.5.  
<https://codes.iccsafe.org/content/IECC2015/chapter-4-ce-commercial-energy-efficiency-2>  
Weblink~~

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16) ~~2015~~2021 International Energy Conservation Code §C403.12.1. Weblink

16)17) 2021 International Mechanical Code, Table 403.3.1.1: Minimum Ventilation Rates.  
<https://codes.iccsafe.org/content/IMC2015/chapter-4-ventilation>.Weblink

18) 2021 International Energy Conservation Code §C403.3.2. Weblink

19) Electronic Code of Federal Regulations, 10 CFR Part 431, Subpart G, §431.110. Weblink



## 2.7.2 ENERGY STAR MANUFACTURED HOMES

Target Sector	Manufactured homes
Measure Unit	Variable
Measure Life	15 Years <sup>Source #31</sup>
Vintage	New Construction

### ELIGIBILITY

### ELIGIBILITY

This measure applies to manufactured homes compliant to and certified by EPA's ENERGY STAR Manufactured Home<sup>2</sup>Homes program standard, [Version 3](#).

### ALGORITHMS

Energy and peak demand savings in the ENERGY STAR Manufactured Homes [programsprogram](#) will be calculated by comparing outputs of energy models of the as-designed home to a minimally code-compliant baseline home.

Modeled energy and peak demand savings shall be produced by a RESNET accredited software program.<sup>90</sup> [Source 2](#)

For ENERGY STAR Manufactured Homes, the baseline building thermal envelope and/or system characteristics shall be based on the current Manufactured Homes Construction and Safety Standards (HUD Code).<sup>Source 3</sup> For this measure, a "manufactured home" means a structure, transportable in one or more sections, which in the traveling mode, is eight body feet or more in width or forty body feet or more in length, or, when erected on site, is three hundred twenty or more square feet, and which is built on a permanent chassis and designed to be used as a dwelling with or without a permanent foundation when connected to the required utilities, and includes the plumbing, heating, air conditioning, and electrical systems contained ~~therein.~~"[in the structure.](#)"<sup>Source 443</sup>

Energy savings will be calculated from the software output using the following algorithm:

*Energy savings of the qualified home (kWh/yr)*

$$\Delta kWh = kWh_{base} - kWh_q$$

~~Peak-If the modeling software provides building-level outputs of hourly energy consumption (an 8760 load profile), then coincident peak demand savings are based on reduction in peak cooling loads. The RESNET accredited may be calculated by averaging the hourly energy savings during the TRM defined peak demand time period.~~

~~If the modeling software does not offer output to allow calculations provide building-level outputs of hourly energy consumption, the system peak electric demand savings for end-uses other than cooling equipment, which is assumed to be active during the peak period, shall be calculated from the software's calculated annual energy savings and the following algorithm:~~

<sup>90</sup> See the RESNET National Registry of Accredited Rating Software Programs for a complete listing: <http://www.resnet.us/professional/programs/energy-rating-software>

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Coincident system peak electric demand savings (kW)

$$\Delta kW_{\text{summer peak}} = \Delta kWh \times ETRDF_{\text{summer}}$$

$$\Delta kW_{\text{winter peak}} = \Delta kWh \times ETRDF_{\text{winter}}$$

Additional demand savings may be claimed under this measure, but these additional demand savings must be calculated using the algorithms from the applicable measure elsewhere in the TRM. For example, to claim demand savings from a refrigerator, demand savings for that end use must be calculated using the demand savings algorithms in Sec. ~~2.4.1 ENERGY STAR Refrigerators~~ 2.4.1 ENERGY STAR Refrigerators. Claiming additional demand savings may require additional EDC data collection than required to generate the energy model.

**DEFINITION OF TERMS**

The system peak electric demand savings for will be calculated from the software output with the following algorithm:

~~Peak demand of the baseline home~~

$$= \frac{PL_{\text{base}}}{EER_{\text{base}}}$$

~~Peak demand of the qualifying home~~

$$= \frac{PL_q}{EER_q}$$

~~Coincident system peak electric demand savings (kW)~~

$$\Delta kW_{\text{peak}} = (\text{Peak demand of the baseline home} - \text{Peak demand of the qualifying home})$$

**DEFINITION OF TERMS**

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**Table 2-159: ENERGY STAR: Terms, Values, and References for Manufactured Homes—References**

Term	Unit	Value	Sources
$kWh_{baseline}$ Estimated annual energy consumption of the baseline home	kWh	Software Calculated	4
$kWh_{qt}$ Estimated annual energy consumption of the qualifying home	kWh	Software Calculated	4
$PL_{br}$ Estimated peak cooling load of the baseline home	kBTU/h	Software Calculated	4
$PL_{qt}$ Estimated peak cooling load for the qualifying home.	kBTU/h	Software Calculated	4
$EER_{br}$ Energy Efficiency Ratio of the baseline unit.	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: $-0.0228 \times SEER_{base}^2 + 1.1522 \times SEER_{base}$	2
$EER_{qt}$ Energy Efficiency Ratio of the qualifying unit.	$\frac{BTU}{W \cdot h}$	EDC Data Gathering Default: $-0.0228 \times SEER_{qt}^2 + 1.1522 \times SEER_{qt}$	2
$SEER_{br}$ Seasonal Energy Efficiency Ratio of the baseline unit.	$\frac{BTU}{W \cdot h}$	13 14 (ASHRAE)	3
$SEER_{qt}$ SEER associated with the HVAC system in the qualifying home.	$\frac{BTU}{W \cdot h}$	EDC Data Gathering	4
$V_r$ , Rated storage volume of baseline water heater	gallons	EDC Data Gathering	EDC Data Gathering
Model inputs for baseline home	Varies	See Table 2-134133	

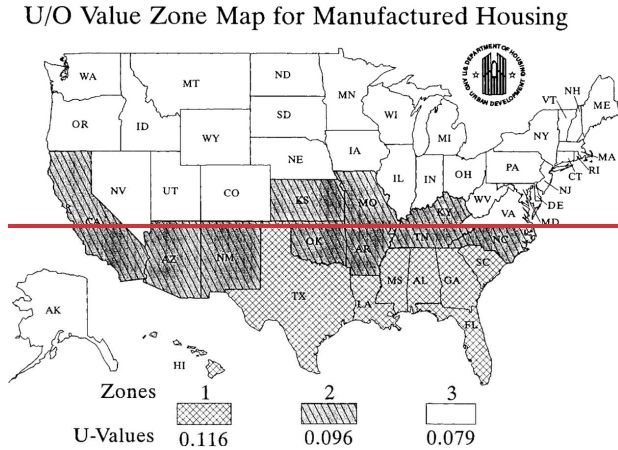
The HUD Code defines required insulation levels as an average envelope  $U_0$  factor per zone. In Pennsylvania zone 3 requirements apply with a required  $U_0$  factor of 0.079. This value cannot be directly used to define a baseline envelope R-values because the  $U_0$  factor is dependent on both the size of the manufactured homes and insulating levels together. However, because manufactured homes are typically built to standard dimensions baseline  $U$ -factors can be estimated with reasonable accuracy.

Figure $kWh_{baseline}$ Estimated annual energy consumption of the baseline home	kWh	Software Calculated	
$kWh_{qt}$ Estimated annual energy consumption of the qualifying home	kWh	Software Calculated	
$ETDF_{peak,summer}$ Summer energy to demand factor	kW/kWh	0.0001376	4
$ETDF_{peak,winter}$ Winter energy to demand factor	kW/kWh	0.0001967	4
Model inputs for baseline home	Varies	See Table 2-160 and Table 2-161	
Model inputs for ENERGY STAR home	Varies	See Table 2-162 and Table 2-163	

Federal energy code for manufactured homes provides both a prescriptive and a performance-based path to meet required insulation levels. Table 2-160 and presents the minimum requirements

for manufactured homes that are manufactured on or after July 1, 2025. Additional federal energy code requirements and TRM assumed baseline values are presented in Table 2-161.

**Table 2-6: U<sub>e</sub>160: Building Thermal Envelope Requirements for Code-Compliant Baseline Requirements<sup>91</sup>**



The HUD Code required insulation levels can be expressed as a set of estimated envelope parameters. Using typical manufactured home sizes, these values are included below along with federal standard baseline parameters below in Table 2-134133.

	Single-section home	Multi-section home
<b>Prescriptive Requirements</b>		
Exterior wall insulation R-value	19	21
Exterior ceiling insulation R-value	22	38
Exterior floor insulation R-value	22	30
Window U-factor	0.35	0.30
Skylight U-factor	0.55	0.55
Door U-factor	0.40	0.40
<b>Prescriptive Requirements – Alternatives to R-Value Requirements</b>		
Exterior ceiling U-factor	0.061	0.037
Exterior wall U-factor	0.068	0.063
Exterior floor U-factor	0.049	0.032
<b>OR Performance Requirements</b>		
Overall thermal transmittance (U <sub>e</sub> )	0.074	0.055

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<sup>91</sup> 24 CFR Part 3280-MANUFACTURED HOMES CONSTRUCTION AND SAFETY STANDARD  
 (<http://www.gpo.gov/fdsys/pkg/CFR-2013-title24-vol5/pdf/CFR-2013-title24-vol5-part3280.pdf>)

**Table 2-161: ENERGY STAR Manufactured Homes – User-Defined Reference: Values and References for Code-Compliant Baseline Home**

Data-Point	Value <sup>92</sup>	Source
Walls	U-factor 0.090	6, 7
Ceilings	U-factor 0.045	6, 7
Floor	U-factor 0.045	6, 7
Windows	U-factor 0.59	6, 7
Doors	U-factor 0.33	6, 7
Air Infiltration Rate	10 ACH50	6
Duct Leakage	Approved model package default	6
Duct Insulation	Approved model package default	6
Duct Location	Supply 100% manufactured home belly, Return 100% conditioned space	8
Data Point	Value	Source
<u>Air Infiltration Rate</u>	<u>5 ACH50</u>	<u>6</u>
Mechanical Ventilation	0.035 CFM/ft <sup>2</sup> Exhaust	7
Lighting	Use baseline wattage as defined in the ENERGY STAR Lighting section.	
<u>Mechanical Ventilation Fan Efficacy</u>	<u>HRV or ERV = 1.2 CFM/W</u> <u>Inline supply/exhaust: 3.8 CFM/W</u> <u>Other exhaust &lt; 90 CFM = 2.8 CFM/W</u> <u>Other exhaust ≥90 CFM = 3.5 CFM/W</u> <u>Air-handler that is integrated to tested and listed HVAC equipment = 1.2 CFM/W</u>	<u>8</u>
<u>Duct Leakage</u>	<u>4 CFM25 / 100 ft<sup>2</sup> conditioned floor area</u>	<u>8</u>
<u>Lighting</u>	<u>Use baseline wattage as defined in the Residential LED Lighting section of the TRM (2.1.1), Table 2-2.</u>	
Appliances	Use baseline values as defined in applicable TRM measure for each appliance.	
<u>Thermostat Setback</u>	<u>Non-Programmable thermostat</u>	<u>6</u>
<u>Temperature Set Points</u>	Heating: 70°F Cooling: 78°F	10
<u>Thermostat Type</u>	<u>Programmable, with ability to maintain zone temperature down to 55 °F (13 °C) or up to 85 °F (29 °C)</u>	<u>9</u>
<u>Temperature Set Points</u>	Heating: 70°F Cooling: 78°F	<u>9</u>
Heating Efficiency		
<u>Furnace</u>	<u>80% AFUE</u>	<u>3</u>
<u>Gas Fired Steam Boiler</u>	<u>82% AFUE</u>	<u>3</u>

<sup>92</sup> Single and multiple family as noted.

Data Point	Value <sup>62</sup>	Source
Gas Fired Hot Water Boiler	84% AFUE	3
Oil Fired Steam Boiler	85% AFUE	3
Oil Fired Hot Water Boiler	86% AFUE	3
Combo Water Heater	76% AFUE (recovery efficiency)	3
Electric Resistance	3.412 HSPF	7
ASHP, GSHP, PTHP, Ductless heat pump	See New Construction values in Table 2-8 in Sec. 2.2.1. For ductless heat pumps, use value for ASHP.	
Furnace	80% AFUE	10
Gas Fired Steam Boiler	82% AFUE	10
Gas Fired Hot Water Boiler	84% AFUE	10
Oil Fired Steam Boiler	85% AFUE	10
Oil Fired Hot Water Boiler	86% AFUE	10
Combo Water Heater	76% AFUE (recovery efficiency)	10
Electric Resistance	3.412 HSPF	
ASHP, GSHP, PTHP, Ductless heat pump	See New Construction values in Table 2-10 in Sec. 2.2.1	AEPS Application; EDC Data Gathering
<b>Cooling Efficiency</b>		
All types	See New Construction values in Table 2-8 in Sec. 2.2.1. For ductless heat pumps, use value for ASHP.	
All types	See New Construction values in Table 2-10 in Sec. 2.2.1	AEPS Application; EDC Data Gathering
<b>Domestic WH Efficiency</b>		
Electric	See volume and load dependent values in Table 2-47 Table 2-61 in Sec. 2.3.12.3.1	44
Natural Gas	See volume and load dependent values in Table 2-132 155 in Sec. 2.7.12.7.1	44
Additional Water Heater Tank Insulation	None	42
Additional Water Heater Tank Insulation	None	

The ENERGY STAR Manufactured Homes program provides a list of requirements for certified homes to meet. Below is a summary of those requirements. <sup>Source 11</sup>

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**Table 2-162: Building Thermal Envelope Requirements for ENERGY STAR Manufactured Home** Source 11

	Single-section home	Multi-section home
<b>Prescriptive Requirements</b>		
Exterior wall insulation R-value		R-21
Exterior ceiling insulation R-value		R-38
Exterior floor insulation R-value		R-33
Window U-factor		0.30
Door U-factor		0.30
<b>OR Performance Requirements</b>		
Single-section overall thermal transmittance ( $U_o$ )	0.057	0.054

Additionally, the ENERGY STAR Manufactured Homes program requires that ducts in floor cavities shall be enclosed by floor insulation and that crossover ducts, ducts in unconditioned attics, and other ducts in unconditioned space shall have at least R-8 duct insulation.

For only multi-section manufactured homes, ENERGY STAR requires additional energy efficiency measures to the required measures listed above. These additional measures are each assigned a point value. The points must sum to at least the program minimum total of 10 points. Table 2-163 presents the point values for climate zone 3.

**Table 2-163: ENERGY STAR Manufactured Homes Program Optional Measure Point Values for Multi-Section Homes**

Energy Efficiency Measure	Point Value
<b>Mandatory requirements</b>	
All requirements in Table 2-162	2.0
<b>Optional Envelope Improvements</b>	
Coefficient of heat transmission ( $U_o$ ) $\leq$ 0.049	4.5
<b>Optional Heating and Cooling Equipment</b>	
Heat pump $\geq$ 7.5 HSPF2 / 14.3 SEER2	17.0
Gas / propane Furnace $\geq$ 90 AFUE	5.5
Gas / propane Furnace $\geq$ 95 AFUE	7.5
Gas / propane Furnace $\geq$ 96 AFUE	8.5
<b>Optional Water Heater Equipment</b>	
Gas / Propane Water Heater $\geq$ 0.93 UEF	0.5
Heat pump water heater $\geq$ 2.20 UEF	1.5
Heat pump water heater $\geq$ 3.30 UEF	1.5
Heat pump water heater $\geq$ 2.20 UEF	7.5
Heat pump water heater $\geq$ 3.30 UEF	9.0
<b>Optional Lighting, Appliances, and Water Fixtures</b>	
LED lighting installed in all permanently installed fixtures	0.5
Bathroom faucets $\leq$ 1.5 gallons per minute (gpm) and showerheads $\leq$ 2.0 gpm	0.5
ENERGY STAR certified refrigerator and dishwasher	0.5
ENERGY STAR certified clothes washer	0.5

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**EVALUATION PROTOCOLS**

The most appropriate evaluation protocol for this measure is verification of installation coupled with EDC data gathering.

## SOURCES

- 1) ~~Calculation of annual energy and peak load consumption of a baseline home from the home energy rating tool based on the reference home energy characteristics.~~
- 2) ~~“Methodology for Calculating Cooling and Heating Energy Input Ratio (EIR) from the Rated Seasonal Performance Efficiency (SEER-OR HSPF)” (Kim, Baltazar, Haberl). April 2013 Accessed December 2018.  
<http://oaktrust.library.tamu.edu/bitstream/handle/1969.1/152118/ESL-TR-13-04-01.pdf>~~
- 1) ~~Hewes, T. and Peeks, B. (2013, February). “Northwest Energy Efficient Manufactured Housing Program Specification Development”. NREL. Weblink. Note: this reference provides measure lives of major home components and not a single home-wide measure life. The ENERGY STAR Manufactured Home program’s requirements and optional measures focus on the building’s envelope and HVAC system, which have measure lives of 45 years and 20 years, respectively. Therefore, the aggregate life for this measure is considered to be 30 years. Note that PA Act 129 savings can be claimed for no more than 15 years, thus the 15 year measure life.~~
- 2) ~~See the RESNET National Registry of Accredited Rating Software Programs for a complete listing: [Weblink](#).~~
- 3) ~~Electronic Code of Federal Regulations, 24 CFR Part 3280, “Manufactured Home Construction and Safety Standards.” [Weblink](#)~~
- 4) ~~Wilson et al. 2021. End-Use Load Profiles for the U.S. Building Stock: Methodology and Results of Model Calibration, Validation, and Uncertainty Quantification. NREL/TP-5500-80889. [Weblink](#)~~
- 5) ~~Electronic Code of Federal Regulations, 10 CFR Part 460, §460.102. “Building Thermal envelope requirements.” All values shown are applicable to climate zone 3, which includes all of Pennsylvania. [Weblink](#).~~
- 6) ~~U.S. Department of Energy. Energy Conservation Program. Energy Conservation Standards for Manufactured Housing. Effective August 1, 2022. [Weblink](#)~~
- 7) ~~Electronic Code of Federal Regulations, 24 CFR Part 3280, Subpart B, §3280.103(b). [Weblink](#).~~
- 8) ~~2021 International Residential Code, Table N1103.6.2(R403.6.2): Whole-Dwelling Mechanical Ventilation System Fan Efficacy. [Weblink](#)~~
- 9) ~~Electronic Code of Federal Regulations, 10 CFR Part 460, §460.202. “Thermostats and controls.” [Weblink](#).~~
- 3)10) ~~Electronic Code of Federal Regulations, 10 CFR Part 430, Subpart C, §430.32, “Energy Conservation Program for Consumer Products: Energy and Water Conservation Standards.” <https://www.ecfr.gov/cgi-bin/retrieveECFR?&n=pt10.3.430#se10.3.430-132>[Weblink](#). Current as of November 13, 2018.~~
- 4) ~~SEER of HVAC unit in energy efficient qualifying home.~~
- 5) ~~Straub, Mary and Switzer, Sheldon. “Using Available Information for Efficient Evaluation of Demand Side Management Programs”. Study by BG&E. The Electricity Journal. Aug/Sept, 2011, p. 95. <http://www.sciencedirect.com/science/article/pii/S1040619011001941>~~
- 6) ~~ENERGY STAR QUALIFIED MANUFACTURED HOMES-Guide for Retailers with instructions for installers and HVAC contractors / June 2007 / ([http://www.research-alliance.org/pages/es\\_retail.htm](http://www.research-alliance.org/pages/es_retail.htm))~~



- ~~7) Electronic Code of Federal Regulations, 24 CFR Part 3280, Manufactured Home Construction and Safety Standards. <https://www.ecfr.gov/cgi-bin/retrieveECFR?&n=pt24.5.3280> Accessed November 16, 2018.~~
- ~~8) Standard manufactured home construction~~
- ~~9) Not a requirement of the HUD Code.~~
- ~~10) 2015 International Energy Conservation Code §R401-R404.~~
- ~~11) US Federal Standards for Residential Water Heaters. Effective April 16, 2015. <https://www.ecfr.gov/cgi-bin/retrieveECFR?n=sp10.3.430.c&r=SUBPART>~~
- ~~12) No requirement in code or federal regulation.~~
- ~~13) NREL, Northwest Energy Efficient Manufactured Housing Program Specification Development, T. Huges, B. Peeks February 2013. <http://www.nrel.gov/docs/fy13osti/56761.pdf>~~

11) ENERGY STAR Manufactured New Homes National Program Requirements, Version 3 (Rev. 01). Weblink

### 2.7.3 HOME ENERGY REPORTS

Target Sector	Residential <del>Establishments</del>
Measure Unit	Household
Measure Life	Specified in protocol
Vintage	Retrofit

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Home Energy Report (HER) programs encourage conservation through greater awareness of consumption patterns and engagement with EDC resources to help reduce usage and lower bills. HER program vendors provide participants with account-specific information that allows customers to view various aspects of their energy use over time. Behavioral reports compare energy use of recipient homes with clusters of similar homes and provide comparisons with other efficient and average homes. This so-called “neighbor” comparison is believed to create cognitive dissonance in participants and spur them to modify their behavior to be more efficient. Reports also include a variety of seasonally appropriate energy-saving tips that are tailored for the home and are often used to promote other EDC program offerings. Historically, HERs have been largely issued on paper via the USPS, but EDCs and their vendors are increasingly moving toward email reports and digital portals to promote increased engagement and conserve resources. This protocol applies to residential HER programs regardless of delivery mode.

A growing list of evaluation studies, including analyses of HER persistence by the Phase II and Phase III Pennsylvania Statewide Evaluation team, have observed energy savings among HER recipient households for two years after HER exposure was discontinued. The persistence of HER savings has implications for calculation of first-year energy savings and cost-effectiveness. This protocol provides guidance to EDCs and their evaluation contractors for calculating first-year incremental savings and lifetime savings from HER programs using a multi-year measure life with “decay” perspective. ~~This multi-year persistence perspective is a departure from prior phases of Act 129, which assumed a 1-year measure life for HER programs.~~

Because Act 129 goals are based on first-year incremental savings, accounting for persistence ~~will yield reduced~~ reduces first-year compliance savings from EDC programs that continue to expose the same homes to HER messaging year after year.

The core assumption in this protocol is an annual decay rate of 31.3%. To illustrate the ~~decay~~ concept of decay, consider a hypothetical cohort of 20,000 treatment group homes that have been receiving HERs for two years. ~~Table 2-135~~ Table 2-164 shows the average kWh savings per treatment group home by year as measured through a billing analysis of the randomized control trial design.

Table 2-164: Home Energy Report Persistence Example

Year	Avg. kWh Savings per Home
1	150
2	250

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For Year 3, the EDC can choose to either continue issuing HERs to the treatment group homes or stop treating them. If the EDC stops issuing HERs to the treatment group in Year 3, little or no cost will be incurred. If the EDC continues issuing HERs to the treatment group in Year 3, a full year of

program delivery costs will be incurred. The key question is “what are the incremental energy savings associated with the decision to mail HERs in Year 3?” Table 2-165 shows the components of this calculation.

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**Table 2-165: Calculation of Avoided Decay and Incremental Annual Compliance Savings**

Year	Avg. kWh Savings per Home	Avg. kWh Savings Absent Year 3 Treatment	Avg. kWh Savings with Year 3 Treatment
1	150		
2	250		
3		$250 \times (1 - 0.313/2) = 210.9$	260

In this hypothetical example the incremental first-year savings achieved by the HER program in Year 3 is 49.1 kWh (260 – 210.9). This is the sum of two separate factors.

- **Avoided Decay** = 39.1 kWh. The avoided decay is the difference between the Year 2 savings and the assumed annual rate of decay. Because the decay rate is assumed to be linear the average amount of decay over the year is equal to half of the decay at the end of the year. The 210.9 kWh value in Table 2-165 is an estimate of what would have happened absent any further program effort. Some kWh savings persist, but at a lower rate than observed in Year 2, when households were actively receiving HER messaging. By continuing to issue HERs in Year 3, the EDC avoids this savings decay.
- **Change in the Average Treatment Effect** = 10 kWh. The “Avg. kWh Savings with Year 3 Treatment” column of Table 2-165 shows an average kWh savings value of 260 kWh per household. This is an increase of 10 kWh over the Year 2 measurement of 250 kWh per household. Many HER programs show growth in the average rate of savings over time as participants continue to respond to the messaging. This component of the calculation of the calculation could also be negative if the Year 3 savings measurement was smaller than the Year 2 measurement. HER savings can fluctuate based on weather and the measurement is inherently noisy because of the small effect size.

The following algorithms and default assumptions provide guidance on calculating and reporting compliance savings from HER programs in Phase IV of Act 129. Several assumptions that straddle technical and policy considerations are listed below.

~~1) The change in perspective from a 1-year EUL to a multi-year with decay approach creates an issue of unaccounted for lifetime savings from Phase III HER programs. Specifically, HER cohorts that were active in PY12 will be assumed to have persistent savings in PY13 even though persistent savings were not accounted for in Phase III TRC calculations. This is unavoidable with a change in accounting methods and best handled at the beginning of a Phase IV. It has no bearing on Phase III compliance savings.~~

2) The assumed annual rate of decay for Act 129 HER programs is based on an analysis of mature programs where treatment group homes received HER messaging for multiple years. Studies have also consistently shown that it takes time for HER savings to mature. For Phase IV of Act 129, new HER cohorts will continue to assume a 1-year EUL during the first year of HER exposure. The persistence and decay assumptions outlined in this protocol will take effect for Year 2 of exposure. Years of exposure are mapped to Act 129 program years. If a cohort begins receiving HER messaging in December (halfway through the program year), that program year is still Year 1, and the following program year is Year 2 with regard to application of persistence assumptions.

- 3)2) Act 129 HER programs should always be delivered as a randomized control trial (RCT), but EDCs have significant flexibility in designing new HER cohorts. New cohorts can be composed of a mix of past HER recipients and control group homes or non-recipients. Randomization should ensure a balanced mix across the new treatment and control group and the billing analysis will capture the savings associated with exposing the new treatment group to HERs, but not the control group. When a new cohort is created, accounting always begins at Year 1, even if some of the treatment and control group homes have received HER messaging previously.
- 4)3) Over time, households close their EDC accounts. The most common reason is because the occupant is moving, but other possibilities exist. This account “churn” happens at a fairly predictable rate for an EDC service territory and can be forecasted with some degree of certainty. Calculating persistent HER savings in future program years requires both an assumption of the savings decay rate and an assumption of the churn rate.
- 5)4) Home Energy Reports are expected to generate summer and winter peak demand savings. The Behavioral Conservation Programs protocol of the Pennsylvania Evaluation Framework provides detailed guidance regarding measurement techniques for peak demand savings. Peak demand (kW) savings are presumed to follow the same persistence logic as energy (kWh) savings with respect to first-year incremental compliance and lifetime impacts.

#### ALGORITHMS

The equations for incremental first-year savings from HER programs are:

##### Year 1 and 2 of HER Exposure:

$$\Delta kWh_x = ATE_y * Treatment\ Accounts_y * Days_y$$

$$FYSATE_y = ATE_y$$

$$\Delta kWh_y = ATE_y * Treatment\ Accounts_y * Days_y$$

$$FYSATE_y = ATE_y$$

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Where  $ATE_y$  is the average daily savings determined through a billing regression analysis, minus the average daily uplift (kWh/day). The uplift of the HER program is determined by examining the cumulative difference in other EE program savings between the treated population and the control group since the inception of the HER cohort. In years 1 and 2 of HER exposure the  $ATE_y$  and  $FYSATE_y$  terms are identical.

If an EDC elects to treat an HER cohort for a 3<sup>rd</sup> year or beyond the equation for incremental first-year savings is:

##### Year 3 of HER Exposure:

$$FYSATE_y = ATE_y - \sum_{x=1}^{x-1} FYSATE_{y-x} - FYSATE_{y-x} * Decay * (X - 0.5)$$

$$\Delta kWh_x = FYSATE_y * Treatment\ Accounts_y * Days_y$$

$$FYSATE_y = ATE_y - \sum_{x=1}^{x-1} FYSATE_{y-x} - FYSATE_{y-x} * Decay * (X - 0.5)$$

$$\Delta kWh_y = FYSATE_y * Treatment\ Accounts_y * Days_y$$

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**Year 4 of HER Exposure:**

$$\begin{aligned}
 FYSATE_y &= ATE_y - \sum_{x=1}^{x=2} FYSATE_{y-x} - FYSATE_{y-x} * Decay * (X - 0.5) \\
 \Delta kWh_y &= FYSATE_y * Treatment\ Accounts_y * Days_y \\
 FYSATE_y &= ATE_y - \sum_{x=1}^{x=2} FYSATE_{y-x} - FYSATE_{y-x} * Decay * (X - 0.5) \\
 \Delta kWh_y &= FYSATE_y * Treatment\ Accounts_y * Days_y
 \end{aligned}$$

**Year 5 and Beyond of HER Exposure:**

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$$\begin{aligned}
 FYSATE_y &= ATE_y - \sum_{x=1}^{x=3} FYSATE_{y-x} - FYSATE_{y-x} * Decay * (X - 0.5) \\
 \Delta kWh_y &= FYSATE_y * Treatment\ Accounts_y * Days_y \\
 FYSATE_y &= ATE_y - \sum_{x=1}^{x=3} FYSATE_{y-x} - FYSATE_{y-x} * Decay * (X - 0.5) \\
 \Delta kWh_y &= FYSATE_y * Treatment\ Accounts_y * Days_y
 \end{aligned}$$

Where FYSATE<sub>y</sub> is the average daily savings attributable to HERs delivered in year Y and FYSATE<sub>y-x</sub> is the average daily savings attributable to HERs delivered in year Y-X.

The equations for calculating lifetime savings from a program year of HER exposure are given below. For Year 1, the lifetime savings are equal to the first-year savings. For the Year 2 and beyond of HER exposure the lifetime savings include both the savings measured at the meter via billing analysis and persistent savings from future program years. The equations below do not include the discount rate, but EDC evaluation contractors should use an approved discount rate to calculate the net present value of future savings when performing the TRC test.

**Year 1 of HER Exposure (where Y = 1):**

$$\begin{aligned}
 \Delta kWh_{y,lifetime} &= ATE_y * Treatment\ Accounts_y * Days_y \\
 \Delta kWh_{y,lifetime} &= ATE_y * Treatment\ Accounts_y * Days_y
 \end{aligned}$$

**Year 2 and Beyond of HER Exposure (where Y >= 2):**

$$\begin{aligned}
 \Delta kWh_{y,lifetime} &= \Delta kWh_y + \sum_{x=1}^{x=3} ((FYSATE_y - FYSATE_y * Decay * (X - 0.5)) * (1 - Churn)^x) \\
 &\quad * Days_{y+x} * Treatment\ Accounts_y \\
 \Delta kWh_{y,lifetime} &= \Delta kWh_y + \sum_{x=1}^{x=3} ((FYSATE_y - FYSATE_y * Decay * (X - 0.5)) \\
 &\quad * (1 - Churn)^x) * Days_{y+x} * Treatment\ Accounts_y
 \end{aligned}$$

For year two and onwards, the lifetime savings are simply a function of the decay rate and customer churn assumption, accounted for the current year and across the three future years where savings persist. In this case, it may be helpful to consider the sum in the formula above a scalar that adjusts

that program year’s savings. For example, in a hypothetical program with 200 kWh of total incremental annual savings in its second year of program delivery, the lifetime savings associated with the second year of program year delivery would be  $200 * 2.44 = 488\text{kWh}$ , where the 2.44 factor is the ratio of the lifetime savings to the incremental first-year savings. The 2.44 approximation factor is valid for programs that rely on the default decay and churn assumptions. EDCs that use the ‘EDC Data Gathering’ option for one or both of these parameters would need to calculate the appropriate lifetime: first-year ratio for the parameter values selected.

**DEFINITION OF TERMS**

**Table 2-166: Terms, Values, and References for HER Persistence Protocol**

Parameter	Unit	Value	Source
$\Delta kWh_y$ , First-year compliance kWh savings for the cohort being evaluated in the program year being analyzed	Total Incremental Annual kWh Savings of an HER cohort	EDC Data Gathering	EDC Data Gathering
$\Delta kWh_{y,lifetime}$ , Lifetime kWh savings for the cohort being evaluated attributable to the program year being analyzed. Inclusive of $\Delta kWh_y$	Total Lifetime kWh Savings of an HER cohort	EDC Data Gathering	EDC Data Gathering
$ATE_y$ , Average Treatment Effect determined via regression analysis of billed consumption, net of Daily Uplift	kWh/day per household	EDC Data Gathering	EDC Data Gathering
$FYSATE_y$ , First-Year Savings Average Treatment Effect attributable to HERs delivered in year Y	kWh/day per household	EDC Data Gathering	EDC Data Gathering
$Treatment\ Accounts_y$ , number of active homes in the treatment group in year Y.	Households (EDC account number)	EDC Data Gathering	EDC Data Gathering
$Days_y$ , average number of post-treatment days in the analysis period per household	Days	EDC Data Gathering	EDC Data Gathering
$Decay$ , Annual rate of decay of the HER effect when exposure is discontinued	-	Default: 31.3%	1
		EDC Data Gathering	
$Churn$ , Average annual reduction in participating households due to account closures, move-out etc.	-	Default: 6%	2
		EDC Data Gathering	

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**EVALUATION PROTOCOLS**

This protocol deals with the measure life and persistence aspects of HER programs. Chapter 6.1 of the Pennsylvania Evaluation Framework provides detailed guidance on other aspects of HER evaluation protocols.

**SOURCES**

- 1) Pennsylvania Statewide Evaluation Team. Residential Behavioral Program Persistence Study. [http://www.puc.state.pa.us/Electric/pdf/Act129/SWE\\_Res\\_Behavioral\\_Program-Persistence\\_Study\\_Addendum2018.pdf#v=1](http://www.puc.state.pa.us/Electric/pdf/Act129/SWE_Res_Behavioral_Program-Persistence_Study_Addendum2018.pdf#v=1)
- 2) SWE Analysis of average annual churn rate among Phase III EDC cohorts.

cohort



## 2.8 MISCELLANEOUS

### 2.8.1 VARIABLE-SPEED ENERGY STAR POOL PUMPS

<b>Target Sector</b>	Residential Establishments
<b>Measure Unit</b>	Pool Pumps
<b>Measure Life</b>	10 years <sup>Source 1</sup>
<b>Vintage</b>	Replace on Burnout, New Construction

High efficiency pump installations typically employ variable frequency drives and are generally configured to run 24 hours per day at low speed. To achieve adequate filtering the pump must run for longer to compensate for a lower speed/flow. However, this still saves energy since pump power consumption increases with the cube of speed. Consequently, load-shifting of continuous VFD's to reduce demand is not recommended since energy consumption nearly doubles with two turnovers in 20 hours versus 24.

#### ELIGIBILITY

This measure is for the purchase and installation of an ENERGY STAR v3.1 pool pump. The target sector primarily consists of single-family residences.

#### ALGORITHMS

This protocol documents the energy savings attributed to various configurations of ENERGY STAR pool pumps

$$\Delta kWh = \frac{Volume \times Turnover \times Days}{1,000} \times \left( \frac{1}{WEF_{base}} - \frac{1}{WEF_{ee}} \right)$$

$$\Delta kW_{summer\ peak} = \left( \Delta kWh / (HOU \times Days) \right) \times CF_{summer}$$

$$\Delta kW_{winter\ peak} = 0$$

#### DEFINITION OF TERMS

Table 2-167: Terms, Values, and References for Variable Speed Pool Pumps

Term	Unit	Values	Source
Days, Pool pump days of operation per year	$\frac{days}{yr}$	EDC Data Gathering Default: Table 2-169	2
WEF <sub>base</sub> , Baseline weighted energy factor of pool pump for Curve C flow.	$\frac{gallons}{W \cdot h}$	EDC Data Gathering Default: Table 2-168 or Table 2-169	3
WEF <sub>ee</sub> , Weighted energy factor of ENERGY STAR pool pump for Curve C flow.	$\frac{gallons}{W \cdot h}$	EDC Data Gathering Default: Table 2-168 or Table 2-169	4
hhp, hydraulic horsepower is a measure of pump output rather than pump input	745.7 W	EDC Data Gathering Default: Table 2-168 or Table 2-169	2

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<u>Term</u>	<u>Unit</u>	<u>Values</u>	<u>Source</u>
<u>Volume, pool capacity</u>	<u>Gallons</u>	<u>EDC Data Gathering</u> <u>Default: Table 2-169</u>	<u>5</u>
<u>Turnover, number of times the full volume of the pool is filtered each day</u>	<u>Pool volumes</u> <u>day</u>	<u>EDC Data Gathering</u> <u>Default: Table 2-169</u>	<u>6.9</u>
<u>HOU, Hours of operation per day</u>	<u>hours</u> <u>day</u>	<u>EDC Data Gathering</u> <u>Default=24</u>	<u>2</u>
<u>CF<sub>summer</sub>, Coincidence factor</u>	<u>None</u>	<u>EDC Data Gathering</u> <u>Default: Table 2-169</u>	<u>7</u>

Table 2-168 shows the federal standard minimum efficiency (effective as of July 19, 2021), alongside the ENERGY STAR v3.1 specifications (effective July 19, 2021).

**Table 2-168: Pool Pump Weighted Energy Factor Requirements and Specifications**

<u>Pump Type</u>	<u>Nameplate Power (hhp)</u>	<u>Federal Minimum (WEF<sub>base</sub>)</u> <sup>Source 3</sup>	<u>ENERGY STAR (WEF<sub>ee</sub>)</u> <sup>Source 4</sup>
<u>Self-Priming (In-ground)</u>	<u>≤0.130</u>	<u>5.55</u>	<u>13.40</u>
	<u>0.130–0.711</u>	<u>-1.30×ln(hhp)+2.90</u>	<u>-2.45×ln(hhp)+8.40</u>
	<u>0.712–2.500</u>	<u>-2.30×ln(hhp)+6.59</u>	<u>-2.45×ln(hhp)+8.40</u>
<u>Non-Self-Priming (Above-ground)</u>	<u>≤0.130</u>	<u>4.60</u>	<u>4.92</u>
	<u>&gt;0.130</u>	<u>-0.85×ln(hhp)+2.87</u>	<u>-1.00×ln(hhp)+3.85</u>
<u>Pressure Cleaner Booster</u>	<u>Any</u>	<u>0.42</u>	<u>0.51</u>

**Table 2-169: Default Inputs**

<u>Pool/ Pump Type</u>	<u>hhp</u>	<u>WEF<sub>base</sub></u>	<u>WEF<sub>ee</sub></u>	<u>Days</u>	<u>Volume</u>	<u>Turnover</u>	<u>CF</u>
<u>In-ground Pool</u>	<u>0.72</u> <u>Source 2</u>	<u>7.35</u> <u>Source 3</u>	<u>9.20</u> <u>Source 4</u>	<u>122</u> <u>Source 2</u>	<u>15,750</u> <u>Source 5</u>	<u>2</u> <u>Source 6</u>	<u>1</u> <u>Source 7</u>
<u>Above-ground Pool</u>	<u>0.72</u> <u>Source 2</u>	<u>3.15</u> <u>Source 3</u>	<u>4.18</u> <u>Source 4</u>	<u>122</u> <u>Source 2</u>	<u>7,540</u> <u>Source 8</u>	<u>2</u> <u>Source 9</u>	<u>1</u> <u>Source 7</u>
<u>Pressure Cleaner Booster</u>	<u>N/A</u>	<u>0.42</u> <u>Source 3</u>	<u>0.51</u> <u>Source 4</u>	<u>Same as pool</u>		<u>0.08</u> <u>Source 10</u>	<u>0.31</u> <u>Source 11</u>

**DEFAULT SAVINGS**

Default energy and demand savings follow however, many ENERGY STAR pool pumps exceed program specifications; some by as much as 190%. Therefore, EDC's are encouraged to collect records of pool volume, WEF and hhp for installed equipment to calculate the full project savings due. Federal regulations require that equipment ratings be printed on the pump.

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**Table 2-170: Default ENERGY STAR Pool Pump Savings**

<b>Pump Type</b>	<b><math>\Delta kWh</math></b>	<b><math>\Delta kW_{summer\ peak}</math></b>
In-ground Pool	106	0.0361
Above-ground Pool	144	0.0493
Pressure Cleaner Booster, In-ground Pool	67	0.0071
Pressure Cleaner Booster, Above-ground Pool	32	0.0034

**EVALUATION PROTOCOL**

The most appropriate evaluation protocol for this measure is verification of installation coupled with survey on run time and speed settings. It may be helpful to work with pool service professionals in addition to surveying customers to obtain pump settings, as some customers may not be comfortable operating their pump controls. Working with a pool service professional may enable the evaluator to obtain more data points and more accurate data.

**SOURCES**

- 1) California Electronic Technical Reference Manual: (2019). "VSD for Pool & Spa Pump". California Technical Forum. Retrieved February 4, 2022 from <https://www.caetrm.com/measure/SWRE002/01/>
- 2) U.S. EPA. (2020). ENERGY STAR Pool Pump Calculator. Retrieved July 31, 2020 from [https://www.energystar.gov/productfinder/downloads/Pool\\_Pump\\_Calculator\\_2020.05.05\\_FINAL.xlsx](https://www.energystar.gov/productfinder/downloads/Pool_Pump_Calculator_2020.05.05_FINAL.xlsx)
- 3) U.S. DOE. (2017). 10 CFR 431.465(f). Retrieved February 4, 2022 from [https://www.ecfr.gov/current/title-10/chapter-II/subchapter-D/part-431/subpart-Y/section-431.465#p-431.465\(f\)](https://www.ecfr.gov/current/title-10/chapter-II/subchapter-D/part-431/subpart-Y/section-431.465#p-431.465(f))
- 4) U.S. EPA. (2021). ENERGY STAR Program Requirements for Pool Pumps Version 3.1. Retrieved February 4, 2022 from [https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.1%20Pool%20Pumps%20Final%20Specification\\_0.pdf](https://www.energystar.gov/sites/default/files/ENERGY%20STAR%20Version%203.1%20Pool%20Pumps%20Final%20Specification_0.pdf)
- 5) Engineering judgement. Source 1 Gives 15,700 gallons (15,754 in reference R802), source 2 gives 22,000 gallons, and Source 8 gives 15,147 gallons.
- 6) International Swimming Pool and Spa Code. (2015). Section 810.1. Retrieved February 4, 2022 from [https://codes.iccsafe.org/content/ISPSC2018/chapter-8-permanent-inground-residential-swimming-pools#ISPSC2018\\_Ch08\\_Sec810.1](https://codes.iccsafe.org/content/ISPSC2018/chapter-8-permanent-inground-residential-swimming-pools#ISPSC2018_Ch08_Sec810.1)
- 7) To maximize energy savings it is assumed that the pump runs 24 hours per day, which includes 100% of peak.
- 8) Koeller, J., Hoffman, H.W., et al. (2010). "Evaluation of Potential Best Management Practices - Pools, Spas, and Fountains." Retrieved on February 21, 2022 from <https://calwep.org/wp-content/uploads/2021/03/Pools-Spas-and-Fountains-PBMP-2010.pdf>
- 9) International Swimming Pool and Spa Code. (2015). Section 704.4. Accessed February 4, 2022. [https://codes.iccsafe.org/content/ISPSC2018/chapter-7-onground-storable-residential-swimming-pools#ISPSC2018\\_Ch07\\_Sec704.4](https://codes.iccsafe.org/content/ISPSC2018/chapter-7-onground-storable-residential-swimming-pools#ISPSC2018_Ch07_Sec704.4)
- 10) U.S. EPA. (2013). ENERGY STAR Pool Pump Calculator. Retrieved July 31, 2020 from <https://web.archive.org/web/20170427214700/https://www.energystar.gov/sites/default/files/asset/document/Pool%20Pump%20Calculator.xlsx>

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11) [Southern California Edison. \(2008\). Pool Pump Demand Response Potential: Demand and Run-time Monitored Data. Retrieved February 4, 2022 from https://www.etcc-ca.com/sites/default/files/reports/dr07\\_01\\_pool\\_pump\\_demand\\_response\\_potential\\_report.pdf](https://www.etcc-ca.com/sites/default/files/reports/dr07_01_pool_pump_demand_response_potential_report.pdf)  
[Average percentage of all pumps operating during peak hours in Table 16.](#)

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## 2.8.2 SINGLE SPEED POOL PUMP REPLACEMENT

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	VFD Pool Pumps
<b>Measure Life</b>	403.3 years <sup>Source 21</sup>
<b>Vintage</b>	Early Replacement
<b>Vintage</b>	Replace on Burnout

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In this measure a variable speed pool pump must be purchased and installed on a residential pool to replace an existing ~~constant single-speed~~ pool pump. Residential variable frequency drive (VFD) pool pumps can be adjusted to match the minimal flow required for each application. This typically involves running all-day long at the flow rate necessary to achieve the desired number of turnovers per day. Reducing the flow rate results in significant energy savings because ~~pump power and pump energy usage scale with the cubic and quadratic powers of the flow rate respectively. Additional savings are achieved because VFD pool pumps typically employ premium efficiency motors even though the run time is extended proportional to the reduction in flow rate, pump power scales with the cube of the flow rate. For example, halving the flow doubles the time required to process the same volume of water, but the flow power consumption is reduced by 87.5%.~~

If the replacement pump is ENERGY STAR qualified, measure 2.8.1 ENERGY STAR Pool Pumps may also be applied for the same equipment.

### ELIGIBILITY

To qualify for this rebate a variable speed pool pump must be purchased and installed on a residential pool to replace an existing single speed pool pump. The target sector primarily consists of single-family residences.

~~Most VFD pool pumps can display instantaneous flow and power.~~

### ALGORITHMS

This protocol documents the energy savings attributed to variable frequency drive pool pumps in various pool sizes. ~~The target sector primarily consists of single-family residences. There are no demand savings for this measure. These pumps are generally configured to run 24 hours per day at low speed because a pump's power requirements increase with the cube of its speed. Most VFD pool pumps can display instantaneous flow and power.~~

$$\Delta kWh = kWh_{base} - kWh_{VFD}$$

$$kWh_{base} = kW_{ss} \times HOU_{ss} \times Days$$

$$kWh_{VFD} \Delta kWh = \frac{Volume \times Turnover}{EF_{VFD,weighted} \times 1,000 \frac{Wh}{kWh}} \times Days$$

$$= \frac{Volume \times Turnover \times Days}{1,000} \times \left( \frac{1}{EF_{base}} - \frac{1}{WEF_{CFR}} \right)$$

$$\Delta kWh = \left( kW_{ss} - \frac{kWh_{VFD}}{(HOU_{VFD} \times Days)} \right) \times CF$$

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$$HOU_{SS} = Volume \times Turnover \div (Flow_{SS} \times 60 \frac{\text{min}}{\text{hr}})$$

VFD pump sizing algorithm to determine  $EF_{VFD,Weighted}$  using Table 2-140. Select the pump with the smallest  $Flow_{VFD,Low}$  that satisfies calculated flow requirements:

$$Flow_{VFD,Low} = Volume \div \left( \frac{HOU_{VFD}}{Turnover} \times 60 \frac{\text{min}}{\text{hr}} \right)$$

**DEFINITION OF TERMS**

**Table 2-138: Terms, Values, and References for Variable Speed Pool Pumps**

$$\Delta kW_{summer} = \frac{Volume \times Turnover}{1,000} \times \left( \frac{CF_{base}}{EF_{base} \times HOU_{base}} - \frac{CF_{CFR}}{WEF_{CFR} \times HOU_{CFR}} \right)$$

Term	Unit	Values	Source
<i>HOU<sub>SS</sub></i> , Hours of operation per day for single speed pump. This quantity should be recorded by the applicant.	$\frac{hours}{day}$	EDC Data Gathering Default = 9.7 or Calculated	4
<i>kW<sub>SS</sub></i> , Electric demand of single speed pump for Curve C flow rate. This quantity should be recorded by the applicant or looked up in Table 2-139 by horsepower.	Kilowatts	EDC Data Gathering Default = 1.803 kW or See Table 2-139	4
<i>Days</i> , Pool pump days of operation per year.	$\frac{days}{yr}$	122 (4 months)	4
<i>EF<sub>VFD,Weighted</sub></i> , Weighted energy factor of variable frequency drive pump for Curve C flow. This quantity should be recorded by the applicant or looked up in Table 2-140 by horsepower.	$\frac{gallons}{W \cdot h}$	EDC Data Gathering or See Table 2-140, selecting smallest pump that meets <i>Flow<sub>VFD,Low</sub></i>	4
<i>Volume</i> , pool capacity	Gallons	EDC Data Gathering Default = 22,000	4
<i>Turnover</i> , number of times the full volume of the pool is filtered each day	$\frac{Pool\ volumes}{day}$	EDC Data Gathering Default = 2	4
<i>Flow<sub>SS</sub></i> , Single speed pump flow rate	$\frac{gallons}{minute}$	Table 2-139 Default = 78	4
<i>Flow<sub>VFD,Low</sub></i> , Variable frequency drive pump low flow rate	$\frac{gallons}{minute}$	EDC Data Gathering Default = Calculated	4
<i>HOU<sub>VFD</sub></i> , Hours of operation per day for variable frequency drive pool pump	$\frac{hours}{day}$	EDC Data Gathering Default = 24	4

*CF<sub>r</sub>*, None EDC Data Gathering 3  
 Default = 0.34

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### Average Single-Speed Pump Electric Demand

Since this measure involves functional pool pumps, actual measurements of pump demand are encouraged. If this is not possible, then the pool pump power can be inferred from the nameplate horsepower. Table 2-1392-139 shows the average electrical power demand per pump size in the Savings Calculator for an ENERGY STAR-Certified Inground Pool Pump.<sup>Source 1</sup> Note that  $kW_{ss} = Flow_{ss} \times 60 \text{ min/hr} \div (EF_{ss} \times 1,000 \text{ W/kWh})$ .

$$HOU_{base} = Volume \times Turnover \div (Flow_{base} \times 60 \frac{\text{min}}{\text{hr}})$$

**DEFINITION OF TERMS**

**Table 2-171: Single Terms, Values, and References for Variable Speed Curve C Pool Pump Specification<sup>93</sup>Pumps**

Nameplate Power (HP)Term	EF <sub>ss</sub> (Gal/Wh)Unit	Flow <sub>ss</sub> (GPM)Values	kW <sub>ss</sub> Source
0-50Days, Pool pump days of operation per year.	3.4 <sup>days</sup> / <sub>yr</sub>	62-00EDC Data Gathering Default: Table 2-174	1-4012
EF <sub>base</sub> , Baseline weighted energy factor of single-speed pool pump for Curve C flow.	<sup>gallons</sup> / <sub>W · h</sub>	EDC Data Gathering Default: Table 2-172	2
0-75WEFCFR, Weighted energy factor of federal minimum compliant variable frequency drive pump for Curve C flow.	3.3 <sup>gallons</sup> / <sub>W · h</sub>	65-00EDC Data Gathering Default: Table 2-173 or Table 2-174	1-1853
h <sub>hp</sub> , hydraulic horsepower is a measure of pump output rather than pump input.	745.7 W	EDC Data Gathering Default: Table 2-173 or Table 2-174	2
Volume, pool capacity	Gallons	EDC Data Gathering Default: Table 2-174	4
Turnover, number of times the full volume of the pool is filtered each day	<sup>Pool volumes</sup> / <sub>day</sub>	EDC Data Gathering Default: Table 2-174	5.8
1-00Days, Pool pump days of operation per year.	2.5Days	75-50122 (4 months)	1-803
1-50Flow <sub>base</sub> , Single speed pump flow rate	2.3 <sup>gallons</sup> / <sub>minute</sub>	Table 2-172 Default=78-14	2-068
2-00HOU <sub>base</sub> , Hours of operation per day for base case single-speed frequency drive pool pump	2.3 <sup>hours</sup> / <sub>day</sub>	89-67EDC Data Gathering Default: Table 2-174	2-314
2-50HOU <sub>CFR</sub> , Hours of operation per day for variable frequency drive pool pump	2.2 <sup>hours</sup> / <sub>day</sub>	93-09EDC Data Gathering Default: 24	2-564
3-00CF <sub>base</sub> , Coincidence factor of existing pool pump	2-0None	404-67EDC Data Gathering Default: Table 2-174	3-0529
CF <sub>CFR</sub> , Coincidence factor of federal minimum compliant variable speed pool pump in continuous use	None	EDC Data Gathering Default: Table 2-174	6

**Average Single Speed Pump Efficiency**

Since this measure involves functional pool pumps, actual measurements of pump flow and wattage are encouraged. If this is not possible, then the pool pump efficiency can be inferred from

<sup>93</sup> Averaged for all listed single-speed pumps in the last available version of the CEC appliance efficiency database. The powers are for 'CEC Curve A,' which represents hydraulic properties of 2" PVC pipes rather than older, 1.5" copper pipes.

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the nameplate horsepower. Table 2-172 shows the average efficiency factor by pump size. Note that  $EF_{base} = (FLOW_{base} \times 60 \text{ minutes/hour}) \div (Watts)$ .

Table 2-172: Variable Single Speed Curve C Pool Pump Specification<sup>94</sup> Efficiency Factors<sup>Source 2</sup>

Hydraulic Horsepower (Nameplate Power at High Speed)	Flow <sub>VFD,Low</sub> (GPM)		Flow <sub>VFD,High</sub> (GPM)		EF <sub>VFD,Weighted</sub> (Gal/Wh)			
0.72 hhp (1-1.4 HP)	40.33		70.00		8.7			
0.95 hhp (1.65 Nameplate Power (HP))	0.50	410.75	781.00	8.91.50	2.00	2.50	3.00	
1.18 hhp (2-HP)	44.75		89.74		9.3			
EF <sub>base</sub> (Gal/Wh)	3.38	3.29	4.25 hhp (2.5 HP)	45.672.27	2.3	2.18	902.00	7.4
1.65 hhp (3-HP) Flow (Gal/min)	5462.00	40265.00	7.175.50	78.14	89.67	93.09	101.67	

Table 2-173: Replacement Pool Pump Weighted Energy Factor<sup>Source 3</sup>

Pump Type	hhp Range	Federal Minimum (WEFCFR)
Self-Priming (In-ground)	≤0.130	5.55
	0.130–0.711	-1.30×ln(hhp)+2.90
	0.712-2.500	-2.30×ln(hhp)+6.59
Non-Self-Priming (Above-ground)	≤0.130	4.60
	>0.130	-0.85×ln(hhp)+2.87

Table 2-174: Default Inputs

Pool/ Pump Type	hhp	WEFCFR	Days	Volume	Turn-over	HOU <sub>base</sub>	CF <sub>base</sub>	CF <sub>CFR</sub>
In-ground Pool	0.72 <small>Source 2</small>	7.35 <small>Source 3</small>	122 <small>Source 2</small>	15,750 <small>Source 4</small>	2 <small>Source 5</small>	6.3 <small>Source 2</small>	0.31 <small>Source 9</small>	1 <small>Source 6</small>
Above-ground Pool	0.72 <small>Source 2</small>	3.15 <small>Source 3</small>	122 <small>Source 2</small>	7,540 <small>Source 7</small>	2 <small>Source 8</small>	4.0 <small>Source 2</small>	0.31 <small>Source 9</small>	1 <small>Source 6</small>

## DEFAULT SAVINGS

Default energy and demand savings for a 1-HP motor are as follows:

$\Delta kWh = 1,517 \text{ kWh}$

$\Delta kW = 0.4936 \text{ kW}$

<sup>94</sup> Averaged for all listed single-speed pumps in the last available version of the CEC appliance efficiency database. The powers are for "CEC Curve A," which represents hydraulic properties of 2" PVC pipes rather than older, 1.5" copper pipes.

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Default energy and demand savings for a 0.72 hhp (1–1.4 HP equivalent)<sup>Source 2</sup> motor are shown in Table 2-175, including those for the installation of a default ENERGY STAR pool pump from 2.8.1. However, you are encouraged to complete your own calculations for an ENERGY STAR installation to capture the full savings of higher efficiency pumps. Also note that the savings from 2.8.1 ENERGY STAR Pool Pumps extend for another 6.7 years beyond the life of this measure.

**Table 2-175: Default Variable Speed Pool Pump Savings**

<b>Pump Type</b>	<b><math>\Delta</math>kWh</b>	<b><math>\Delta</math>kW<sub>summer peak</sub></b>
<u>Non-ENERGY STAR In-ground Pool</u>	<u>1,170</u>	<u>0.5041</u>
<u>Non-ENERGY STAR Above-ground Pool</u>	<u>226</u>	<u>0.3153</u>
<u>ENERGY STAR In-ground Pool</u>	<u>1,275</u>	<u>0.5402</u>
<u>ENERGY STAR Above-ground Pool</u>	<u>371</u>	<u>0.3646</u>

### **EVALUATION PROTOCOL**

The most appropriate evaluation protocol for this measure is verification of installation coupled with survey on run time and speed settings. It may be helpful to work with pool service professionals in addition to surveying customers to obtain pump settings, as some customers may not be comfortable operating their pump controls. Working with a pool service professional may enable the evaluator to obtain more data points and more accurate data.

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- 4) Engineering judgement. Source 1 Gives 15,700 gallons (15,754 in reference R802), source 2 gives 22,000 gallons, and Source 8 gives 15,147 gallons.
- 2) International Swimming Pool and Spa Code. (2015). California-Public-Utilities-Commission Database for Energy Efficient Resources (DEER) EUL Support Table for 2020, <http://www.deeresources.com/files/DEER2020/download/SupportTable-EUL2020.xlsx>.
- 3) Derived from values for 2pm-6pm for all pool pumps in Pool Pump and Demand Response Potential, DR-07.01 Report, SCE Design and Engineering, Table 16. [https://www.etc-ca.com/sites/default/files/reports/dr07-01\\_pool\\_pump\\_demand\\_response\\_potential\\_report.pdf](https://www.etc-ca.com/sites/default/files/reports/dr07-01_pool_pump_demand_response_potential_report.pdf)
- 5) Section 810.1. Retrieved February 4, 2022 from [https://codes.iccsafe.org/content/ISPSC2018/chapter-8-permanent-inground-residential-swimming-pools#ISPSC2018\\_Ch08\\_Sec810.1](https://codes.iccsafe.org/content/ISPSC2018/chapter-8-permanent-inground-residential-swimming-pools#ISPSC2018_Ch08_Sec810.1)
- 6) To maximize energy savings it is assumed that the pump runs 24 hours per day, which includes 100% of peak.
- 7) Koeller, J., Hoffman, H.W., et al. (2010). "Evaluation of Potential Best Management Practices - Pools, Spas, and Fountains." Retrieved on February 21, 2022 from <https://calwep.org/wp-content/uploads/2021/03/Pools-Spas-and-Fountains-PBMP-2010.pdf>
- 8) International Swimming Pool and Spa Code. (2015). Section 704.4. Accessed February 4, 2022. [https://codes.iccsafe.org/content/ISPSC2018/chapter-7-onground-storable-residential-swimming-pools#ISPSC2018\\_Ch07\\_Sec704.4](https://codes.iccsafe.org/content/ISPSC2018/chapter-7-onground-storable-residential-swimming-pools#ISPSC2018_Ch07_Sec704.4)
- 9) Southern California Edison. (2008). Pool Pump Demand Response Potential: Demand and Run-time Monitored Data. Retrieved February 4, 2022 from [https://www.etc-ca.com/sites/default/files/reports/dr07\\_01\\_pool\\_pump\\_demand\\_response\\_potential\\_report.pdf](https://www.etc-ca.com/sites/default/files/reports/dr07_01_pool_pump_demand_response_potential_report.pdf)  
*Average percentage of all pumps operating during peak hours in Table 16.*

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### 2.8.3 PHOTOVOLTAIC (PV) SOLAR GENERATION

<b>Target Sector</b>	Residential
<b>Measure Unit</b>	Photovoltaic (PV) array
<b>Measure Life</b>	15 years <sup>Source 1</sup>
<b>Vintage</b>	Retrofit or New Construction

#### ELIGIBILITY

Photovoltaic (PV) solar systems consist of an array of panels or thin-film substrates that generate direct current (DC) power when exposed to sunlight. These surfaces are tied together into a single circuit to expand generation levels. The DC power output is converted to alternating current (AC) power through inverter(s) that transform the electricity into the type of power used in residential homes. Generated power must be used to offset concurrent building loads and feed onto the local power grid through net metering to meet the needs of other customers. Charging of on-site battery systems is permitted, however peak demand savings as defined by this measure assumes non-tracking arrays without battery backup. This measure covers residential PV systems up to 30 kW DC.

The goals of Pennsylvania Act 129 are to reduce consumption and congestion on the state's power grid. Projects that generate savings for Act 129 programs must offset existing facility loads. Virtual metering of multiple sites, within the guidelines provided by 52 Pa. Code § 75.14.(e) <sup>Source 2</sup>, will be permitted to define existing loads. Annual generated AC power from the PV array must not exceed 110% of the annual electric energy load of the customer's utility metered consumption.

Default values for project generation estimates can be developed using the National Renewable Energy Laboratory PV Watts<sup>®</sup> calculator <sup>Source 3</sup>. Additional details on required inputs for the PV Watts<sup>®</sup> model are included in the *Algorithms* section below. Demand savings estimated in this measure assume no tracking, panel tilt of 20°, and instantaneous fulfillment of on-site loads or back feeding to the grid.

#### ALGORITHMS

All energy savings will be determined by the PV Watts<sup>®</sup> model and installed system specifications. System losses defined below will be the sum of PV Watts<sup>®</sup> deemed losses (14.08%) and an estimated in-situ loss factor to align model capacity factors with a Pennsylvania statewide analysis of PV system production and expected PV Watts<sup>®</sup> estimates <sup>Source 4</sup>. If the array contains non-tracking panels at varying azimuths or tilts, a new PV Watts<sup>®</sup> model must be completed for each array with the results combined to estimate project savings. There are no default savings for this measure.

$$\text{System Losses} = \text{Default Model Losses} + \text{In-situ Losses}$$

$$\Delta kWh = \text{Provided by PV Watts}$$

$$\Delta kWh_{\text{peak,summer}} = \Delta kWh \times ETDf_{\text{summer}}$$

$$ETDf_{\text{summer}} = ETDf_{\text{summer,ordinal}} + (\Delta \text{Azimuth} * ETDf_{\text{summer,incremental}})$$

$$\Delta \text{Azimuth} = \text{Difference between PV array azimuth and closest, smaller ordinal direction (90, 135, 180, or 225)}$$

$$\Delta kWh_{\text{peak,winter}} = \Delta kWh \times ETDf_{\text{winter}}$$

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$$ETDF_{winter} = ETDF_{winter,ordinal} + (\Delta Azimuth * ETDF_{winter,incremental})$$

**DEFINITION OF TERMS**

**Table 2-176 Terms, Values, and References for Solar PV**

Term	Unit	Value	Sources
<u>Location</u>	<u>n/a</u>	<u>EDC Data Gathering</u>	<u>EDC Data Gathering</u>
<u>DC System Size</u>	<u>kW</u>	<u>EDC Data Gathering</u>	<u>EDC Data Gathering</u>
<u>Module Type</u>	<u>n/a</u>	<u>Standard</u>	<u>Default</u>
<u>Array Type</u>	<u>n/a</u>	<u>EDC Data Gathering</u>	<u>EDC Data Gathering</u>
<u>System Losses</u>	<u>%</u>	<u>Default Model Losses + In-situ Losses</u>	<u>Calculated</u>
<u>Default Model Losses</u>	<u>%</u>	<u>14.08%</u>	<u>PV Watts Model</u>
<u>In-situ Losses</u>	<u>%</u>	<u>Up to 30 kW<sub>DC</sub></u> <u>15%</u>	<u>4</u>
<u>Array Tilt</u>	<u>degrees</u>	<u>EDC Data Gathering</u>	<u>EDC Data Gathering</u>
<u>Array Azimuth</u>	<u>degrees</u>	<u>EDC Data Gathering</u>	<u>EDC Data Gathering</u>
<u>ΔAzimuth</u>	<u>degrees</u>	<u>Calculated</u>	<u>Calculation</u>
<u>Advanced Parameters</u>	<u>n/a</u>	<u>As defined by PV Watts</u>	<u>PV Watts Model</u>
<u>DC to AC Size Ratio</u>	<u>n/a</u>	<u>1.2</u>	<u>Default</u>
<u>Inverter Efficiency</u>	<u>%</u>	<u>96</u>	<u>Default</u>
<u>Ground Coverage Ratio</u>	<u>n/a</u>	<u>0.4</u>	<u>Default</u>
<u>Albedo</u>	<u>n/a</u>	<u>Varies by location</u>	<u>Default</u>
<u>Bifacial</u>	<u>n/a</u>	<u>No</u>	<u>Default</u>
<u>Monthly Irradiance Loss</u>	<u>%</u>	<u>0 for all months</u>	<u>Default</u>
<u>ETDF<sub>summer,ordinal</sub></u>	<u><math>\frac{kW}{kWh}</math></u>	<u>See Table 2-177</u>	<u>5</u>
<u>ETDF<sub>summer,increments</sub></u>	<u><math>\frac{kW}{kWh}</math></u>	<u>See Table 2-178</u>	<u>Calculated</u>
<u>ETDF<sub>winter,ordinal</sub></u>	<u><math>\frac{kW}{kWh}</math></u>	<u>See Table 2-179</u>	<u>6</u>
<u>ETDF<sub>winter,increments</sub></u>	<u><math>\frac{kW}{kWh}</math></u>	<u>See Table 2-180</u>	<u>Calculated</u>

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**Table 2-177: Summer Energy to Demand Factor, East to West facing Ordinal Numbers (ETDF<sub>summer,ordinal</sub>)**

Climate Region	Reference City	Array Azimuth				
		90°	135°	180°	225°	270°
C	Allentown	0.0624265	0.0651860	0.0817416	0.1044553	0.1245200
A	Binghamton	0.0678131	0.0719111	0.0907818	0.1150982	0.1357120
G	Bradford	0.0699694	0.0740833	0.0928029	0.1162379	0.1357924
I	Erie	0.0788975	0.0851381	0.1067952	0.1320825	0.1520063
E	Harrisburg	0.0647908	0.0680365	0.0857973	0.1096607	0.1307424
D	Philadelphia	0.0600152	0.0620246	0.0772186	0.0988952	0.1185881
H	Pittsburgh	0.0722741	0.0765022	0.0948878	0.1179122	0.1370800
B	Scranton	0.0630191	0.0664687	0.0836893	0.1063465	0.1257134
F	Williamsport	0.0679989	0.0712337	0.0883588	0.1107460	0.1301680

**Table 2-178: Summer Energy to Demand Factor Increments, (ETDF<sub>summer,increments</sub>)**

Climate Region	Reference City	Array Azimuth Range			
		90 to 135	135 to 180	180 to 225	225 to 270
C	Allentown	0.0000613	0.0003679	0.0005047	0.0004459
A	Binghamton	0.0000911	0.0004193	0.0005404	0.0004581
G	Bradford	0.0000914	0.0004160	0.0005208	0.0004345
I	Erie	0.0001387	0.0004813	0.0005619	0.0004428
E	Harrisburg	0.0000721	0.0003947	0.0005303	0.0004685
D	Philadelphia	0.0000447	0.0003376	0.0004817	0.0004376
H	Pittsburgh	0.0000940	0.0004086	0.0005117	0.0004260
B	Scranton	0.0000767	0.0003827	0.0005035	0.0004304
F	Williamsport	0.0000719	0.0003806	0.0004975	0.0004316

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**Table 2-179: Winter Energy to Demand Factor Ordinal, East to West facing Ordinal Numbers (ETDF<sub>winter,ordinal</sub>)**

Climate Region	Reference City	Array Azimuth				
		90°	135°	180°	225°	270°
C	Allentown	0.0121198	0.0113890	0.0085075	0.0035736	0.0019462
A	Binghamton	0.0099532	0.0092431	0.0070935	0.0033193	0.0022980
G	Bradford	0.0074126	0.0068730	0.0052236	0.0022748	0.0017657
I	Erie	0.0045040	0.0041701	0.0030910	0.0013280	0.0011115
E	Harrisburg	0.0099236	0.0092490	0.0068901	0.0029286	0.0018332
D	Philadelphia	0.0125401	0.0118317	0.0088548	0.0037608	0.0020548
H	Pittsburgh	0.0060367	0.0056171	0.0043588	0.0019083	0.0015966
B	Scranton	0.0106358	0.0100137	0.0076209	0.0034986	0.0021796
F	Williamsport	0.0096529	0.0089461	0.0067885	0.0030166	0.0020645

**Table 2-180: Winter Energy to Demand Factor Increments, (ETDF<sub>winter,increments</sub>)**

Climate Region	Reference City	Array Azimuth Range			
		90° to 135°	135° to 180°	180° to 225°	225° to 270°
C	Allentown	(0.0000162)	(0.0000640)	(0.0001096)	(0.0000362)
A	Binghamton	(0.0000158)	(0.0000478)	(0.0000839)	(0.0000227)
G	Bradford	(0.0000120)	(0.0000367)	(0.0000655)	(0.0000113)
I	Erie	(0.0000074)	(0.0000240)	(0.0000392)	(0.0000048)
E	Harrisburg	(0.0000150)	(0.0000524)	(0.0000880)	(0.0000243)
D	Philadelphia	(0.0000157)	(0.0000662)	(0.0001132)	(0.0000379)
H	Pittsburgh	(0.0000093)	(0.0000280)	(0.0000545)	(0.0000069)
B	Scranton	(0.0000138)	(0.0000532)	(0.0000916)	(0.0000293)
F	Williamsport	(0.0000157)	(0.0000479)	(0.0000838)	(0.0000212)

**EVALUATION PROTOCOLS**

For most projects, the appropriate evaluation protocol is to verify system specifications (array size, azimuth, tilt, etc.) through document or on-site review and ensure PV Watts® model inputs align with the design parameters used for system generation estimates.

**SOURCES**

- 19) Wisler, R. Bolinger, M. Seel, J. (2020, June). “Benchmarking Utility-Scale PV Operational Expenses and Project Lifetimes: Results from a Survey of U.S. Solar Industry Professionals”. Current EUL assumptions are 25-35 years with an average of 32.5 years. Act 129 caps lifetime at 15 years. Weblink
- 20) 52 Pa. Code § 75.14.(e). Weblink

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- 21) [PV Watts® Calculator. National Renewable Energy Lab \(NREL\). Weblink](#)
- 22) [InClimate for PA PUC. \(2024, February\). "Capacity Factor Analysis EY2014-EY2023". Analysis of Pennsylvania Alternative Energy Portfolio Standards \(AEPS\) Program and additional losses needed to align PV Watts capacity factor output with AEPS Program DC capacity factor analysis.](#)
- 23) [Calculated through the ratio of PV Array total summer peak demand savings \(aligned with PA Ph V peak demand definitions\) and the annual electric generation for a given array azimuth installed at 20° tilt. Incremental  \$ETDF\_{summer}\$  calculated assuming linear changes between two ordinal values.](#)
- 24) [Calculated through the ratio of PV Array total winter peak demand savings \(aligned with PA Ph V peak demand definitions\) and the annual electric generation for a given array azimuth installed at 20° tilt. Incremental  \$ETDF\_{winter}\$  calculated assuming linear changes between two ordinal values.](#)

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## 2.9 DEMAND RESPONSE

The primary focus of this section of the TRM is to provide technical guidance for estimating the load impacts of demand response programs. The methods discussed are aimed at providing accurate estimates of the true load impacts at the program level. EDCs and CSPs may use alternate methods for quarterly reporting of ex ante impacts or to calculate financial settlements with participating customers, but the methods detailed in the TRM should be used to verify achievement of Phase **IV** demand reduction targets. In some instances, the analysis may be carried out at the individual customer level, however, the outcome of interest is the aggregate load reduction (MW) that is caused by the program.

### 2.9.1 DIRECT LOAD CONTROL AND BEHAVIOR-BASED DEMAND RESPONSE PROGRAMS

Target Sector	Residential <del>Establishments</del>
Measure Unit	N/A
Measure Life	Direct Load Control: 11 years Behavioral DR: 1 year
Measure Vintage	N/A

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The protocols for Act 129 covering Direct Load Control (DLC) and Behavior-Based demand response programs are intended to give guidance to the EDCs when dispatching and evaluating the load impacts of an event over the course of Phase **IV**. In these programs, residential and small commercial customers either allow EDCs to remotely reduce equipment run time during peak hours (DLC programs) or reduce their loads voluntarily in response to a combination of incentive payments, messaging and/or other behavioral stimuli.

Behavior-based demand response programs ~~are ones that~~ have a goal of reducing electric load during peak load hours. Examples of behavior-based demand response programs include utility programs that request customers to reduce electric loads during peak load hours voluntarily, programs where customers are provided with real-time information on the cost of electricity and can then take action voluntarily to reduce electric loads during high-cost hours and other similar information programs. For purposes of the Pennsylvania TRM, behavior-based demand response programs do not include utility information programs that are based on consumer education or marketing and have a goal of reducing electricity use on a year-round basis, including non-peak load hours.

For DLC programs, the participants may elect to receive incentive payments for allowing a signaled device to control or limit the power draw of certain HVAC, electric water heating, or swimming pool pump equipment at a participant's home, contributing to the reduction of peak demand. For measurement purposes, peak demand reductions are defined as the difference between a customer's actual (measured) electricity demand, and an estimate of the amount of electricity the customer would have demanded in the absence of the program incentive. The estimate of this counterfactual outcome is referred to as the reference load throughout this protocol.

EDCs must use one of the evaluation approaches below when estimating peak period load reductions that result from DLC and behavior-based programs. The approaches are not equivalent in terms of their ability to produce accurate and robust results and are therefore listed in descending order of desirability. Because of these differences in performance, EDCs shall use Option 2 only under circumstances when Option 1 is infeasible and shall similarly use Option 3 only under circumstances where both Option 1 and Option 2 are infeasible. In situations where Option 1 and/or

2 are not utilized, justification(s) must be provided by the EDC. EDCs with interval meter data available should use it to estimate load impacts. For DLC and behavior-based programs where advanced metering infrastructure (AMI) data is not available for all participants, estimates based on a sample of metered homes is permissible at the discretion of the SWE.

- 1) An analysis based on an experimental design that makes appropriate use of random assignment so that the reference load is estimated using a representative control group of program participants.<sup>95</sup> The most common type of design satisfying this ~~criteria~~ criteria is a randomized control trial (RCT), but other designs may also be used. The specific design used can be selected by the EDC evaluation contractor based on their professional experience. It is important to note that experimental approaches to evaluation generally require the ability to call events at the individual device level. An operations strategy must be determined ahead of time ~~in order~~ to ensure that an appropriate control group is available for the analysis.
- 2) A comparison group analysis where the loads of a group of non-participating customers that are ~~similar to like~~ participating homes with respect to observable characteristics (e.g. electricity consumption) are used to estimate the reference load. A variety of matching techniques are available, and the EDC evaluation contractor can choose the technique used to select the comparison group based on their professional judgment. If ~~summer~~ events are most likely to be called on hot days, hot non-event days should be used for statistical matching and very cool days should be excluded.<sup>96</sup> Similarly, if winter events are most likely to be fall on very cold days, cold non-event days should be used for matching and mild days should be excluded. A good match will result in the loads of treatment and comparison group being virtually identical on non-event days. Difference-in-differences estimators should be used in the analysis to control for any remaining non-event day differences after matching.
- 3) A 'within-subjects' analysis where the loads of participating customers on non-event days<sup>97</sup> (Act 129 or PJM) are used to estimate the reference load. This can be accomplished via a regression equation that relates loads to temperature and other variables that influence usage. The regression model should be estimated using hot or cold days that would be similar to an event. Including ~~cooler~~ mild days in the model can degrade accuracy because it puts more pressure on accurately modeling the relationship between weather and load across a broad temperature spectrum, which is hard because the relationship is not linear. Reducing the ~~estimating~~ estimation sample to relevant days reduces that modeling challenge, ~~or a 'day-matching' technique with a day-of-or-weather adjustment to account for the more extreme conditions in place on event days.~~
- 3) The weather conditions in place at the time of the event are always used to claim savings. Weather-normalized or extrapolation of impacts to other weather conditions is not permitted.

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## ELIGIBILITY

~~In order to~~ To be eligible for ~~the~~ a direct load control program, a customer must have a signaled device used to control the operability of the equipment specified to be called upon during an event.

<sup>95</sup> For discussion on the rationale of random assignment, see Shadish, et al. (*Experimental and quasi-experimental designs for generalized causal inference*, 2002), Khandker, et al. (*Handbook on impact evaluation: quantitative methods and practices*, World Bank Publications, 2010) and Todd, et al. (*Evaluation, measurement and verification (EM&V) of residential behavior-based energy efficiency programs: issues and recommendations*, 2012). More detailed technical discussions of the core evaluation issues and Options 1-3 are provided in the Phase III Evaluation Framework.

<sup>96</sup> Though including some amount of variability in temperatures is necessary for identifying the relationship between temperature and load, including too broad a spectrum of temperatures can reduce modeling accuracy due to the non-linear relationship between the variables. Focusing on hot, event-like days helps to isolate a linear piece of the relationship and enhances the ability of the model to predict accurately.

<sup>97</sup> Either Act 129 or PJM.

All residential and small commercial customers are eligible to participate in the behavior-based program.

**ALGORITHMS**

The specific algorithms(s) used to estimate the demand impacts caused by DLC and behavior-based programs will depend on the specific method of evaluation used. In general, regression-based estimates are most preferred, due to their ability to produce more precise impact estimates and quantitative measures of uncertainty. Details on specific types of equations that can be used for each evaluation approach are provided in the Pennsylvania Evaluation Framework.

Annual peak demand savings must be estimated using individual customer data (e.g. account, meter, or site as defined by program rules) regardless of which evaluation method is used. Program savings are the sum of the load impacts across all participants. Equations 1 and 2 The following equations provide mathematical definitions of the average peak period load impact estimate that would be calculated using an approved method.

$$\Delta kW_{peak} = \frac{\sum_{i=1}^n \Delta kW_i}{n} = \frac{\sum_{i=1}^{n_{summer}} \Delta kW_i}{n_{summer}}$$

$$\Delta kW_{winter peak} = \frac{\sum_{i=1}^{n_{winter}} \Delta kW_i}{n_{winter}}$$

$$\Delta kW_i = kW_{Reference_i} - kW_{Metered_i}$$

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**DEFINITION OF TERMS**

Table 2-181 Definition of Terms for Estimating DLC and Behavior-based Load Impacts

Term	Unit	Values	Source
$n_{summer}$ , Number of summer DR hours during a program year for the EDC	Hours	EDC Data Gathering	EDC Data Gathering
$n_{winter}$ , Number of winter DR hours during a program year for the EDC	Hours	EDC Data Gathering	EDC Data Gathering
$\Delta kW_i$ , Estimated load impact achieved by an LC participant in hour i. This term can be positive (a load reduction) or negative (a load increase).	kW	EDC Data Gathering	EDC Data Gathering
$kW_{Reference_i}$ , Estimated customer load absent DR during hour i	kW	EDC Data Gathering	EDC Data Gathering
$kW_{Metered_i}$ , Measured customer load during hour i	kW	EDC Data Gathering	EDC Data Gathering

**DEFAULT SAVINGS**

Default savings are not available for DLC or behavior-based programs.

### **EVALUATION PROTOCOLS AND REQUIRED REPORTING**

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Technical details of the evaluation protocols for Direct Load Control measures and Behavior-based DR programs are described in the Pennsylvania Evaluation Framework. The end result of following the protocols will be a common set of outputs that allow for an “apples-to-apples” comparison of load impacts across different DR resource options, event conditions and time. These outputs are designed to ensure that the documentation of methods and results allows knowledgeable reviewers to judge the quality and validity of the impact estimates.

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